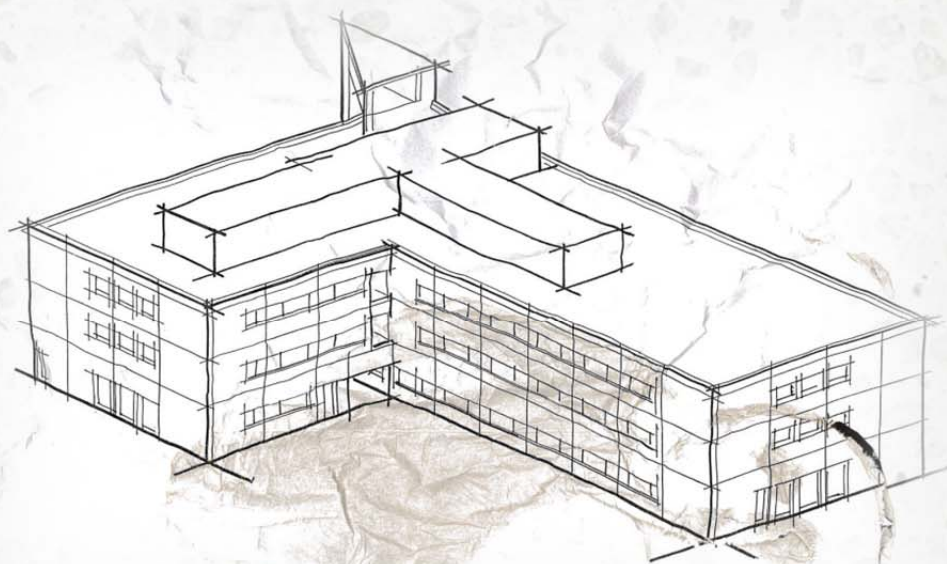


*Masteroppgave ved UiS*

# **ANALYSE & Design**

Ole Kristian Rødde Pedersen

2014



**TILLEGG**

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## ETABS-RESULTATER FOR SYSCO

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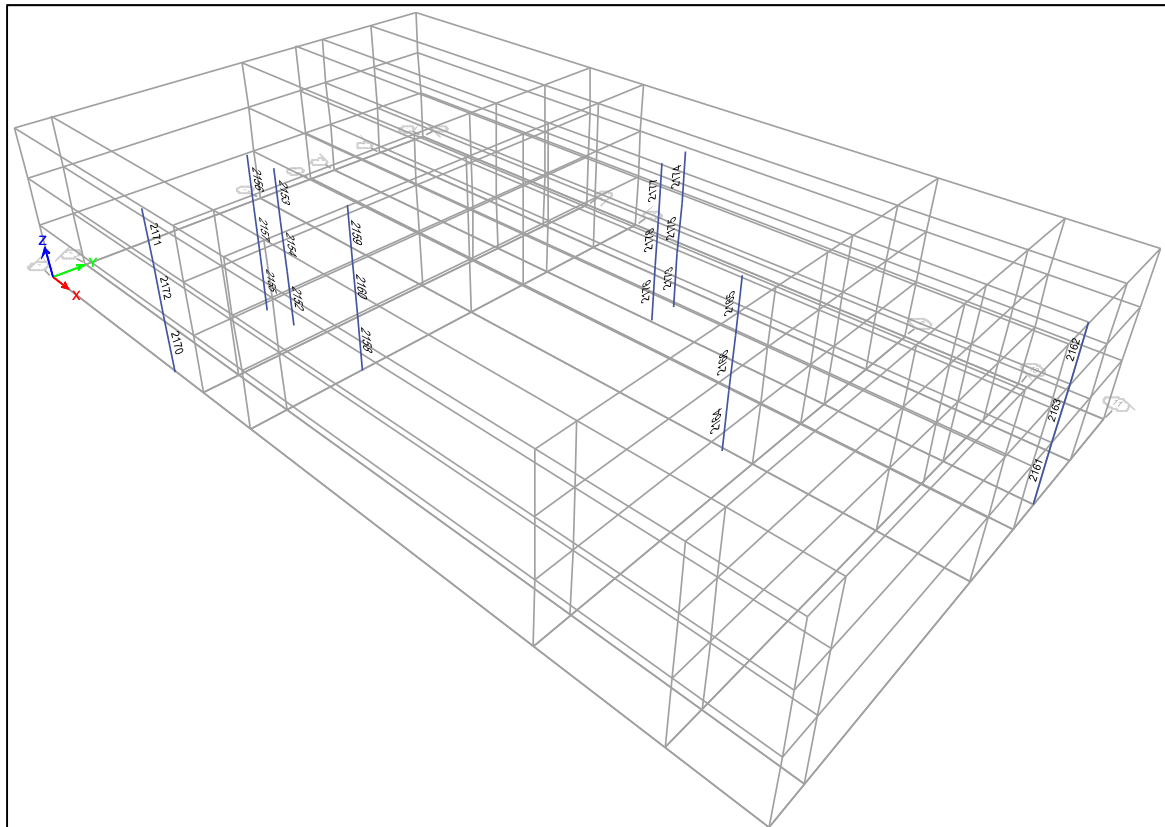
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## 2 IDENTIFISERING AV ELEMENTER

For å finne fram i analyseresultatene er det nødvendig å vite hvor hver stav befinner seg. Her vises stavene på tegning/illustrasjon og i tilhørende tabell

### 2.1 SKJÆRVEGGER

Modelleres som søyler med tykkelse 200mm (tilsvarer innersjiktet i fasadeveggene) og utstrekning 3m. Hver skjærvegg gis samme lengde på 3m for å få en målbar forskyvning i etasjene.



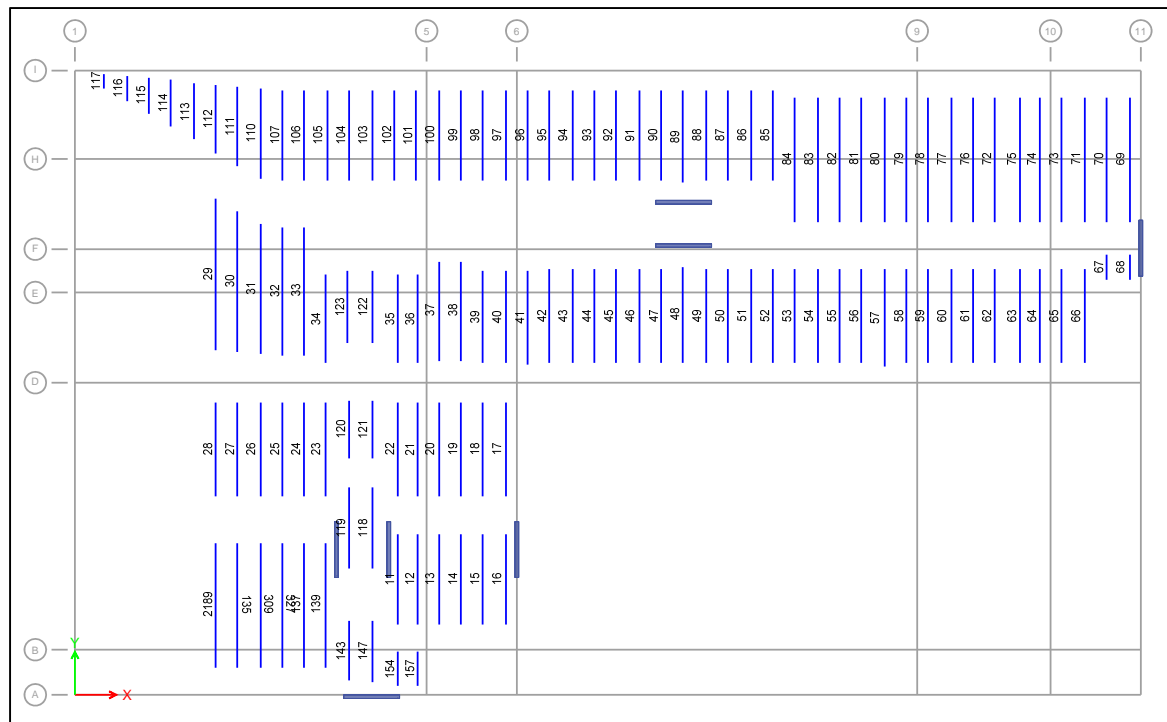
FIGUR A 1 SKJÆRVEGGER

TABLE: Column Connectivity					TABLE: Column Connectivity				
Story	Label	Unique Name	Points	Length mm	Story	Label	Unique Name	Points	Length mm
Story1	C1	2152	2210; 7	4000	Story2	C7	2172	13; 2205	3500
Story1	C2	2155	2211; 249	4000	Story2	C8	2175	10; 2203	3500
Story1	C3	2158	2212; 507	4000	Story2	C9	2178	12; 2204	3500
Story1	C5	2164	2214; 15	4000	Story2	C6	2163	286; 2101	3500
Story1	C7	2170	2216; 13	4000	Story3	C1	2153	2201; 1486	3500
Story1	C8	2173	2217; 10	4000	Story3	C2	2156	2132; 1417	3500
Story1	C9	2176	2218; 12	4000	Story3	C3	2159	1886; 1171	3500
Story1	C6	2161	2213; 286	4000	Story3	C5	2165	2206; 1491	3500
Story2	C1	2154	7; 2201	3500	Story3	C7	2171	2205; 1490	3500
Story2	C2	2157	249; 2132	3500	Story3	C8	2174	2203; 1488	3500
Story2	C3	2160	507; 1886	3500	Story3	C9	2177	2204; 1489	3500
Story2	C5	2166	15; 2206	3500	Story3	C6	2162	2101; 1386	3500

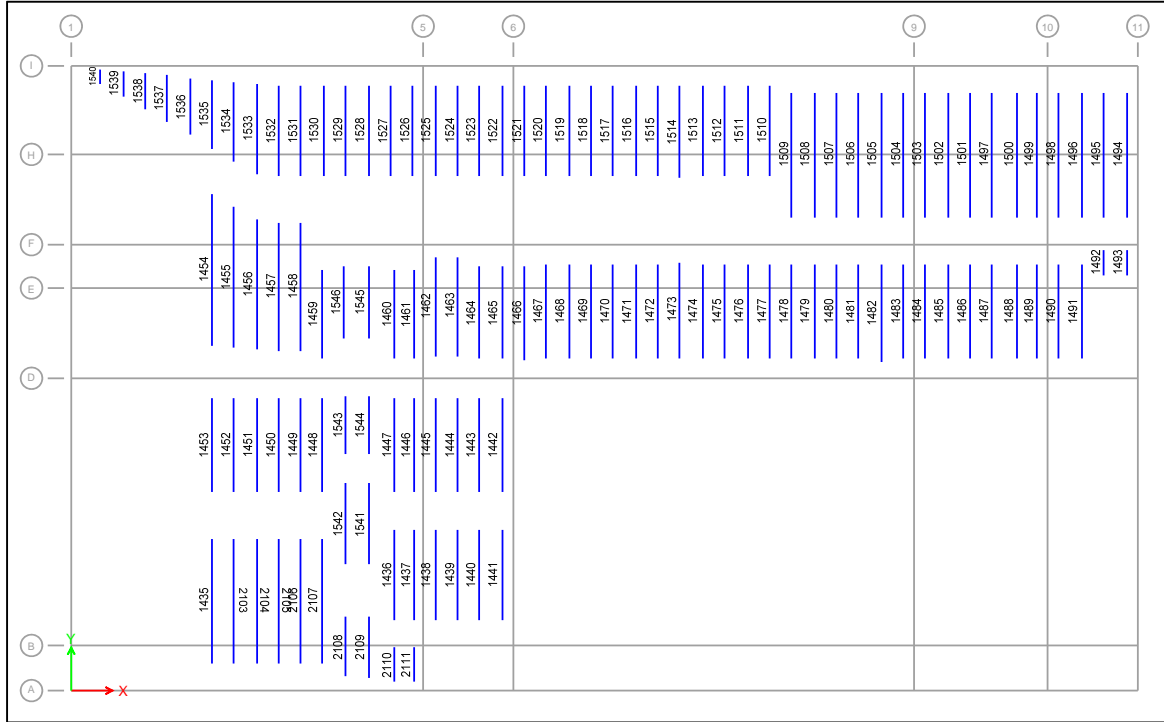
TABELL A 1SKJÆRVEGGER

## 2.2 HULLDEKKESTAVER

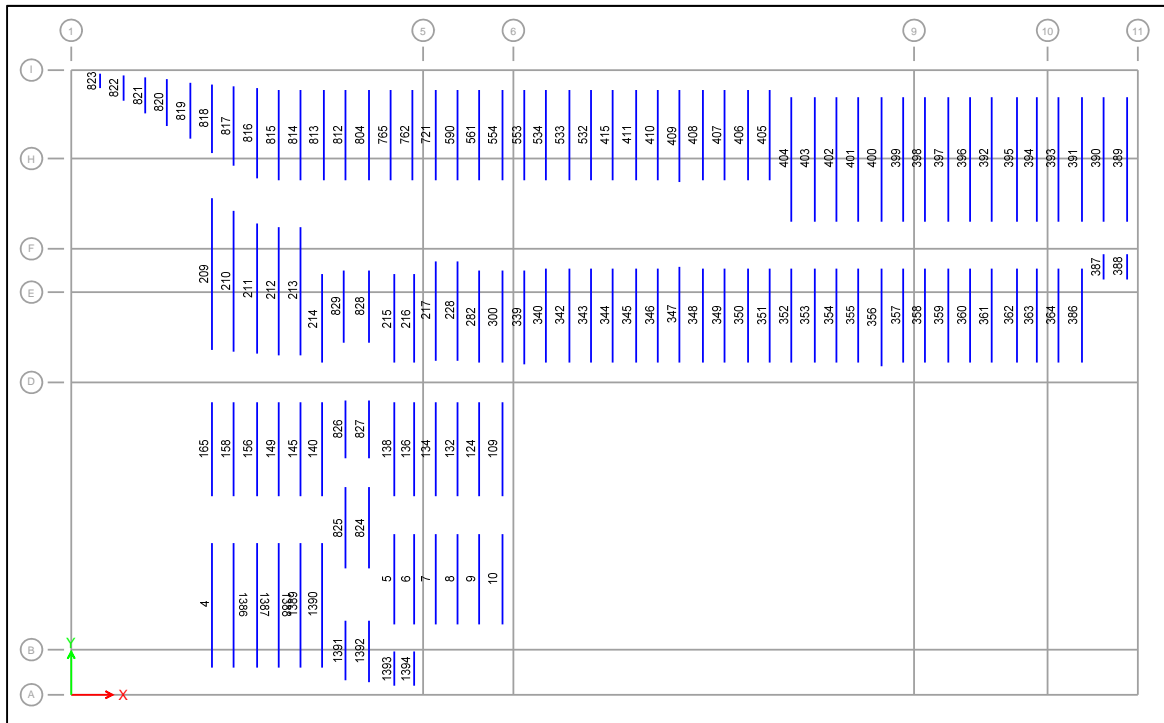
Modelleres med korrekt tverrsnitt tilsvarende HD320 for eksakte forskyvningsberegninger.



FIGUR A 2 HD-STAVER: DEKKE OVER 1.ETG



FIGUR A 3 HD-STAVER: DEKKE OVER 2.ETG



FIGUR A 4 HD-STAVER: DEKKE OVER 3.ETG



TABLE: Beam Connectivity					TABLE: Beam Connectivity				
Story	Label	Unique Name	Points	Length	Story	Label	Unique Name	Points	Length
				mm					mm
Story1	B11	11	21; 22	6890	Story2	B97	1522	1612; 1613	7025
Story1	B12	12	23; 24	6890	Story2	B98	1523	1614; 1615	7025
Story1	B13	13	25; 26	6890	Story2	B99	1524	1616; 1617	7025
Story1	B14	14	27; 28	6890	Story2	B100	1525	1618; 1619	7025
Story1	B15	15	29; 30	6890	Story2	B101	1526	1620; 1621	7025
Story1	B16	16	31; 32	6890	Story2	B102	1527	1622; 1623	7025
Story1	B17	17	32; 33	7200	Story2	B103	1528	1624; 1625	7025
Story1	B18	18	30; 34	7200	Story2	B104	1529	1626; 1627	7025
Story1	B19	19	28; 35	7200	Story2	B105	1530	1628; 1629	7025
Story1	B20	20	26; 36	7200	Story2	B106	1531	1630; 1631	7025
Story1	B21	21	24; 37	7200	Story2	B107	1532	1632; 1633	7025
Story1	B22	22	22; 38	7200	Story2	B110	1533	1525; 1634	6833.7
Story1	B25	25	8; 41	7200	Story2	B111	1534	1524; 1635	6032.3
Story1	B26	26	6; 42	7200	Story2	B112	1535	1636; 1523	5230.9
Story1	B27	27	4; 43	7200	Story2	B113	1536	1637; 1638	4429.5
Story1	B28	28	2; 44	7200	Story2	B114	1537	1639; 1640	3628.2
Story1	B29	29	45; 44	11569.1	Story2	B115	1538	1641; 1642	2826.8
Story1	B30	30	46; 43	10767.7	Story2	B116	1539	1643; 1644	2025.4
Story1	B31	31	42; 47	9966.3	Story2	B117	1540	1645; 1646	1224
Story1	B35	35	38; 51	6825	Story2	B120	1543	1649; 1650	4430
Story1	B36	36	52; 37	6825	Story2	B121	1544	1651; 1652	4430
Story1	B37	37	36; 53	7640	Story2	B155	1467	1653; 1534	7285
Story1	B38	38	35; 54	7640	Story2	B156	1468	1654; 1535	7285
Story1	B39	39	34; 55	7025	Story2	B157	1469	1655; 1536	7285
Story1	B40	40	33; 56	7025	Story2	B159	1471	1657; 1538	7285
Story1	B41	41	57; 58	7115	Story2	B160	1472	1658; 1539	7285
Story1	B52	52	79; 80	7290	Story2	B169	1488	1663; 1577	7290
Story1	B53	53	81; 82	7290	Story2	B170	1489	1664; 1575	7290
Story1	B55	55	85; 86	7290	Story2	B171	1490	1665; 1573	7290
Story1	B56	56	87; 88	7290	Story2	B172	1491	1666; 1570	7290
Story1	B58	58	91; 92	7290	Story2	B42	1448	1668; 1669	7200
Story1	B59	59	93; 94	7290	Story2	B43	1449	1667; 1670	7200
Story1	B60	60	95; 96	7290	Story2	B45	1459	1669; 1671	6825
Story1	B61	61	97; 98	7290	Story2	B46	1546	1672; 1673	5595
Story1	B62	62	99; 100	7290	Story2	B47	1457	1632; 1519	9775
Story1	B67	67	109; 110	1940	Story2	B48	1458	1670; 1630	9775
Story1	B68	68	111; 112	1940	Story2	B49	1542	1648; 1649	6200
Story1	B69	69	112; 113	9600	Story2	B50	1541	1647; 1651	6200
Story1	B70	70	110; 114	9600	Story2	B51	1545	1674; 1675	5600

Story1	B71	71	115; 116	9600	Story2	B210	1479	1547; 1548	7290
Story1	B72	72	100; 117	9600	Story2	B54	1435	2136; 1495	9600
Story1	B73	73	118; 119	9600	Story2	B430	2103	1496; 2137	9600
Story1	B74	74	120; 121	9600	Story2	B531	2104	1497; 2138	9600
Story1	B75	75	122; 123	9600	Story2	B533	2105	1498; 2139	9600
Story1	B76	76	98; 124	9600	Story2	B535	2106	2140; 1667	9600
Story1	B77	77	96; 125	9600	Story2	B537	2107	1668; 2141	9600
Story1	B78	78	94; 126	9600	Story2	B539	2108	2142; 1499	4680
Story1	B79	79	92; 127	9600	Story2	B543	2110	2144; 1501	2710
Story1	B80	80	90; 128	9600	Story2	B545	2111	2145; 1503	2710
Story1	B81	81	88; 129	9600	Story2	B10	2109	2205; 1500	4795
Story1	B82	82	86; 130	9600	Story2	B2	1473	2207; 2204	7435
Story1	B83	83	84; 131	9600	Story2	B3	1470	1537; 1656	7285
Story1	B84	84	82; 132	9600	Story2	B9	1474	1661; 1540	7285
Story1	B85	85	133; 134	7025	Story2	B24	1475	1660; 1541	7285
Story1	B86	86	135; 136	7025	Story2	B32	1476	1659; 1542	7285
Story1	B87	87	137; 138	7025	Story2	B33	1482	1553; 2206	7450
Story1	B88	88	139; 140	7025	Story2	B34	1514	1597; 2203	7155
Story1	B90	90	143; 144	7025	Story3	B11	5	449; 450	6890
Story1	B91	91	145; 146	7025	Story3	B12	6	451; 452	6890
Story1	B92	92	147; 148	7025	Story3	B13	7	453; 454	6890
Story1	B93	93	149; 150	7025	Story3	B14	8	455; 521	6890
Story1	B94	94	151; 152	7025	Story3	B15	9	522; 530	6890
Story1	B95	95	153; 154	7025	Story3	B16	10	556; 579	6890
Story1	B96	96	155; 156	7025	Story3	B17	109	579; 594	7200
Story1	B97	97	157; 158	7025	Story3	B18	124	530; 610	7200
Story1	B98	98	159; 160	7025	Story3	B19	132	521; 635	7200
Story1	B99	99	161; 162	7025	Story3	B20	134	454; 636	7200
Story1	B100	100	163; 164	7025	Story3	B21	136	452; 641	7200
Story1	B101	101	165; 166	7025	Story3	B22	138	450; 642	7200
Story1	B102	102	167; 168	7025	Story3	B25	149	446; 643	7200
Story1	B103	103	169; 170	7025	Story3	B26	156	445; 729	7200
Story1	B104	104	171; 172	7025	Story3	B27	158	444; 731	7200
Story1	B105	105	173; 174	7025	Story3	B28	165	443; 799	7200
Story1	B106	106	175; 176	7025	Story3	B29	209	808; 799	11569.1
Story1	B107	107	177; 178	7025	Story3	B30	210	809; 731	10767.7
Story1	B110	110	47; 183	6833.7	Story3	B31	211	729; 810	9966.3
Story1	B111	111	46; 184	6032.3	Story3	B35	215	642; 811	6825
Story1	B112	112	185; 45	5230.9	Story3	B36	216	812; 641	6825
Story1	B113	113	186; 187	4429.5	Story3	B37	217	636; 813	7640
Story1	B114	114	188; 189	3628.2	Story3	B38	228	635; 814	7640
Story1	B115	115	190; 191	2826.8	Story3	B39	282	610; 815	7025
Story1	B116	116	192; 193	2025.4	Story3	B40	300	594; 816	7025
Story1	B117	117	194; 195	1224	Story3	B41	339	817; 818	7115



Story1	B120	120	200; 201	4430	Story3	B52	351	828; 829	7290
Story1	B121	121	202; 203	4430	Story3	B53	352	830; 831	7290
Story1	B155	42	237; 59	7285	Story3	B55	354	834; 835	7290
Story1	B156	43	238; 61	7285	Story3	B56	355	836; 837	7290
Story1	B157	44	239; 63	7285	Story3	B58	357	839; 840	7290
Story1	B159	46	241; 67	7285	Story3	B59	358	841; 842	7290
Story1	B160	47	242; 69	7285	Story3	B60	359	843; 844	7290
Story1	B169	63	259; 122	7290	Story3	B61	360	845; 846	7290
Story1	B170	64	260; 120	7290	Story3	B62	361	847; 848	7290
Story1	B171	65	261; 118	7290	Story3	B67	387	849; 850	1940
Story1	B172	66	262; 115	7290	Story3	B68	388	851; 852	1940
Story1	B42	23	19; 20	7200	Story3	B69	389	852; 853	9600
Story1	B43	24	17; 60	7200	Story3	B70	390	850; 854	9600
Story1	B45	34	20; 64	6825	Story3	B71	391	855; 856	9600
Story1	B46	123	66; 68	5595	Story3	B72	392	848; 857	9600
Story1	B47	32	177; 41	9775	Story3	B73	393	858; 859	9600
Story1	B48	33	60; 175	9775	Story3	B74	394	860; 861	9600
Story1	B49	119	198; 200	6200	Story3	B75	395	862; 863	9600
Story1	B50	118	196; 202	6200	Story3	B76	396	846; 864	9600
Story1	B51	122	70; 72	5600	Story3	B77	397	844; 865	9600
Story1	B210	54	83; 84	7290	Story3	B78	398	842; 866	9600
Story1	B54	2189	644; 2	9600	Story3	B79	399	840; 867	9600
Story1	B430	135	4; 645	9600	Story3	B80	400	838; 868	9600
Story1	B531	309	6; 671	9600	Story3	B81	401	837; 869	9600
Story1	B533	327	8; 672	9600	Story3	B82	402	835; 870	9600
Story1	B535	137	707; 17	9600	Story3	B83	403	833; 871	9600
Story1	B537	139	19; 708	9600	Story3	B84	404	831; 872	9600
Story1	B539	143	712; 14	4680	Story3	B85	405	873; 874	7025
Story1	B543	154	714; 21	2710	Story3	B86	406	875; 876	7025
Story1	B545	157	715; 23	2710	Story3	B87	407	877; 878	7025
Story1	B10	147	13; 16	4795	Story3	B88	408	879; 880	7025
Story1	B2	48	3; 12	7435	Story3	B90	410	883; 884	7025
Story2	B11	1436	1501; 1502	6890	Story3	B91	411	885; 886	7025
Story2	B12	1437	1503; 1504	6890	Story3	B92	415	887; 888	7025
Story2	B13	1438	1505; 1506	6890	Story3	B93	532	889; 890	7025
Story2	B14	1439	1507; 1508	6890	Story3	B94	533	891; 892	7025
Story2	B15	1440	1509; 1510	6890	Story3	B95	534	893; 894	7025
Story2	B16	1441	1511; 1512	6890	Story3	B96	553	895; 896	7025
Story2	B17	1442	1512; 1513	7200	Story3	B97	554	897; 898	7025
Story2	B18	1443	1510; 1514	7200	Story3	B98	561	899; 900	7025
Story2	B19	1444	1508; 1515	7200	Story3	B99	590	901; 902	7025
Story2	B20	1445	1506; 1516	7200	Story3	B100	721	903; 904	7025
Story2	B21	1446	1504; 1517	7200	Story3	B101	762	905; 906	7025
Story2	B22	1447	1502; 1518	7200	Story3	B102	765	907; 908	7025

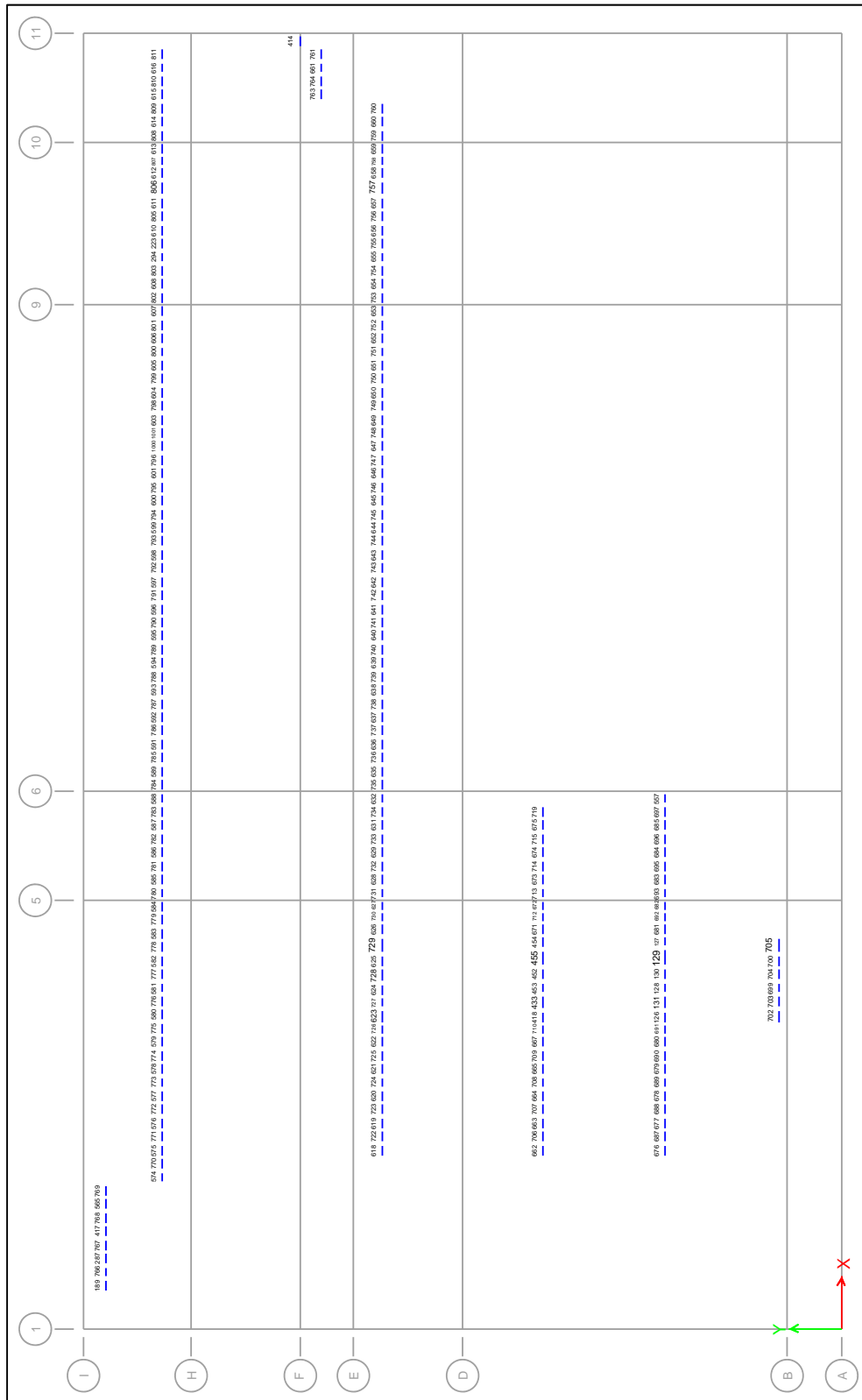
Story2	B25	1450	1498; 1519	7200	Story3	B103	804	909; 910	7025
Story2	B26	1451	1497; 1520	7200	Story3	B104	812	911; 912	7025
Story2	B27	1452	1496; 1521	7200	Story3	B105	813	913; 914	7025
Story2	B28	1453	1495; 1522	7200	Story3	B106	814	915; 916	7025
Story2	B29	1454	1523; 1522	11569.1	Story3	B107	815	917; 918	7025
Story2	B30	1455	1524; 1521	10767.7	Story3	B110	816	810; 919	6833.7
Story2	B31	1456	1520; 1525	9966.3	Story3	B111	817	809; 920	6032.3
Story2	B35	1460	1518; 1526	6825	Story3	B112	818	921; 808	5230.9
Story2	B36	1461	1527; 1517	6825	Story3	B113	819	922; 923	4429.5
Story2	B37	1462	1516; 1528	7640	Story3	B114	820	924; 925	3628.2
Story2	B38	1463	1515; 1529	7640	Story3	B115	821	926; 927	2826.8
Story2	B39	1464	1514; 1530	7025	Story3	B116	822	928; 929	2025.4
Story2	B40	1465	1513; 1531	7025	Story3	B117	823	930; 931	1224
Story2	B41	1466	1532; 1533	7115	Story3	B120	826	934; 935	4430
Story2	B52	1477	1543; 1544	7290	Story3	B121	827	936; 937	4430
Story2	B53	1478	1545; 1546	7290	Story3	B155	340	938; 819	7285
Story2	B55	1480	1549; 1550	7290	Story3	B156	342	939; 820	7285
Story2	B56	1481	1551; 1552	7290	Story3	B157	343	940; 821	7285
Story2	B58	1483	1554; 1555	7290	Story3	B159	345	942; 823	7285
Story2	B59	1484	1556; 1557	7290	Story3	B160	346	943; 824	7285
Story2	B60	1485	1558; 1559	7290	Story3	B169	362	948; 862	7290
Story2	B61	1486	1560; 1561	7290	Story3	B170	363	949; 860	7290
Story2	B62	1487	1562; 1563	7290	Story3	B171	364	950; 858	7290
Story2	B67	1492	1564; 1565	1940	Story3	B172	386	951; 855	7290
Story2	B68	1493	1566; 1567	1940	Story3	B42	140	953; 954	7200
Story2	B69	1494	1567; 1568	9600	Story3	B43	145	952; 955	7200
Story2	B70	1495	1565; 1569	9600	Story3	B45	214	954; 956	6825
Story2	B71	1496	1570; 1571	9600	Story3	B46	829	957; 958	5595
Story2	B72	1497	1563; 1572	9600	Story3	B47	212	917; 643	9775
Story2	B73	1498	1573; 1574	9600	Story3	B48	213	955; 915	9775
Story2	B74	1499	1575; 1576	9600	Story3	B49	825	933; 934	6200
Story2	B75	1500	1577; 1578	9600	Story3	B50	824	932; 936	6200
Story2	B76	1501	1561; 1579	9600	Story3	B51	828	959; 960	5600
Story2	B77	1502	1559; 1580	9600	Story3	B210	353	832; 833	7290
Story2	B78	1503	1557; 1581	9600	Story3	B54	4	1421; 443	9600
Story2	B79	1504	1555; 1582	9600	Story3	B430	1386	444; 1422	9600
Story2	B80	1505	1553; 1583	9600	Story3	B531	1387	445; 1423	9600
Story2	B81	1506	1552; 1584	9600	Story3	B533	1388	446; 1424	9600
Story2	B82	1507	1550; 1585	9600	Story3	B535	1389	1425; 952	9600
Story2	B83	1508	1548; 1586	9600	Story3	B537	1390	953; 1426	9600
Story2	B84	1509	1546; 1587	9600	Story3	B539	1391	1427; 447	4680
Story2	B85	1510	1588; 1589	7025	Story3	B543	1393	1429; 449	2710
Story2	B86	1511	1590; 1591	7025	Story3	B545	1394	1430; 451	2710
Story2	B87	1512	1592; 1593	7025	Story3	B10	1392	1490; 448	4795

Story2	B88	1513	1594; 1595	7025	Story3	B2	347	1492; 1489	7435
Story2	B90	1515	1598; 1599	7025	Story3	B3	344	822; 941	7285
Story2	B91	1516	1600; 1601	7025	Story3	B9	348	946; 825	7285
Story2	B92	1517	1602; 1603	7025	Story3	B24	349	945; 826	7285
Story2	B93	1518	1604; 1605	7025	Story3	B32	350	944; 827	7285
Story2	B94	1519	1606; 1607	7025	Story3	B33	356	838; 1491	7450
Story2	B95	1520	1608; 1609	7025	Story3	B34	409	882; 1488	7155
Story2	B96	1521	1610; 1611	7025					

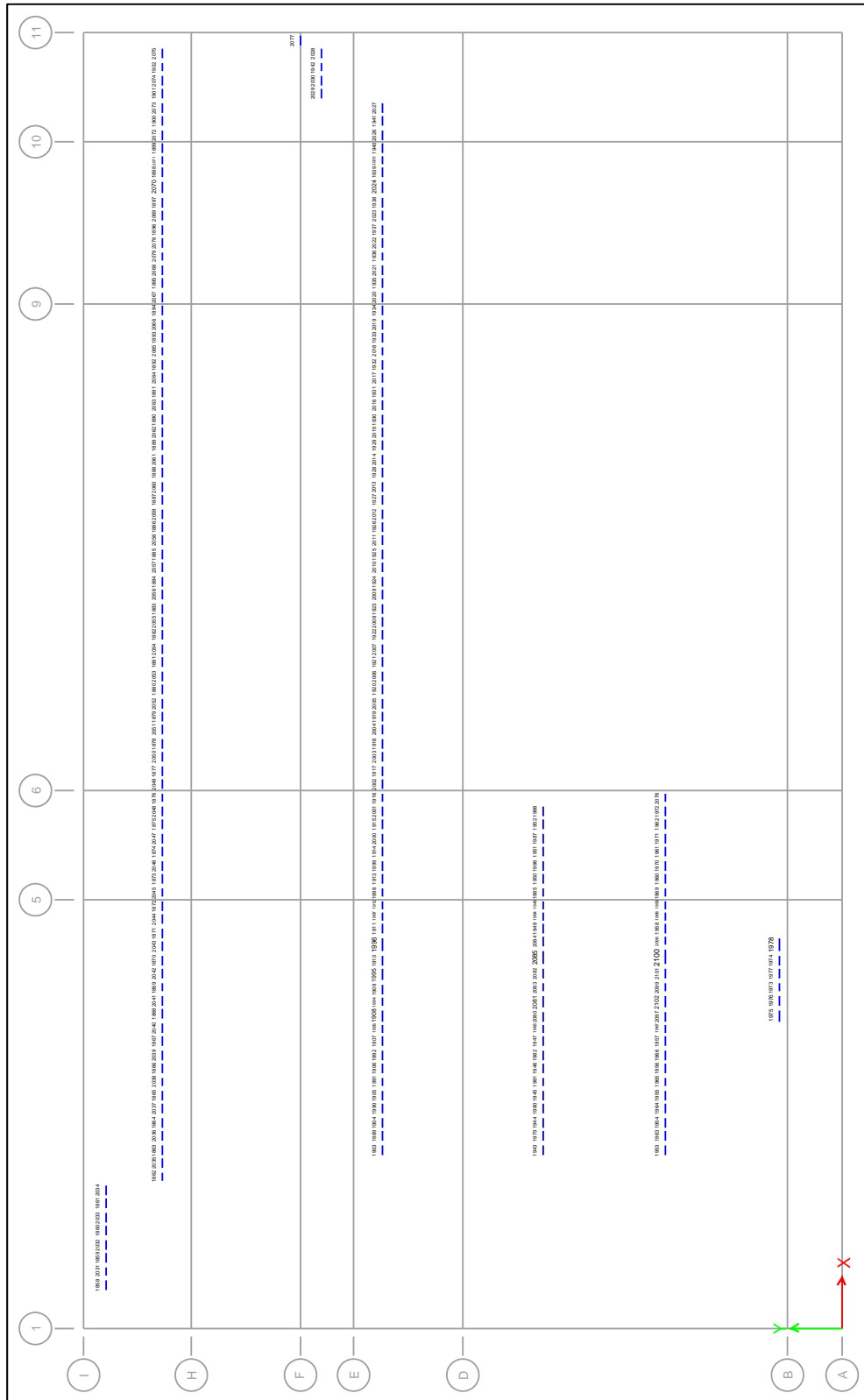
TABELL A 2 HULLDEKKESTAVER

## 2.3 HD-SKJÆRSTAV

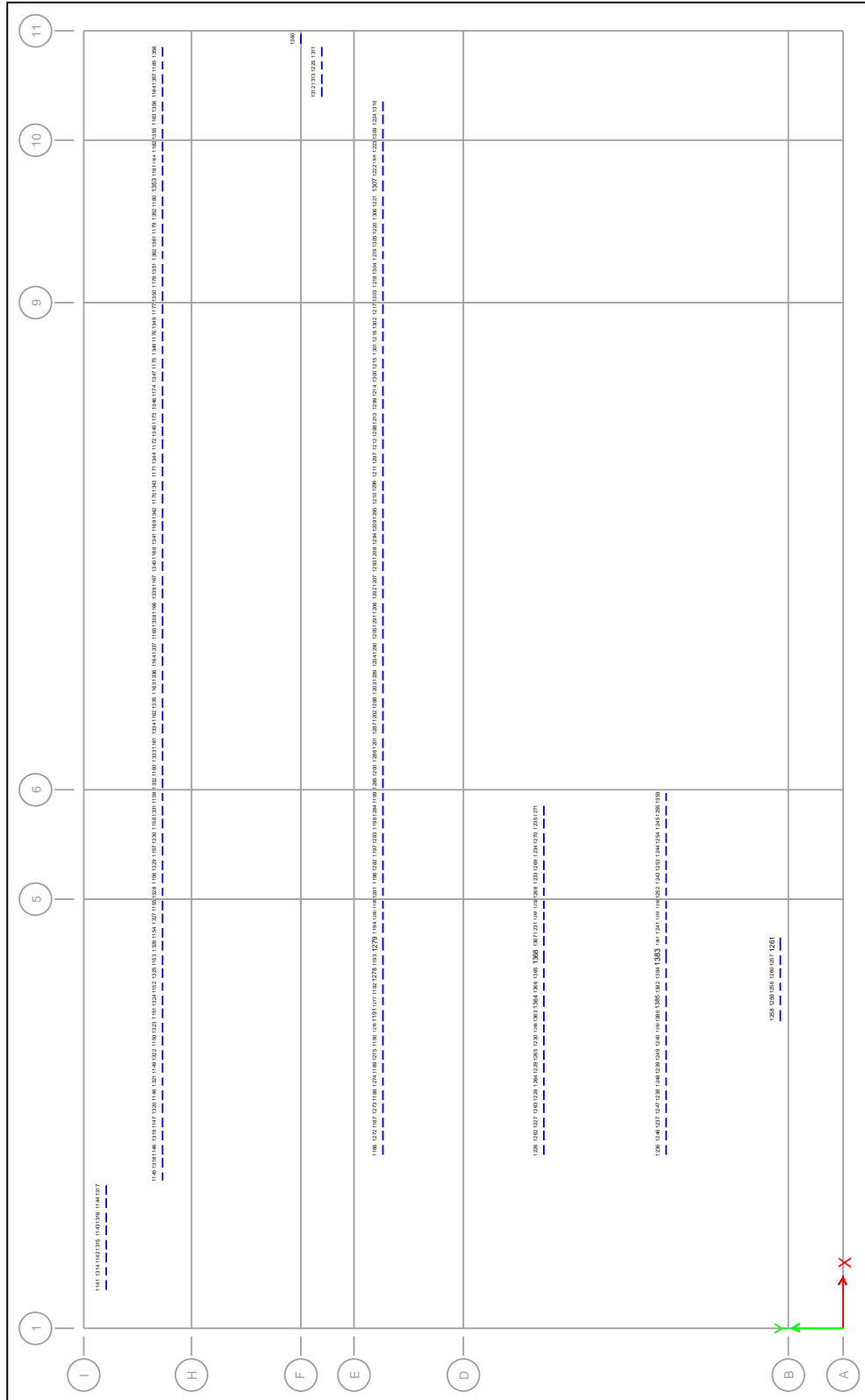
Skjærforbindelser i fuger mellom elementene og mot skjærvegger



FIGUR A 5 SKJÆRSTAV: DEKKE OVER 1.ETG



FIGUR A 6 SKJÆRSTAVER: DEKKE OVER 2.ETG



FIGUR A 7 SKJÆRSTAVER: DEKKE OVER 3.ETG



TABLE: Beam Connectivity					TABLE: Beam Connectivity				
Story	Label	Unique Name	Points	Length	Story	Label	Unique Name	Points	Length
				mm					mm
Story1	B530	557	512; 507	600	Story2	B785	2058	1940; 1941	600
Story1	B288	287	374; 489	600	Story2	B786	2059	1942; 1943	600
Story1	B574	578	532; 533	600	Story2	B787	2060	1944; 1945	600
Story1	B575	579	534; 535	600	Story2	B788	2061	1946; 2099	600
Story1	B576	580	536; 537	600	Story2	B208	1889	2099; 1947	600
Story1	B577	581	538; 539	600	Story2	B209	1890	1948; 1949	600
Story1	B578	582	540; 541	600	Story2	B282	1891	1950; 1951	600
Story1	B579	583	542; 543	600	Story2	B286	1892	1952; 1953	600
Story1	B580	584	544; 545	600	Story2	B294	1893	1954; 1955	600
Story1	B581	585	546; 547	600	Story2	B414	1894	1956; 1957	600
Story1	B582	586	548; 549	600	Story2	B429	1895	1958; 1959	600
Story1	B583	587	550; 551	600	Story2	B479	1896	1961; 1962	600
Story1	B584	588	552; 553	600	Story2	B509	1897	1963; 1964	600
Story1	B585	589	554; 555	600	Story2	B527	1898	1965; 1966	600
Story1	B586	785	555; 557	600	Story2	B528	1899	1967; 1968	600
Story1	B587	591	557; 558	600	Story2	B529	1900	1969; 1970	600
Story1	B588	592	559; 560	600	Story2	B550	1901	1971; 1972	600
Story1	B589	593	561; 562	600	Story2	B561	1902	1973; 1974	600
Story1	B590	594	563; 564	600	Story2	B613	2062	1947; 1948	600
Story1	B591	595	565; 566	600	Story2	B629	2063	1949; 1950	600
Story1	B592	596	567; 568	600	Story2	B661	2064	1951; 1952	600
Story1	B593	597	569; 570	600	Story2	B696	2065	1953; 1954	600
Story1	B594	598	571; 572	600	Story2	B706	2066	1955; 1956	600
Story1	B595	599	573; 574	600	Story2	B755	2067	1957; 1958	600
Story1	B596	600	575; 576	600	Story2	B758	2068	1959; 1960	600
Story1	B597	601	577; 578	600	Story2	B806	2069	1962; 1963	600
Story1	B631	636	647; 648	600	Story2	B808	2070	1964; 1965	725
Story1	B632	637	649; 650	600	Story2	B810	2071	1966; 1967	475
Story1	B633	638	651; 652	600	Story2	B811	2072	1968; 1969	600
Story1	B634	639	653; 654	600	Story2	B812	2073	1970; 1971	600
Story1	B635	640	655; 656	600	Story2	B813	2074	1972; 1973	600
Story1	B636	641	657; 658	600	Story2	B814	2075	1974; 1975	600
Story1	B637	642	659; 660	600	Story2	B816	2078	2102; 1961	600
Story1	B638	643	661; 662	600	Story2	B817	2079	1960; 2102	600
Story1	B639	644	663; 664	600	Story2	B842	1858	2103; 1889	600
Story1	B640	645	665; 666	600	Story2	B843	2031	1889; 1890	600
Story1	B641	646	667; 668	600	Story2	B844	1860	2097; 1892	600
Story1	B642	647	669; 670	600	Story2	B845	2033	1892; 2104	600
Story1	B644	649	673; 674	600	Story2	B846	1861	2104; 1893	600
Story1	B645	650	675; 676	600	Story2	B847	2034	1893; 2098	600
Story1	B646	651	677; 678	600	Story2	B848	1865	2105; 1900	600
Story1	B647	652	679; 680	600	Story2	B849	2038	1900; 1901	600
Story1	B648	653	681; 682	600	Story2	B850	1864	1898; 1899	600
Story1	B649	654	683; 684	600	Story2	B851	2037	1899; 2105	600
Story1	B650	655	685; 686	600	Story2	B852	1863	1896; 1897	600

Story1	B651	656	687; 688	600	Story2	B853	2036	1897; 1898	600
Story1	B652	657	689; 690	600	Story2	B854	1862	1894; 1895	600
Story1	B653	658	691; 692	600	Story2	B855	2035	1895; 1896	600
Story1	B654	659	693; 694	600	Story2	B856	1917	2106; 2004	600
Story1	B655	660	695; 696	600	Story2	B857	2003	2004; 2005	600
Story1	B656	661	697; 698	600	Story2	B858	1903	1976; 1977	600
Story1	B657	662	699; 700	600	Story2	B859	1904	1978; 1979	600
Story1	B658	663	701; 702	600	Story2	B860	1905	1980; 1981	600
Story1	B659	664	703; 704	600	Story2	B861	1906	1982; 1983	600
Story1	B660	665	705; 706	600	Story2	B862	1907	1984; 1985	600
Story1	B662	667	709; 710	600	Story2	B863	1908	1986; 1987	700
Story1	B666	671	717; 718	600	Story2	B864	1909	1988; 1989	600
Story1	B667	672	719; 720	500	Story2	B865	1910	1990; 1991	600
Story1	B668	673	721; 722	600	Story2	B866	1911	1992; 1993	600
Story1	B669	674	723; 724	600	Story2	B867	1912	1994; 1995	500
Story1	B670	675	725; 726	600	Story2	B868	1913	1996; 1997	600
Story1	B701	706	700; 701	600	Story2	B869	1914	1998; 1999	600
Story1	B702	707	702; 703	600	Story2	B870	1915	2000; 2001	600
Story1	B703	708	704; 705	600	Story2	B871	1916	2002; 2003	600
Story1	B704	709	706; 709	600	Story2	B872	1989	1977; 1978	600
Story1	B705	710	710; 711	500	Story2	B873	1990	1979; 1980	600
Story1	B707	712	718; 719	500	Story2	B874	1991	1981; 1982	600
Story1	B708	713	720; 721	600	Story2	B875	1992	1983; 1984	600
Story1	B709	714	722; 723	600	Story2	B876	1993	1985; 1986	500
Story1	B710	715	724; 725	600	Story2	B877	1994	1987; 1988	500
Story1	B712	719	726; 764	600	Story2	B878	1995	1989; 1990	700
Story1	B730	737	648; 649	600	Story2	B879	1996	1991; 1992	800
Story1	B731	738	650; 651	600	Story2	B880	1997	1993; 1994	500
Story1	B732	739	652; 653	600	Story2	B881	1998	1995; 1996	600
Story1	B733	740	654; 655	600	Story2	B882	1999	1997; 1998	600
Story1	B734	741	656; 657	600	Story2	B883	2000	1999; 2000	600
Story1	B735	742	658; 659	600	Story2	B884	2001	2001; 2002	600
Story1	B736	743	660; 661	600	Story2	B885	2002	2003; 2106	600
Story1	B737	744	662; 663	600	Story2	B886	1958	2107; 2081	600
Story1	B738	745	664; 665	600	Story2	B887	1959	2108; 2082	500
Story1	B739	746	666; 667	600	Story2	B888	1960	2109; 2083	600
Story1	B740	747	668; 669	600	Story2	B889	1961	2110; 2084	600
Story1	B741	748	670; 673	600	Story2	B890	1962	2111; 2085	600
Story1	B742	749	674; 675	600	Story2	B891	1968	2081; 2108	500
Story1	B743	750	676; 677	600	Story2	B892	1969	2082; 2109	600
Story1	B744	751	678; 679	600	Story2	B893	1970	2083; 2110	600
Story1	B745	752	680; 681	600	Story2	B894	1971	2084; 2111	600
Story1	B746	753	682; 683	600	Story2	B895	1972	2085; 2100	600
Story1	B747	754	684; 685	600	Story2	B896	1953	2112; 2076	600
Story1	B748	755	686; 687	600	Story2	B897	1954	2113; 2077	600
Story1	B749	756	688; 689	600	Story2	B898	1955	2114; 2078	600
Story1	B750	757	690; 691	725	Story2	B899	1956	2115; 2079	600
Story1	B751	758	692; 693	475	Story2	B900	1957	2116; 2080	600

Story1	B752	759	694; 695	600	Story2	B901	1963	2076; 2113	600
Story1	B753	760	696; 776	600	Story2	B902	1964	2077; 2114	600
Story1	B754	761	698; 777	600	Story2	B903	1965	2078; 2115	600
Story1	B756	763	778; 779	600	Story2	B904	1966	2079; 2116	600
Story1	B757	764	779; 697	600	Story2	B905	1967	2080; 2117	500
Story1	B760	767	489; 783	600	Story2	B906	2080	2065; 2118	600
Story1	B767	774	533; 534	600	Story2	B908	2081	2118; 2119	700
Story1	B768	775	535; 536	600	Story2	B910	2083	2119; 2121	600
Story1	B769	776	537; 538	600	Story2	B911	2082	2121; 2120	600
Story1	B770	777	539; 540	600	Story2	B914	2084	2122; 2066	600
Story1	B771	778	541; 542	600	Story2	B915	2085	2120; 2122	800
Story1	B772	779	543; 544	600	Story2	B8	2097	2117; 2132	600
Story1	B773	780	545; 546	600	Story2	B148	2099	2133; 2134	600
Story1	B774	781	547; 548	600	Story2	B152	2102	2132; 2133	700
Story1	B775	782	549; 550	600	Story2	B154	2101	2134; 2135	600
Story1	B776	783	551; 552	600	Story2	B4	2098	2201; 2107	500
Story1	B777	784	553; 554	600	Story2	B5	2100	2135; 2201	900
Story1	B778	786	558; 559	600	Story2	B44	2077	1567; 2101	600
Story1	B779	787	560; 561	600	Story2	B145	1973	459; 460	600
Story1	B780	788	562; 563	600	Story2	B146	1974	461; 466	600
Story1	B781	789	564; 565	600	Story2	B147	1975	467; 468	650
Story1	B782	790	566; 567	600	Story2	B149	1976	468; 459	650
Story1	B783	791	568; 569	600	Story2	B150	1977	460; 461	600
Story1	B784	792	570; 571	600	Story2	B151	1978	466; 1690	800
Story1	B785	793	572; 573	600	Story3	B530	1359	1385; 1171	600
Story1	B786	794	574; 575	600	Story3	B288	1142	1175; 1176	600
Story1	B787	795	576; 577	600	Story3	B574	1149	1186; 1187	600
Story1	B788	796	578; 790	600	Story3	B575	1150	1188; 1189	600
Story1	B208	1000	790; 580	600	Story3	B576	1151	1190; 1191	600
Story1	B209	603	581; 582	600	Story3	B577	1152	1192; 1193	600
Story1	B282	604	583; 584	600	Story3	B578	1153	1194; 1195	600
Story1	B286	605	585; 586	600	Story3	B579	1154	1196; 1197	600
Story1	B294	606	587; 588	600	Story3	B580	1155	1198; 1199	600
Story1	B414	607	589; 590	600	Story3	B581	1156	1200; 1201	600
Story1	B429	608	591; 592	600	Story3	B582	1157	1202; 1203	600
Story1	B479	610	595; 596	600	Story3	B583	1158	1204; 1205	600
Story1	B509	611	597; 598	600	Story3	B584	1159	1206; 1207	600
Story1	B527	612	599; 600	600	Story3	B585	1160	1208; 1209	600
Story1	B528	613	601; 602	600	Story3	B586	1333	1209; 1210	600
Story1	B529	614	603; 604	600	Story3	B587	1161	1210; 1211	600
Story1	B550	615	605; 606	600	Story3	B588	1162	1212; 1213	600
Story1	B561	616	607; 608	600	Story3	B589	1163	1214; 1215	600
Story1	B613	1001	580; 581	600	Story3	B590	1164	1216; 1217	600
Story1	B629	798	582; 583	600	Story3	B591	1165	1218; 1219	600
Story1	B661	799	584; 585	600	Story3	B592	1166	1220; 1221	600
Story1	B696	800	586; 587	600	Story3	B593	1167	1222; 1223	600
Story1	B706	801	588; 589	600	Story3	B594	1168	1224; 1225	600
Story1	B755	802	590; 591	600	Story3	B595	1169	1226; 1227	600

Story1	B758	803	592; 593	600	Story3	B596	1170	1228; 1229	600
Story1	B806	805	596; 597	600	Story3	B597	1171	1230; 1231	600
Story1	B808	806	598; 599	725	Story3	B631	1201	1290; 1291	600
Story1	B810	807	600; 601	475	Story3	B632	1202	1292; 1293	600
Story1	B811	808	602; 603	600	Story3	B633	1203	1294; 1295	600
Story1	B812	809	604; 605	600	Story3	B634	1204	1296; 1297	600
Story1	B813	810	606; 607	600	Story3	B635	1205	1298; 1299	600
Story1	B814	811	608; 609	600	Story3	B636	1206	1300; 1301	600
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Story1	B817	294	593; 210	600	Story3	B638	1208	1304; 1305	600
Story1	B842	189	211; 207	600	Story3	B639	1209	1306; 1307	600
Story1	B843	766	207; 374	600	Story3	B640	1210	1308; 1309	600
Story1	B844	417	783; 502	600	Story3	B641	1211	1310; 1311	600
Story1	B845	768	502; 212	600	Story3	B642	1212	1312; 1313	600
Story1	B846	565	212; 523	600	Story3	B644	1213	1314; 1315	600
Story1	B847	769	523; 785	600	Story3	B645	1214	1316; 1317	600
Story1	B848	577	213; 531	600	Story3	B646	1215	1318; 1319	600
Story1	B849	773	531; 532	600	Story3	B647	1216	1320; 1321	600
Story1	B850	576	528; 529	600	Story3	B648	1217	1322; 1323	600
Story1	B851	772	529; 213	600	Story3	B649	1218	1324; 1325	600
Story1	B852	575	526; 527	600	Story3	B650	1219	1326; 1327	600
Story1	B853	771	527; 528	600	Story3	B651	1220	1328; 1329	600
Story1	B854	574	524; 525	600	Story3	B652	1221	1330; 1331	600
Story1	B855	770	525; 526	600	Story3	B653	1222	1332; 1333	600
Story1	B856	635	285; 646	600	Story3	B654	1223	1334; 1335	600
Story1	B857	736	646; 647	600	Story3	B655	1224	1336; 1337	600
Story1	B858	618	611; 612	600	Story3	B656	1225	1338; 1339	600
Story1	B859	619	613; 614	600	Story3	B657	1226	1340; 1341	600
Story1	B860	620	615; 616	600	Story3	B658	1227	1342; 1343	600
Story1	B861	621	617; 618	600	Story3	B659	1228	1344; 1345	600
Story1	B862	622	619; 620	600	Story3	B660	1229	1346; 1347	600
Story1	B863	623	621; 622	700	Story3	B662	1230	1348; 1349	600
Story1	B864	624	623; 624	600	Story3	B666	1231	1351; 1352	600
Story1	B865	625	625; 626	600	Story3	B667	1232	1353; 1354	500
Story1	B866	626	627; 628	600	Story3	B668	1233	1355; 1356	600
Story1	B867	627	629; 630	500	Story3	B669	1234	1357; 1358	600
Story1	B868	628	631; 632	600	Story3	B670	1235	1359; 1360	600
Story1	B869	629	633; 634	600	Story3	B701	1262	1341; 1342	600
Story1	B870	631	637; 638	600	Story3	B702	1263	1343; 1344	600
Story1	B871	632	639; 640	600	Story3	B703	1264	1345; 1346	600
Story1	B872	722	612; 613	600	Story3	B704	1265	1347; 1348	600
Story1	B873	723	614; 615	600	Story3	B705	1266	1349; 1350	500
Story1	B874	724	616; 617	600	Story3	B707	1267	1352; 1353	500
Story1	B875	725	618; 619	600	Story3	B708	1268	1354; 1355	600
Story1	B876	726	620; 621	500	Story3	B709	1269	1356; 1357	600
Story1	B877	727	622; 623	500	Story3	B710	1270	1358; 1359	600
Story1	B878	728	624; 625	700	Story3	B712	1271	1360; 1377	600
Story1	B879	729	626; 627	800	Story3	B730	1287	1291; 1292	600

Story1	B880	730	628; 629	500	Story3	B731	1288	1293; 1294	600
Story1	B881	731	630; 631	600	Story3	B732	1289	1295; 1296	600
Story1	B882	732	632; 633	600	Story3	B733	1290	1297; 1298	600
Story1	B883	733	634; 637	600	Story3	B734	1291	1299; 1300	600
Story1	B884	734	638; 639	600	Story3	B735	1292	1301; 1302	600
Story1	B885	735	640; 285	600	Story3	B736	1293	1303; 1304	600
Story1	B886	681	287; 738	600	Story3	B737	1294	1305; 1306	600
Story1	B887	682	288; 740	500	Story3	B738	1295	1307; 1308	600
Story1	B888	683	289; 742	600	Story3	B739	1296	1309; 1310	600
Story1	B889	684	290; 744	600	Story3	B740	1297	1311; 1312	600
Story1	B890	685	291; 746	600	Story3	B741	1298	1313; 1314	600
Story1	B891	692	738; 288	500	Story3	B742	1299	1315; 1316	600
Story1	B892	693	740; 289	600	Story3	B743	1300	1317; 1318	600
Story1	B893	695	742; 290	600	Story3	B744	1301	1319; 1320	600
Story1	B894	696	744; 291	600	Story3	B745	1302	1321; 1322	600
Story1	B895	697	746; 512	600	Story3	B746	1303	1323; 1324	600
Story1	B896	676	292; 728	600	Story3	B747	1304	1325; 1326	600
Story1	B897	677	293; 730	600	Story3	B748	1305	1327; 1328	600
Story1	B898	678	320; 732	600	Story3	B749	1306	1329; 1330	600
Story1	B899	679	367; 734	600	Story3	B750	1307	1331; 1332	725
Story1	B900	680	395; 736	600	Story3	B751	1308	1333; 1334	475
Story1	B901	687	728; 293	600	Story3	B752	1309	1335; 1336	600
Story1	B902	688	730; 320	600	Story3	B753	1310	1337; 1378	600
Story1	B903	689	732; 367	600	Story3	B754	1311	1339; 1379	600
Story1	B904	690	734; 395	600	Story3	B756	1312	1380; 1381	600
Story1	B905	691	736; 408	500	Story3	B757	1313	1381; 1338	600
Story1	B906	418	711; 409	600	Story3	B760	1315	1176; 1382	600
Story1	B908	433	409; 475	700	Story3	B767	1322	1187; 1188	600
Story1	B910	453	475; 484	600	Story3	B768	1323	1189; 1190	600
Story1	B911	452	484; 477	600	Story3	B769	1324	1191; 1192	600
Story1	B914	454	503; 717	600	Story3	B770	1325	1193; 1194	600
Story1	B915	455	477; 503	800	Story3	B771	1326	1195; 1196	600
Story1	B8	126	408; 249	600	Story3	B772	1327	1197; 1198	600
Story1	B148	128	518; 519	600	Story3	B773	1328	1199; 1200	600
Story1	B152	131	249; 518	700	Story3	B774	1329	1201; 1202	600
Story1	B154	130	519; 520	600	Story3	B775	1330	1203; 1204	600
Story1	B4	127	7; 287	500	Story3	B776	1331	1205; 1206	600
Story1	B5	129	520; 7	900	Story3	B777	1332	1207; 1208	600
Story1	B44	414	112; 286	600	Story3	B778	1334	1211; 1212	600
Story1	B145	699	389; 391	600	Story3	B779	1335	1213; 1214	600
Story1	B146	700	392; 412	600	Story3	B780	1336	1215; 1216	600
Story1	B147	702	413; 415	650	Story3	B781	1337	1217; 1218	600
Story1	B149	703	415; 389	650	Story3	B782	1338	1219; 1220	600
Story1	B150	704	391; 392	600	Story3	B783	1339	1221; 1222	600
Story1	B151	705	412; 208	800	Story3	B784	1340	1223; 1224	600
Story2	B530	2076	2100; 1886	600	Story3	B785	1341	1225; 1226	600
Story2	B288	1859	1890; 1891	600	Story3	B786	1342	1227; 1228	600
Story2	B574	1866	1901; 1902	600	Story3	B787	1343	1229; 1230	600

Story2	B575	1867	1903; 1904	600	Story3	B788	1344	1231; 1384	600
Story2	B576	1868	1905; 1906	600	Story3	B208	1172	1384; 1232	600
Story2	B577	1869	1907; 1908	600	Story3	B209	1173	1233; 1234	600
Story2	B578	1870	1909; 1910	600	Story3	B282	1174	1235; 1236	600
Story2	B579	1871	1911; 1912	600	Story3	B286	1175	1237; 1238	600
Story2	B580	1872	1913; 1914	600	Story3	B294	1176	1239; 1240	600
Story2	B581	1873	1915; 1916	600	Story3	B414	1177	1241; 1242	600
Story2	B582	1874	1917; 1918	600	Story3	B429	1178	1243; 1244	600
Story2	B583	1875	1919; 1920	600	Story3	B479	1179	1246; 1247	600
Story2	B584	1876	1921; 1922	600	Story3	B509	1180	1248; 1249	600
Story2	B585	1877	1923; 1924	600	Story3	B527	1181	1250; 1251	600
Story2	B586	2050	1924; 1925	600	Story3	B528	1182	1252; 1253	600
Story2	B587	1878	1925; 1926	600	Story3	B529	1183	1254; 1255	600
Story2	B588	1879	1927; 1928	600	Story3	B550	1184	1256; 1257	600
Story2	B589	1880	1929; 1930	600	Story3	B561	1185	1258; 1259	600
Story2	B590	1881	1931; 1932	600	Story3	B613	1345	1232; 1233	600
Story2	B591	1882	1933; 1934	600	Story3	B629	1346	1234; 1235	600
Story2	B592	1883	1935; 1936	600	Story3	B661	1347	1236; 1237	600
Story2	B593	1884	1937; 1938	600	Story3	B696	1348	1238; 1239	600
Story2	B594	1885	1939; 1940	600	Story3	B706	1349	1240; 1241	600
Story2	B595	1886	1941; 1942	600	Story3	B755	1350	1242; 1243	600
Story2	B596	1887	1943; 1944	600	Story3	B758	1351	1244; 1245	600
Story2	B597	1888	1945; 1946	600	Story3	B806	1352	1247; 1248	600
Story2	B631	1918	2005; 2006	600	Story3	B808	1353	1249; 1250	725
Story2	B632	1919	2007; 2008	600	Story3	B810	1354	1251; 1252	475
Story2	B633	1920	2009; 2010	600	Story3	B811	1355	1253; 1254	600
Story2	B634	1921	2011; 2012	600	Story3	B812	1356	1255; 1256	600
Story2	B635	1922	2013; 2014	600	Story3	B813	1357	1257; 1258	600
Story2	B636	1923	2015; 2016	600	Story3	B814	1358	1259; 1260	600
Story2	B637	1924	2017; 2018	600	Story3	B816	1361	1387; 1246	600
Story2	B638	1925	2019; 2020	600	Story3	B817	1362	1245; 1387	600
Story2	B639	1926	2021; 2022	600	Story3	B842	1141	1388; 1174	600
Story2	B640	1927	2023; 2024	600	Story3	B843	1314	1174; 1175	600
Story2	B641	1928	2025; 2026	600	Story3	B844	1143	1382; 1177	600
Story2	B642	1929	2027; 2028	600	Story3	B845	1316	1177; 1389	600
Story2	B644	1930	2029; 2030	600	Story3	B846	1144	1389; 1178	600
Story2	B645	1931	2031; 2032	600	Story3	B847	1317	1178; 1383	600
Story2	B646	1932	2033; 2034	600	Story3	B848	1148	1390; 1185	600
Story2	B647	1933	2035; 2036	600	Story3	B849	1321	1185; 1186	600
Story2	B648	1934	2037; 2038	600	Story3	B850	1147	1183; 1184	600
Story2	B649	1935	2039; 2040	600	Story3	B851	1320	1184; 1390	600
Story2	B650	1936	2041; 2042	600	Story3	B852	1146	1181; 1182	600
Story2	B651	1937	2043; 2044	600	Story3	B853	1319	1182; 1183	600
Story2	B652	1938	2045; 2046	600	Story3	B854	1145	1179; 1180	600
Story2	B653	1939	2047; 2048	600	Story3	B855	1318	1180; 1181	600
Story2	B654	1940	2049; 2050	600	Story3	B856	1200	1391; 1289	600
Story2	B655	1941	2051; 2052	600	Story3	B857	1286	1289; 1290	600
Story2	B656	1942	2053; 2054	600	Story3	B858	1186	1261; 1262	600



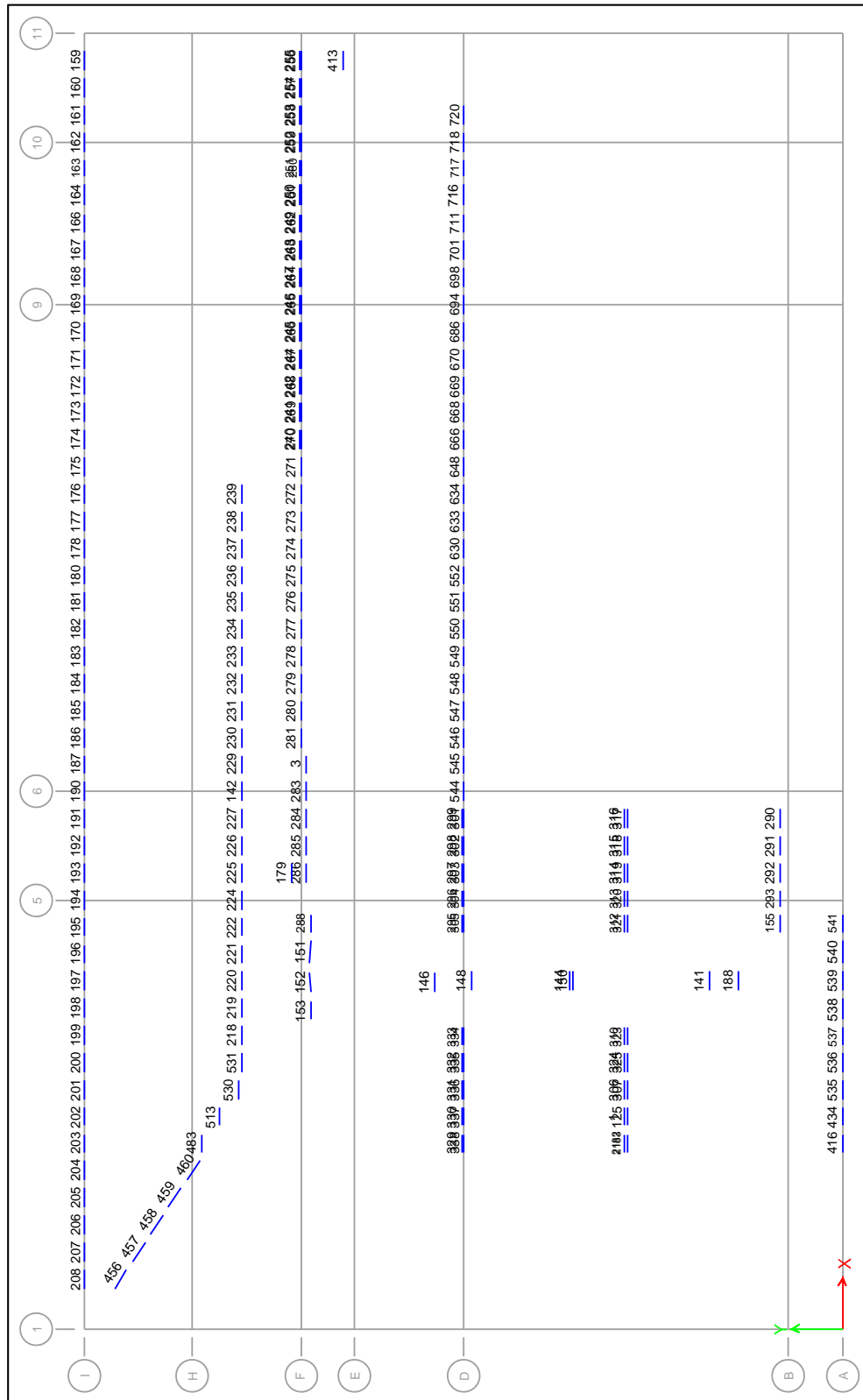
Story2	B657	1943	2055; 2056	600	Story3	B859	1187	1263; 1264	600
Story2	B658	1944	2057; 2058	600	Story3	B860	1188	1265; 1266	600
Story2	B659	1945	2059; 2060	600	Story3	B861	1189	1267; 1268	600
Story2	B660	1946	2061; 2062	600	Story3	B862	1190	1269; 1270	600
Story2	B662	1947	2063; 2064	600	Story3	B863	1191	1271; 1272	700
Story2	B666	1948	2066; 2067	600	Story3	B864	1192	1273; 1274	600
Story2	B667	1949	2068; 2069	500	Story3	B865	1193	1275; 1276	600
Story2	B668	1950	2070; 2071	600	Story3	B866	1194	1277; 1278	600
Story2	B669	1951	2072; 2073	600	Story3	B867	1195	1279; 1280	500
Story2	B670	1952	2074; 2075	600	Story3	B868	1196	1281; 1282	600
Story2	B701	1979	2056; 2057	600	Story3	B869	1197	1283; 1284	600
Story2	B702	1980	2058; 2059	600	Story3	B870	1198	1285; 1286	600
Story2	B703	1981	2060; 2061	600	Story3	B871	1199	1287; 1288	600
Story2	B704	1982	2062; 2063	600	Story3	B872	1272	1262; 1263	600
Story2	B705	1983	2064; 2065	500	Story3	B873	1273	1264; 1265	600
Story2	B707	1984	2067; 2068	500	Story3	B874	1274	1266; 1267	600
Story2	B708	1985	2069; 2070	600	Story3	B875	1275	1268; 1269	600
Story2	B709	1986	2071; 2072	600	Story3	B876	1276	1270; 1271	500
Story2	B710	1987	2073; 2074	600	Story3	B877	1277	1272; 1273	500
Story2	B712	1988	2075; 2092	600	Story3	B878	1278	1274; 1275	700
Story2	B730	2004	2006; 2007	600	Story3	B879	1279	1276; 1277	800
Story2	B731	2005	2008; 2009	600	Story3	B880	1280	1278; 1279	500
Story2	B732	2006	2010; 2011	600	Story3	B881	1281	1280; 1281	600
Story2	B733	2007	2012; 2013	600	Story3	B882	1282	1282; 1283	600
Story2	B734	2008	2014; 2015	600	Story3	B883	1283	1284; 1285	600
Story2	B735	2009	2016; 2017	600	Story3	B884	1284	1286; 1287	600
Story2	B736	2010	2018; 2019	600	Story3	B885	1285	1288; 1391	600
Story2	B737	2011	2020; 2021	600	Story3	B886	1241	1392; 1366	600
Story2	B738	2012	2022; 2023	600	Story3	B887	1242	1393; 1367	500
Story2	B739	2013	2024; 2025	600	Story3	B888	1243	1394; 1368	600
Story2	B740	2014	2026; 2027	600	Story3	B889	1244	1395; 1369	600
Story2	B741	2015	2028; 2029	600	Story3	B890	1245	1396; 1370	600
Story2	B742	2016	2030; 2031	600	Story3	B891	1251	1366; 1393	500
Story2	B743	2017	2032; 2033	600	Story3	B892	1252	1367; 1394	600
Story2	B744	2018	2034; 2035	600	Story3	B893	1253	1368; 1395	600
Story2	B745	2019	2036; 2037	600	Story3	B894	1254	1369; 1396	600
Story2	B746	2020	2038; 2039	600	Story3	B895	1255	1370; 1385	600
Story2	B747	2021	2040; 2041	600	Story3	B896	1236	1397; 1361	600
Story2	B748	2022	2042; 2043	600	Story3	B897	1237	1398; 1362	600
Story2	B749	2023	2044; 2045	600	Story3	B898	1238	1399; 1363	600
Story2	B750	2024	2046; 2047	725	Story3	B899	1239	1400; 1364	600
Story2	B751	2025	2048; 2049	475	Story3	B900	1240	1401; 1365	600
Story2	B752	2026	2050; 2051	600	Story3	B901	1246	1361; 1398	600
Story2	B753	2027	2052; 2093	600	Story3	B902	1247	1362; 1399	600
Story2	B754	2028	2054; 2094	600	Story3	B903	1248	1363; 1400	600
Story2	B756	2029	2095; 2096	600	Story3	B904	1249	1364; 1401	600
Story2	B757	2030	2096; 2053	600	Story3	B905	1250	1365; 1402	500
Story2	B760	2032	1891; 2097	600	Story3	B906	1363	1350; 1403	600

Story2	B767	2039	1902; 1903	600	Story3	B908	1364	1403; 1404	700
Story2	B768	2040	1904; 1905	600	Story3	B910	1366	1404; 1406	600
Story2	B769	2041	1906; 1907	600	Story3	B911	1365	1406; 1405	600
Story2	B770	2042	1908; 1909	600	Story3	B914	1367	1407; 1351	600
Story2	B771	2043	1910; 1911	600	Story3	B915	1368	1405; 1407	800
Story2	B772	2044	1912; 1913	600	Story3	B8	1380	1402; 1417	600
Story2	B773	2045	1914; 1915	600	Story3	B148	1382	1418; 1419	600
Story2	B774	2046	1916; 1917	600	Story3	B152	1385	1417; 1418	700
Story2	B775	2047	1918; 1919	600	Story3	B154	1384	1419; 1420	600
Story2	B776	2048	1920; 1921	600	Story3	B4	1381	1486; 1392	500
Story2	B777	2049	1922; 1923	600	Story3	B5	1383	1420; 1486	900
Story2	B778	2051	1926; 1927	600	Story3	B44	1360	852; 1386	600
Story2	B779	2052	1928; 1929	600	Story3	B145	1256	429; 435	600
Story2	B780	2053	1930; 1931	600	Story3	B146	1257	436; 437	600
Story2	B781	2054	1932; 1933	600	Story3	B147	1258	438; 458	650
Story2	B782	2055	1934; 1935	600	Story3	B149	1259	458; 429	650
Story2	B783	2056	1936; 1937	600	Story3	B150	1260	435; 436	600
Story2	B784	2057	1938; 1939	600	Story3	B151	1261	437; 975	800

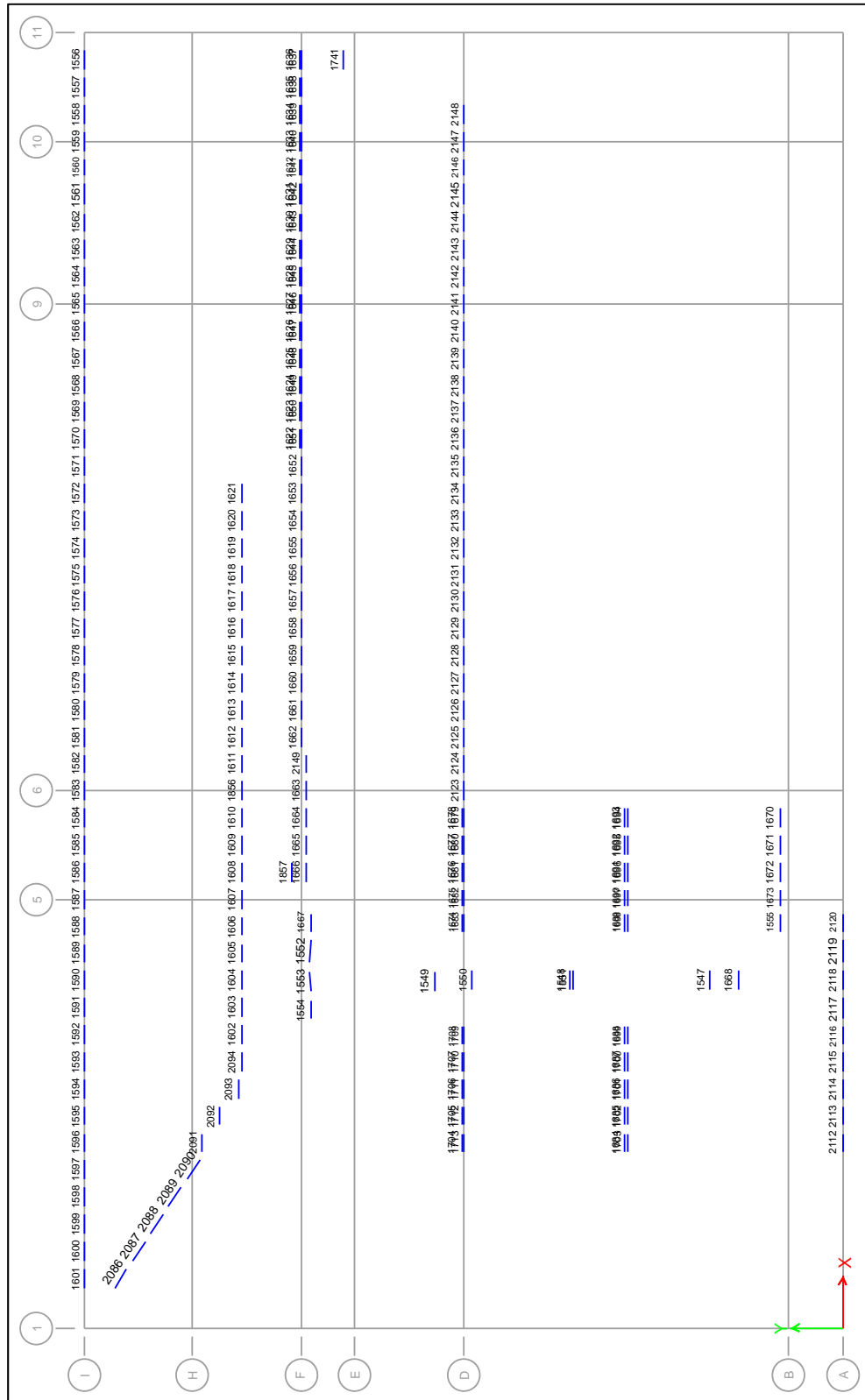
TABELL A 3 SKJÆRSTAVER

## 2.4 STRINGERELEMENTER

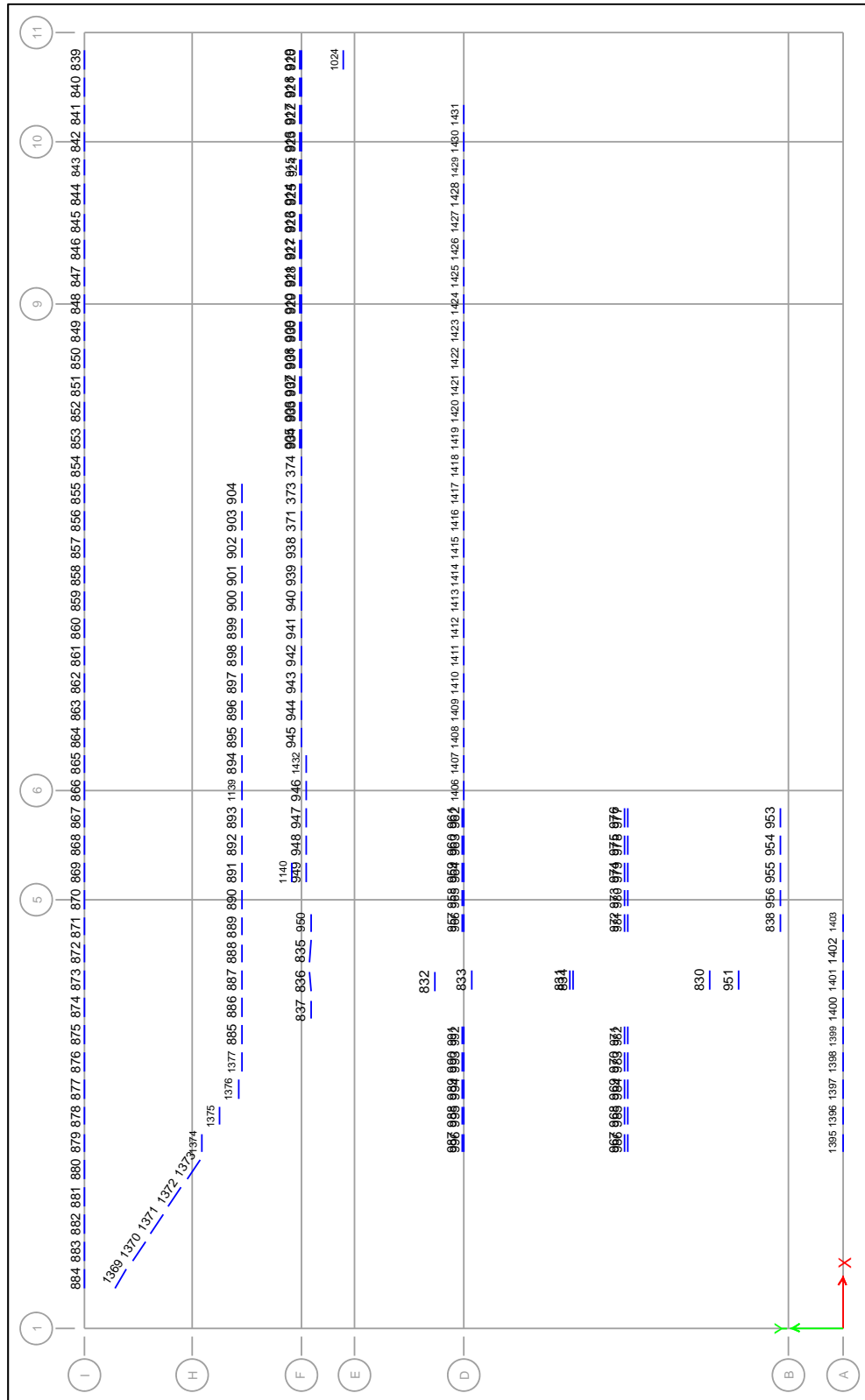
Tilsvarende skivearmoring i strekksituasjon og fugestøp i trykksituasjon



FIGUR A 8 STRINGERE: DEKKE OVER 1.ETG



FIGUR A 9 STRINGERE: DEKKE OVER 2.ETG



FIGUR A 10 STRINGERE: DEKKE OVER 3.ETG

TABLE: Beam Connectivity					TABLE: Beam Connectivity				
Story	Label	Unique Name	Points	Length	Story	Label	Unique Name	Points	Length
				mm					mm
Story1	B64	141	76; 78	1200	Story2	B267	1653	1794; 1793	1199.8
Story1	B108	144	104; 105	1200	Story2	B268	1654	1795; 1794	1200.2
Story1	B118	146	107; 108	1300	Story2	B269	1655	1796; 1795	1200
Story1	B122	148	181; 180	1200	Story2	B270	1656	1797; 1796	1200
Story1	B124	150	102; 197	1200	Story2	B271	1657	1798; 1797	1200
Story1	B125	151	204; 199	1400	Story2	B272	1658	1799; 1798	1200
Story1	B126	152	205; 204	1299.6	Story2	B273	1659	1800; 1799	1200
Story1	B127	153	206; 205	1200.2	Story2	B274	1660	1801; 1800	1200
Story1	B129	155	208; 209	1100	Story2	B275	1661	1802; 1801	1200
Story1	B130	159	215; 214	1200	Story2	B276	1662	1803; 1802	1200
Story1	B131	160	216; 215	1200	Story2	B278	1663	1805; 1804	1200
Story1	B132	161	217; 216	1200	Story2	B279	1664	1806; 1805	1200
Story1	B133	162	218; 217	1200	Story2	B280	1665	1807; 1806	1200
Story1	B134	163	219; 218	1075	Story2	B281	1666	1808; 1807	1200
Story1	B135	164	220; 219	1325	Story2	B283	1667	1686; 1809	1100.2
Story1	B139	166	223; 220	1200	Story2	B287	1668	1810; 1811	1200
Story1	B140	167	224; 223	1200	Story2	B290	1670	1815; 1814	1200
Story1	B141	168	225; 224	1200	Story2	B291	1671	1816; 1815	1200
Story1	B142	169	226; 225	1200	Story2	B292	1672	1817; 1816	1200
Story1	B143	170	227; 226	1200	Story2	B293	1673	1691; 1817	1100
Story1	B153	171	229; 227	1200	Story2	B295	1674	1818; 1819	1100
Story1	B165	172	231; 229	1200	Story2	B296	1675	1819; 1820	1100
Story1	B166	173	232; 231	1200	Story2	B297	1676	1820; 1821	1200
Story1	B167	174	233; 232	1200	Story2	B298	1677	1821; 1822	1200
Story1	B168	175	234; 233	1200	Story2	B299	1678	1822; 1823	1200
Story1	B173	176	235; 234	1200	Story2	B301	1679	1825; 1824	1200
Story1	B174	177	236; 235	1200	Story2	B302	1680	1826; 1825	1200
Story1	B175	178	246; 236	1200	Story2	B303	1681	1827; 1826	1200
Story1	B177	180	250; 246	1200	Story2	B304	1682	1828; 1827	1100
Story1	B178	181	251; 250	1200	Story2	B305	1683	1829; 1828	1100
Story1	B179	182	252; 251	1200	Story2	B306	1684	1830; 1831	1200
Story1	B180	183	253; 252	1200	Story2	B307	1685	1831; 1832	1200
Story1	B181	184	254; 253	1200	Story2	B308	1686	1832; 1833	1200
Story1	B182	185	255; 254	1200	Story2	B309	1687	1833; 1834	1200
Story1	B184	186	256; 255	1200	Story2	B310	1688	1834; 1835	1100
Story1	B185	187	257; 256	1200	Story2	B312	1689	1836; 1837	1100
Story1	B186	190	264; 257	1200	Story2	B313	1690	1837; 1838	1100
Story1	B187	191	265; 264	1200	Story2	B314	1691	1838; 1839	1200
Story1	B188	192	266; 265	1200	Story2	B315	1692	1839; 1840	1200
Story1	B189	193	267; 266	1200	Story2	B316	1693	1840; 1841	1200
Story1	B190	194	268; 267	1200	Story2	B317	1694	1843; 1842	1200
Story1	B191	195	269; 268	1200	Story2	B318	1695	1844; 1843	1200
Story1	B192	196	270; 269	1200	Story2	B319	1696	1845; 1844	1200
Story1	B193	197	271; 270	1200	Story2	B320	1697	1846; 1845	1100
Story1	B194	198	272; 271	1200	Story2	B321	1698	1847; 1846	1100



Story1	B195	199	273; 272	1200	Story2	B323	1699	1849; 1848	1100
Story1	B196	200	274; 273	1200	Story2	B324	1700	1850; 1849	1200
Story1	B197	201	275; 274	1200	Story2	B325	1701	1851; 1850	1200
Story1	B198	202	276; 275	1200	Story2	B326	1702	1852; 1851	1200
Story1	B199	203	277; 276	1200	Story2	B327	1703	2148; 1852	1200
Story1	B200	204	278; 277	1200	Story2	B329	1704	1853; 1854	1200
Story1	B201	205	279; 278	1200	Story2	B330	1705	1854; 1855	1200
Story1	B202	206	280; 279	1200	Story2	B331	1706	1855; 1856	1200
Story1	B203	207	281; 280	1200	Story2	B332	1707	1856; 1857	1200
Story1	B204	208	282; 281	1200	Story2	B333	1708	1857; 1858	1100
Story1	B213	531	514; 294	1200	Story2	B334	1709	1860; 1859	1100
Story1	B214	218	294; 295	1200	Story2	B335	1710	1861; 1860	1200
Story1	B215	219	295; 296	1200	Story2	B336	1711	1862; 1861	1200
Story1	B216	220	296; 297	1200	Story2	B337	1712	1863; 1862	1200
Story1	B217	221	297; 298	1200	Story2	B338	1713	1864; 1863	1200
Story1	B218	222	298; 299	1200	Story2	B413	1741	1865; 1866	1200
Story1	B219	224	299; 300	1200	Story2	B65	1856	1748; 1749	1200
Story1	B220	225	300; 301	1200	Story2	B183	1857	1888; 1887	1200
Story1	B221	226	301; 302	1200	Story2	B921	2091	1523; 2128	1200
Story1	B222	227	302; 303	1200	Story2	B922	2092	1524; 2129	1200
Story1	B224	229	304; 305	1200	Story2	B923	2093	1525; 2130	1200
Story1	B225	230	305; 306	1200	Story2	B547	2112	2136; 2137	1200.3
Story1	B226	231	306; 307	1200	Story2	B548	2113	2137; 2138	1199.9
Story1	B227	232	307; 308	1200	Story2	B549	2114	2138; 2139	1199.9
Story1	B228	233	308; 309	1200	Story2	B553	2115	2139; 2140	1199.9
Story1	B229	234	309; 310	1200	Story2	B557	2116	2140; 2141	1100
Story1	B230	235	310; 311	1200	Story2	B566	2117	2141; 2142	1300
Story1	B231	236	311; 312	1200	Story2	B570	2118	2142; 2143	1200
Story1	B232	237	312; 313	1200	Story2	B571	2119	2143; 2144	1400
Story1	B233	238	313; 314	1200	Story2	B572	2120	2144; 2145	1100
Story1	B234	239	314; 315	1200	Story2	B608	2123	1824; 2150	1200
Story1	B235	240	316; 317	1200	Story2	B609	2124	2150; 2151	1200
Story1	B236	241	317; 318	1200	Story2	B610	2125	2151; 2152	1200
Story1	B237	242	318; 319	1200	Story2	B611	2126	2152; 2153	1200
Story1	B239	244	319; 321	1200	Story2	B612	2127	2153; 2154	1200
Story1	B240	245	321; 322	1200	Story2	B614	2128	2154; 2155	1200
Story1	B241	246	322; 323	1200	Story2	B615	2129	2155; 2156	1200
Story1	B242	247	323; 324	1200	Story2	B616	2130	2156; 2157	1200
Story1	B243	248	324; 325	1200	Story2	B617	2131	2157; 2158	1200
Story1	B244	249	325; 326	1200	Story2	B618	2132	2158; 2159	1200
Story1	B245	250	326; 327	1325	Story2	B619	2133	2159; 2160	1200
Story1	B246	251	327; 328	1075	Story2	B620	2134	2160; 2161	1200
Story1	B247	252	328; 329	1200	Story2	B621	2135	2161; 2162	1200
Story1	B248	253	329; 330	1200	Story2	B622	2136	2162; 2163	1200
Story1	B249	254	330; 331	1200	Story2	B623	2137	2163; 2164	1200
Story1	B250	255	331; 332	1200	Story2	B624	2138	2164; 2165	1200
Story1	B251	256	334; 333	1200	Story2	B625	2139	2165; 2166	1200
Story1	B252	257	335; 334	1200	Story2	B626	2140	2166; 2167	1200

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Story1	B254	259	337; 336	1200	Story2	B628	2142	2168; 2169	1200
Story1	B255	260	338; 337	1075	Story2	B630	2143	2169; 2170	1200
Story1	B256	261	339; 338	1325	Story2	B643	2144	2170; 2171	1200
Story1	B257	262	340; 339	1200	Story2	B663	2145	2171; 2172	1325
Story1	B258	263	341; 340	1200	Story2	B664	2146	2172; 2173	1075
Story1	B259	264	342; 341	1200	Story2	B665	2147	2173; 2174	1200
Story1	B260	265	343; 342	1200	Story2	B671	2148	2174; 2175	1200
Story1	B261	266	344; 343	1200	Story2	B6	2149	1804; 2202	1200
Story1	B262	267	345; 344	1200	Story2	B1	2086	1645; 1643	1443
Story1	B263	268	346; 345	1200	Story2	B57	2087	1643; 1641	1443
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Story1	B313	313	397; 398	1100	Story3	B186	866	1005; 1004	1200
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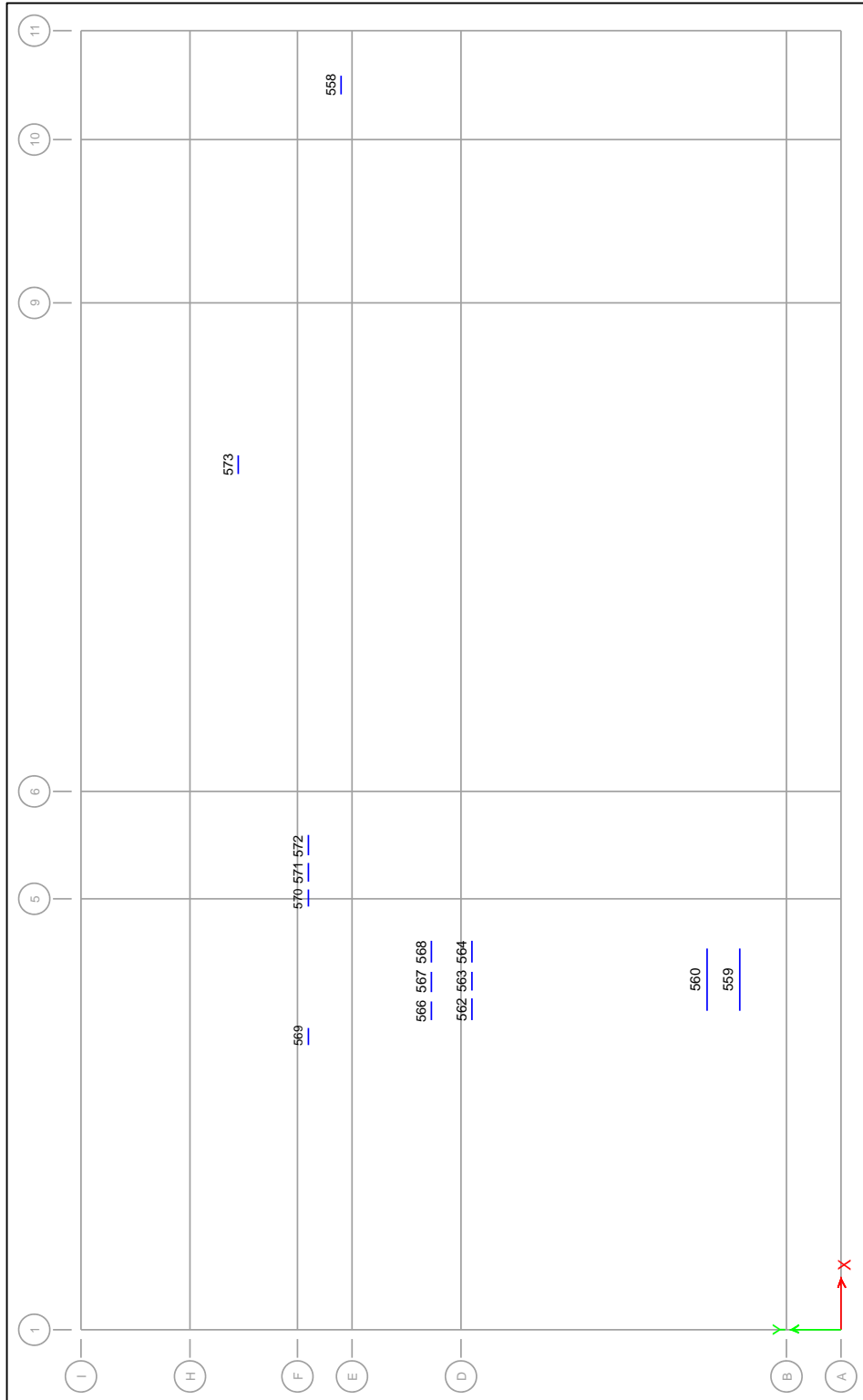
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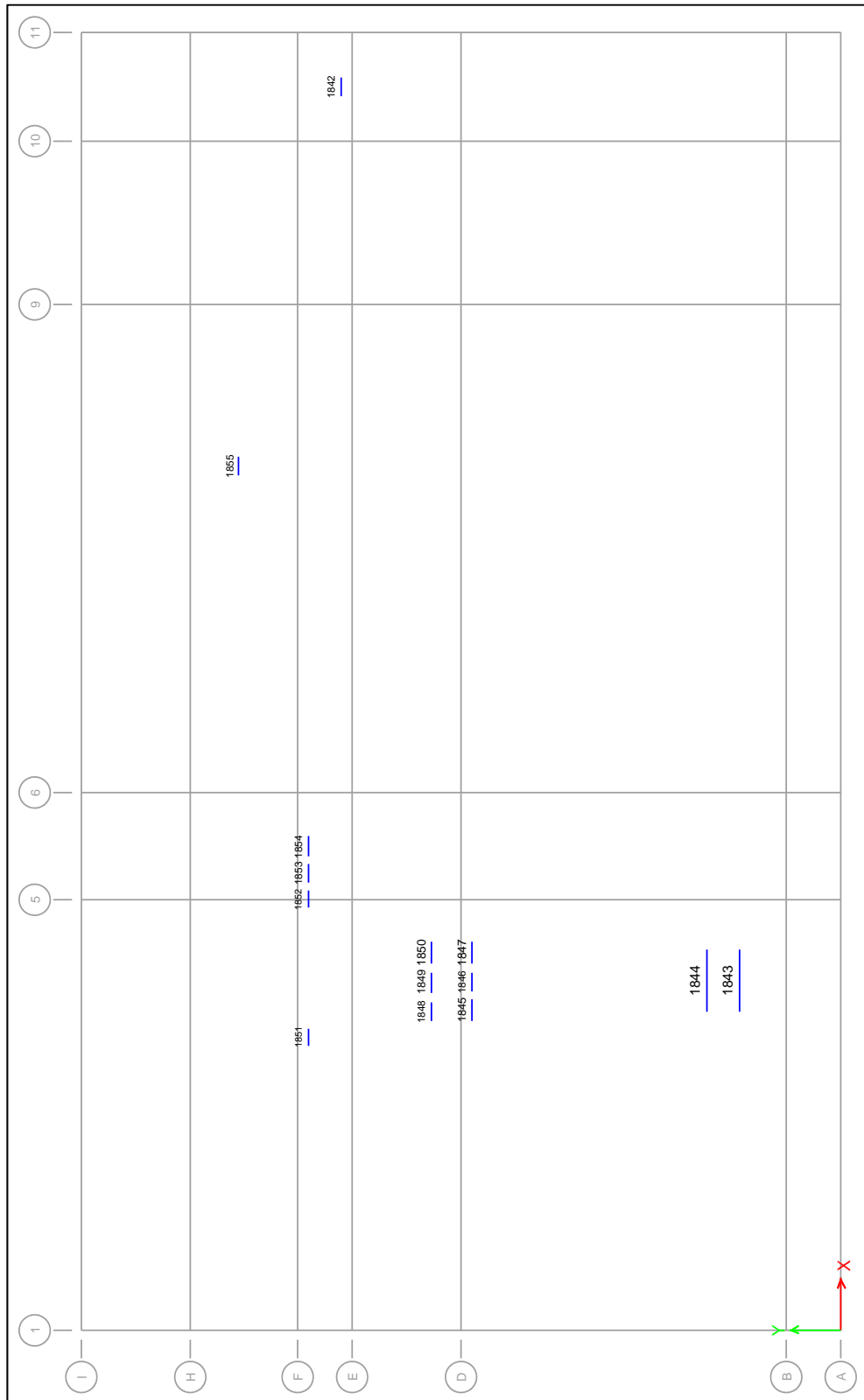
## 2.5 STREKKSTÅL VED DISKONTINUITET I ARMERING

Strekkforbindelsene som opptar kreftene der hvor armeringen ikke kan føres, tilordnes egne elementer i ETABS-modellen.

Stålkvalitet S355J0 og tverrsnitt 8x100mm som et utgangspunkt.

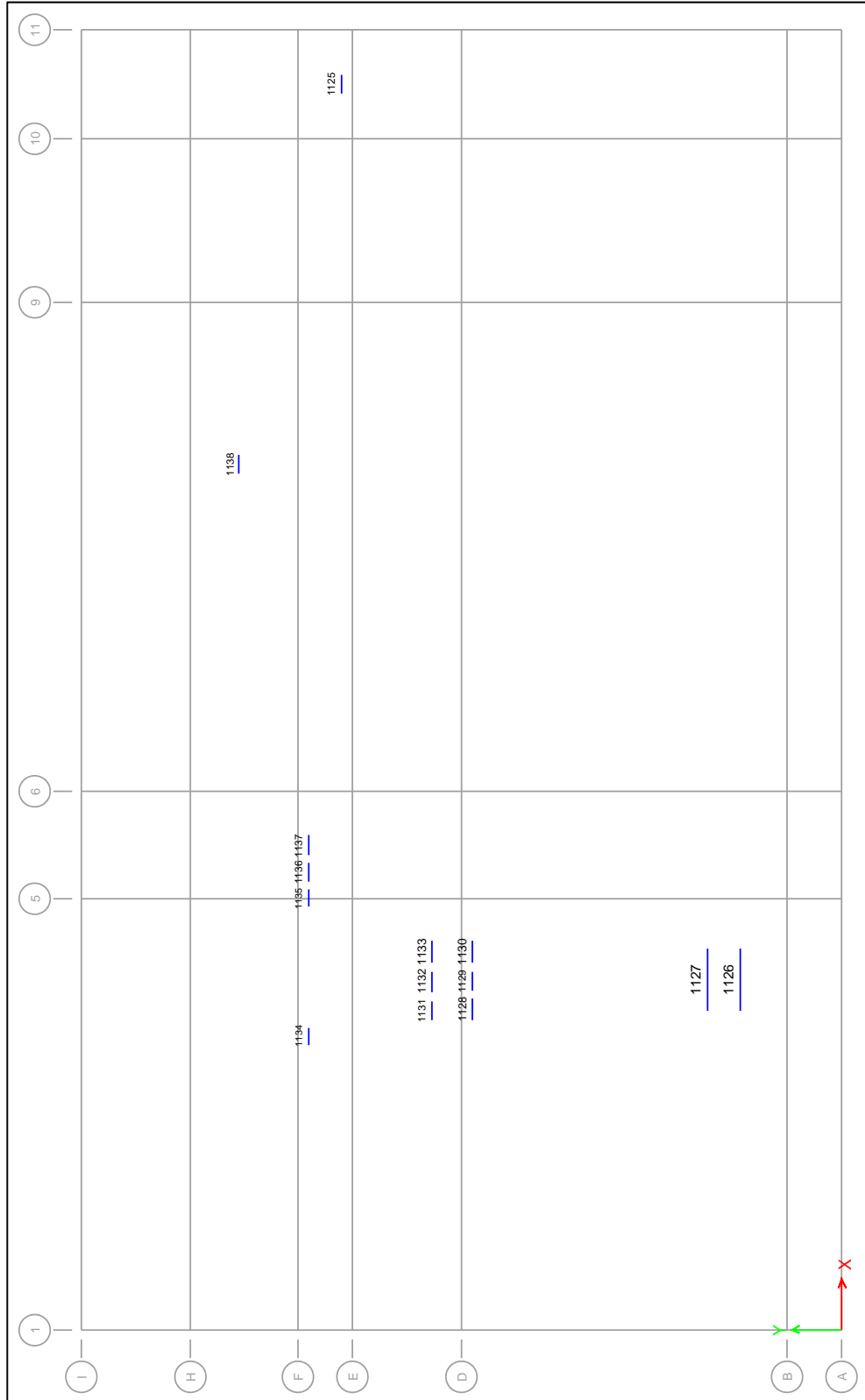


FIGUR A 11 STREKKSTÅL: DEKKE OVER 1.ETG



FIGUR A 12 STREKKSTÅL: DEKKE OVER 2.ETG





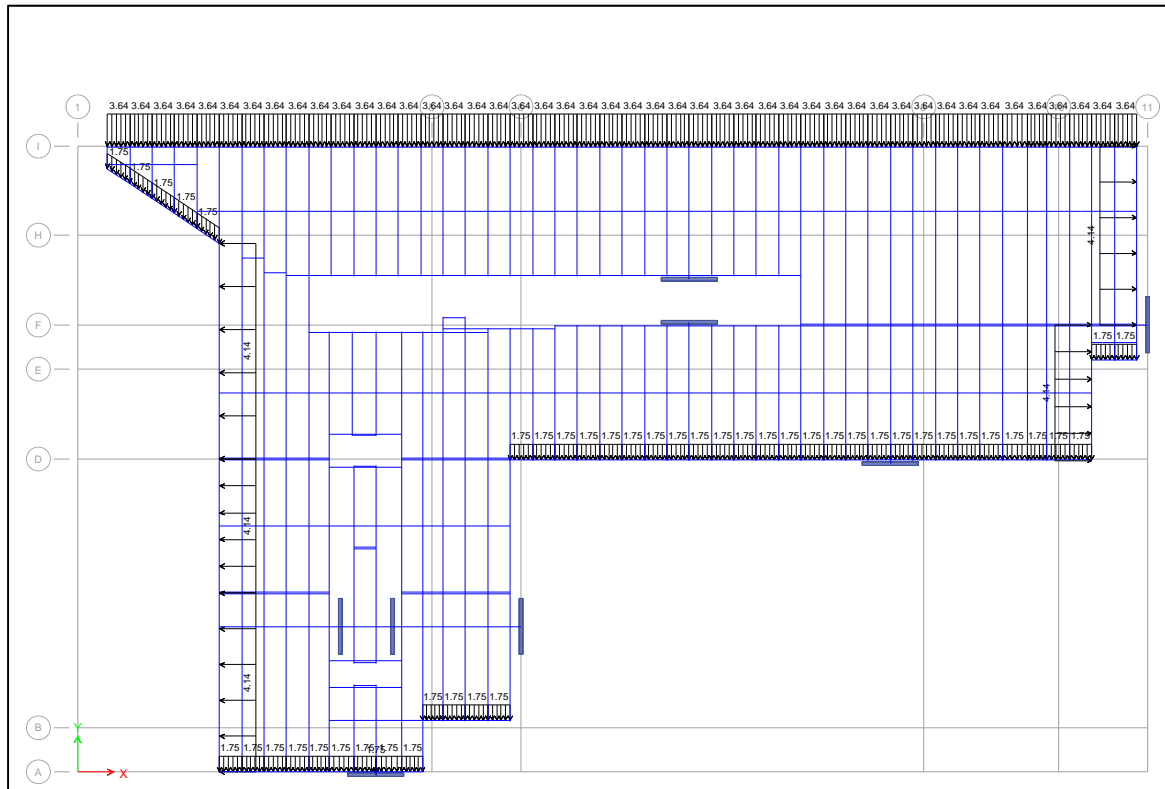
FIGUR A 13 STREKKSTÅL: DEKKE OVER 3.ETG

TABLE: Beam Connectivity					TABLE: Beam Connectivity				
Story	Label	Unique Name	Points	Length	Story	Label	Unique Name	Points	Length
				mm					mm
Story1	B555	559	480; 481	3900	Story2	B564	1850	1879; 1880	1400
Story1	B556	560	483; 482	3900	Story2	B567	1853	1882; 1883	1200
Story1	B558	562	485; 486	1300	Story2	B568	1854	1883; 1884	1200
Story1	B559	563	486; 487	1200	Story2	B144	1852	1809; 1882	1100
Story1	B560	564	487; 488	1400	Story2	B123	1842	182; 1865	1200
Story1	B562	566	490; 491	1200	Story2	B128	1855	1760; 283	1200
Story1	B563	567	491; 492	1300	Story2	B136	1851	382; 1689	1100
Story1	B564	568	492; 493	1400	Story3	B555	1126	1154; 1155	3900
Story1	B567	571	495; 496	1200	Story3	B556	1127	1157; 1156	3900
Story1	B568	572	496; 497	1200	Story3	B558	1128	1158; 1159	1300
Story1	B144	570	369; 495	1100	Story3	B559	1129	1159; 1160	1200
Story1	B123	558	5; 103	1200	Story3	B560	1130	1160; 1161	1400
Story1	B128	573	315; 228	1200	Story3	B562	1131	1162; 1163	1200
Story1	B136	569	284; 206	1100	Story3	B563	1132	1163; 1164	1300
Story2	B555	1843	1869; 1870	3900	Story3	B564	1133	1164; 1165	1400
Story2	B556	1844	1872; 1871	3900	Story3	B567	1136	1167; 1168	1200
Story2	B558	1845	1873; 1874	1300	Story3	B568	1137	1168; 1169	1200
Story2	B559	1846	1874; 1875	1200	Story3	B144	1135	1094; 1167	1100
Story2	B560	1847	1875; 1876	1400	Story3	B123	1125	141; 1150	1200
Story2	B562	1848	1877; 1878	1200	Story3	B128	1138	1045; 248	1200
Story2	B563	1849	1878; 1879	1300	Story3	B136	1134	368; 974	1100

TABELL A 5 STREKKSTÅLSTAVER

### 3 HORIZONTALA LASTER

Det kjøres én lastkombinasjon: Vindlast i negativ Y-retning. Lastsituasjonen er den samme i alle etasjer:



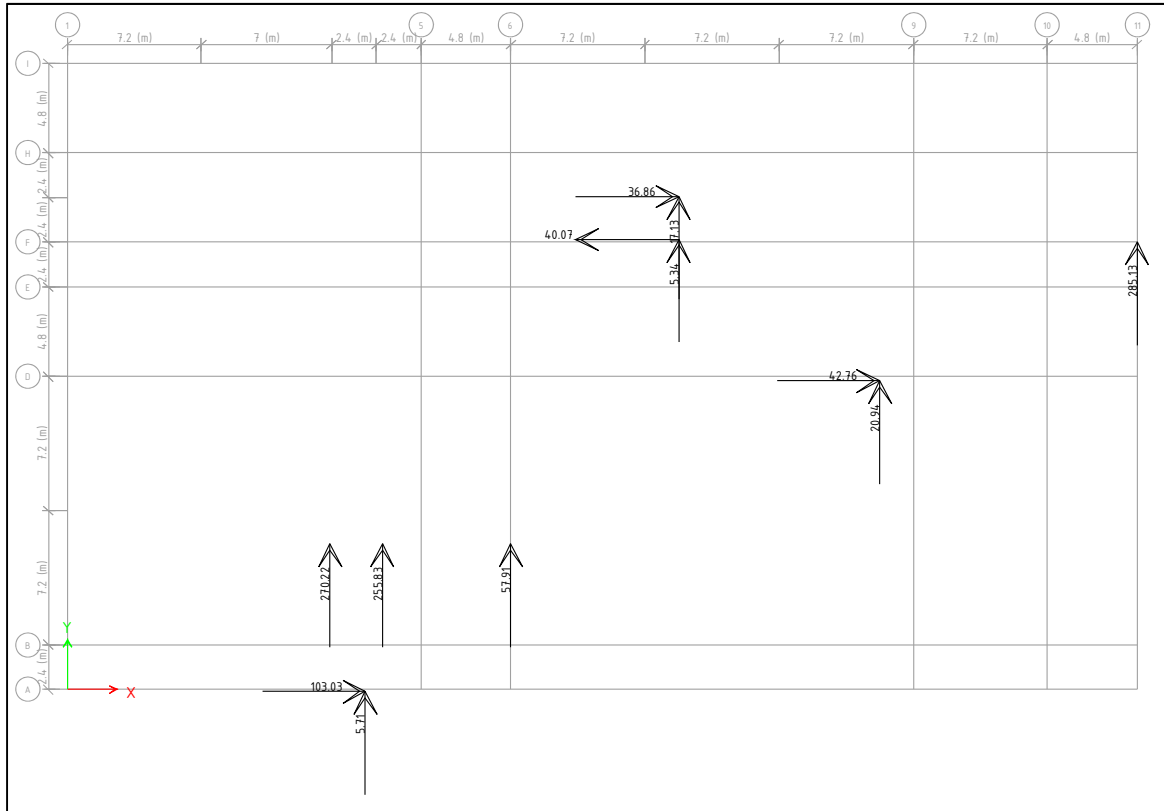
FIGUR A 14 HORIZONTALA LASTER: DEKKE OVER 1.-3.ETG

### 4 ANALYSERESULTATER

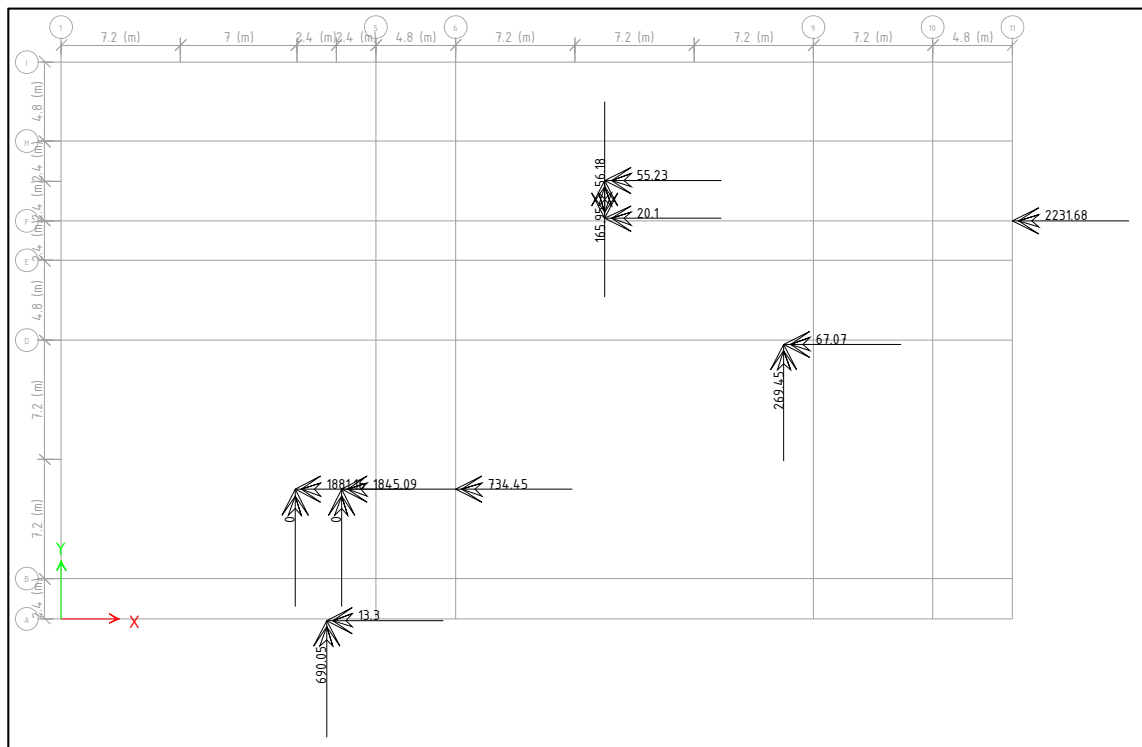
Analyseresultatene presenteres grafisk som vist på skjermen i ETABS. I tillegg vises tabelloversikter over krefter og kraftvirkninger.

Etter som at alle elementene er modellert som staver skal det la seg gjøre å lese kreftene som virker på hver stav direkte ut fra skjermbildet/tabellen.

### 4.1 OPPLAGERREAKSJONER I SKJÆRVEGGENE



FIGUR A 15 KREFTER PÅ SKJÆRVEGGER MOT FUNDAMENT

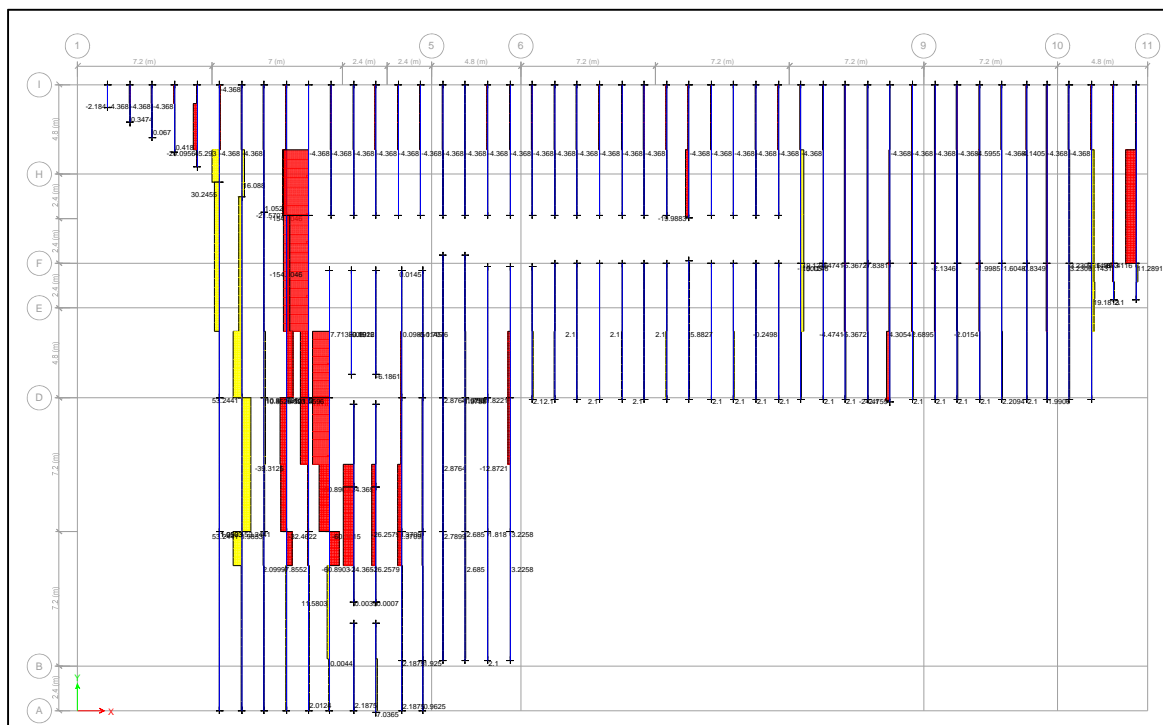


FIGUR A 16 MOMENTER PÅ SKJÆRVEGGER MOT FUNDAMENT

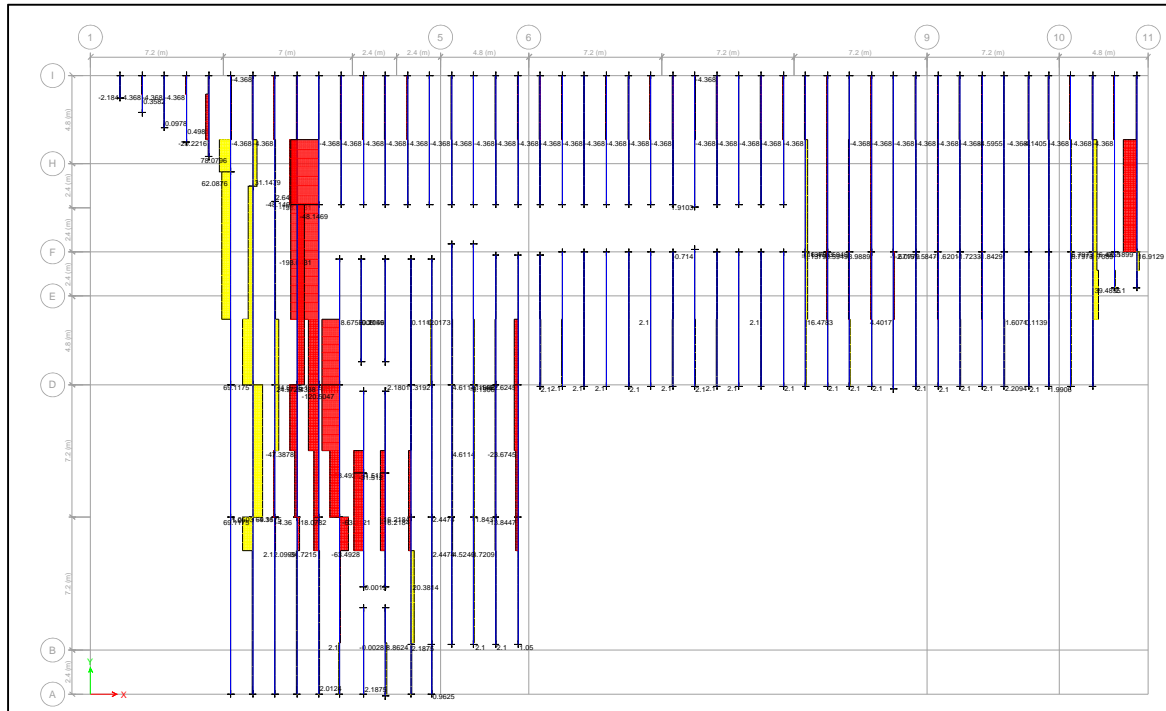
TABLE: Joint Reactions								
Story	Joint Label	Load Case/	FX	FY	FZ	MX	MY	MZ
			kN	kN	kN	kN-m	kN-m	kN-m
Base	499	Vind-y	0	57.908	0	-734.4487	0	-34.7448
Base	182	Vind-y	0	270.2191	0	-1881.1641	0	-3.2722
Base	7	Vind-y	0	255.828	0	-1845.0906	0	-5.7996
Base	10	Vind-y	36.8584	17.1329	0	-55.2305	165.9528	-3.6858
Base	12	Vind-y	-40.0736	5.3436	0	-20.0998	-56.181	-4.0074
Base	13	Vind-y	103.0273	5.7085	0	-13.3045	690.0503	-10.3027
Base	15	Vind-y	42.7581	20.9407	0	-67.073	269.4542	-4.2758
Base	11	Vind-y	0	285.1315	0	-2231.682	0	-

TABELL A 6 SKJÆRVEGGER KRAFTOVERFØRINGER MOT FUNDAMENT

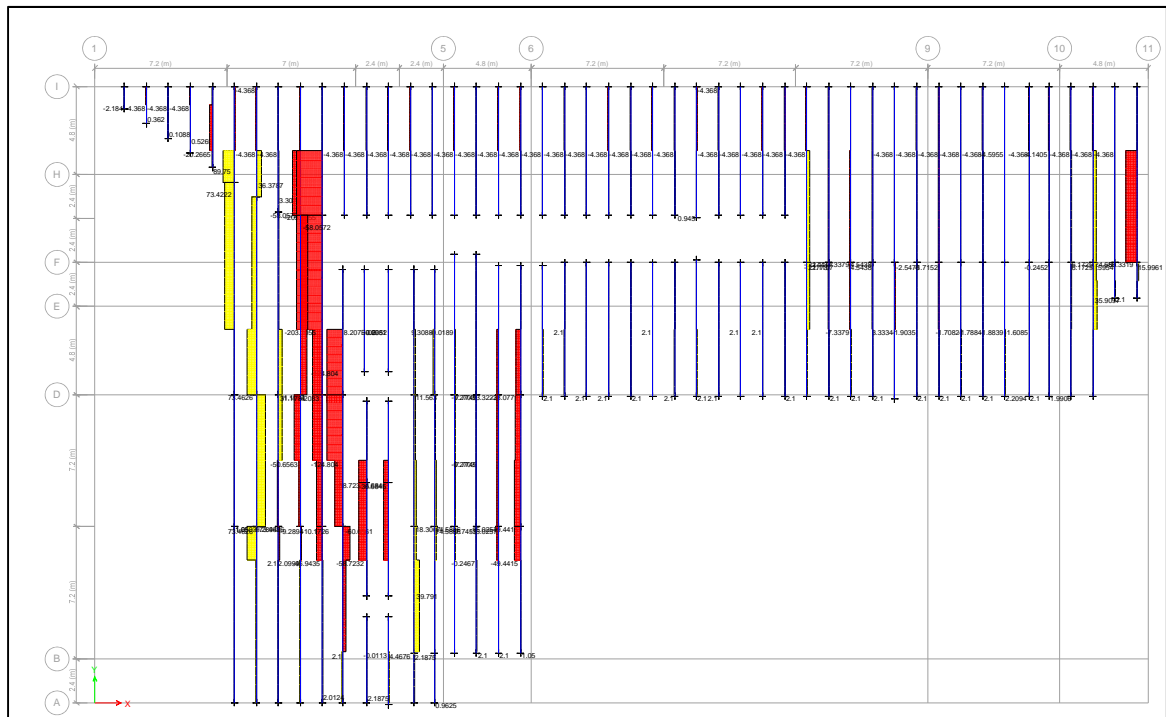
## 4.2 AKSIALKREFTER I HD-STAVER



FIGUR A 17 AKSIALKREFTER I HD-STAVER: DEKKE OVER 1.ETG

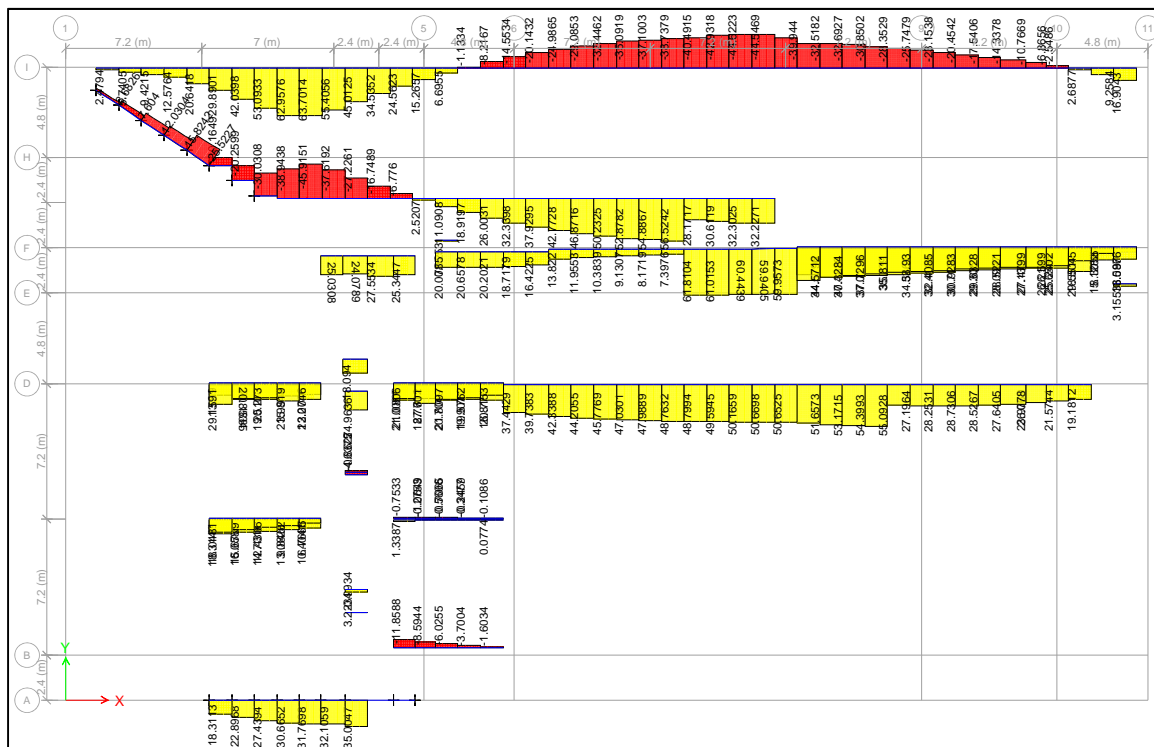


FIGUR A 18 AKSIALKREFTER I HD-STAVER: DEKKE OVER 2.ETG

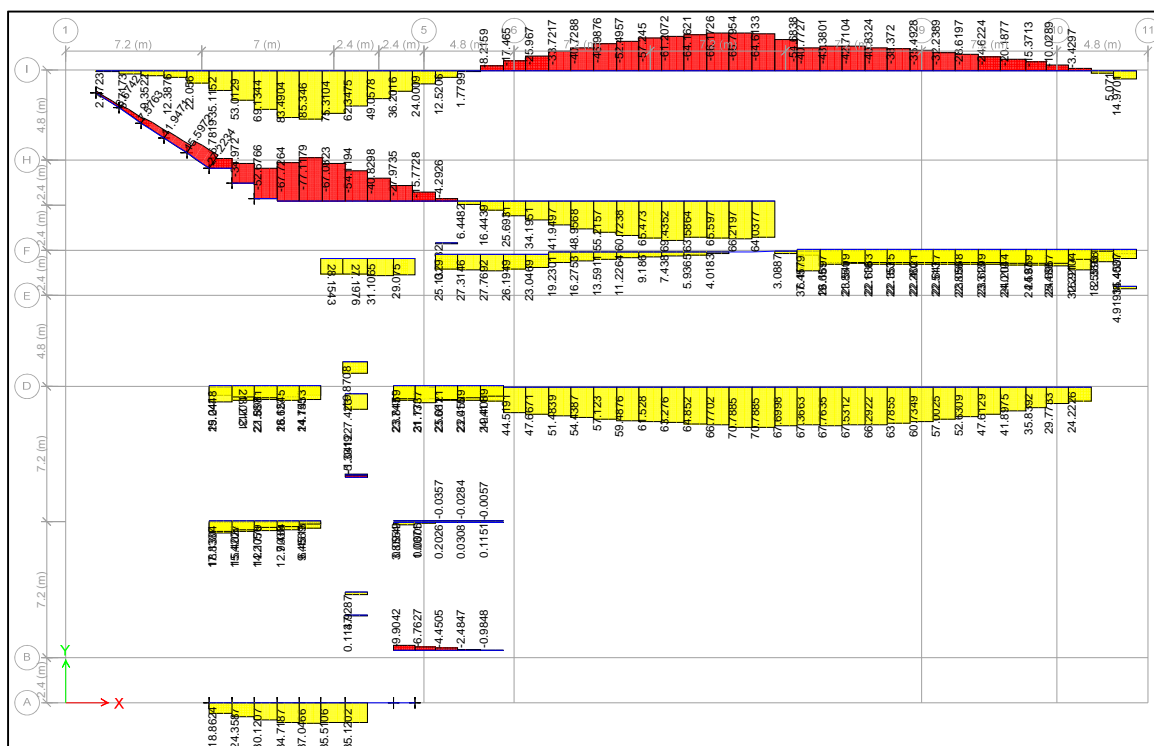


FIGUR A 19 AKSIALKREFTER I HD-STAVER: DEKKE OVER 3.ETG

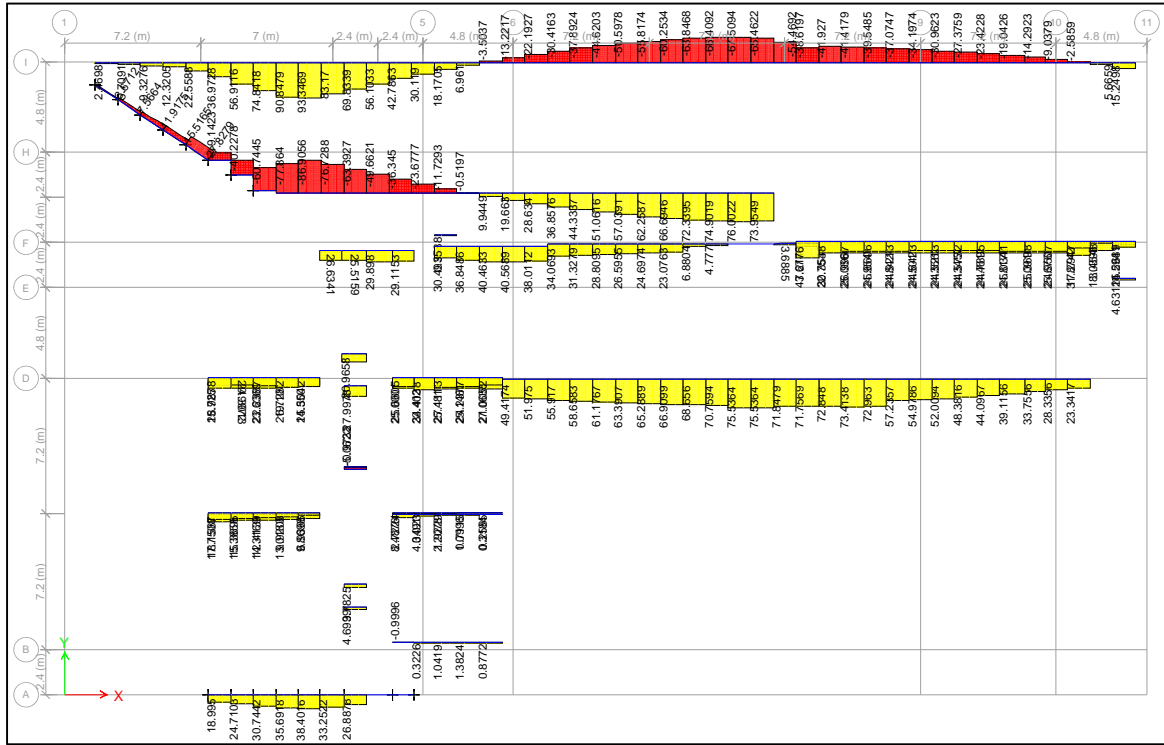
### 4.3 AKSIALKRAFT I STRINGERE



FIGUR A 20 AKSIALKREFTER I STRINGERE: DEKE OVER 1.ETG

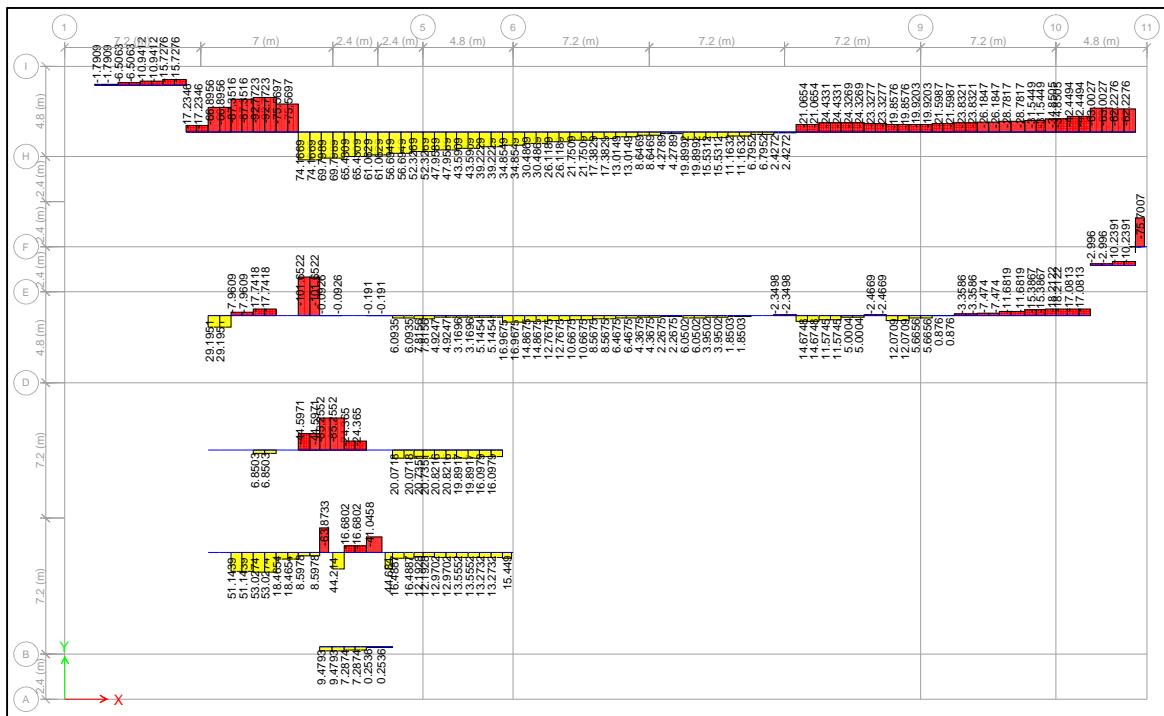


FIGUR A 21 AKSIALKREFTER I STRINGERE: DEKE OVER 2.ETG



FIGUR A 22 AKSIALKREFTER I STRINGERE: DEKKE OVER 3.ETG

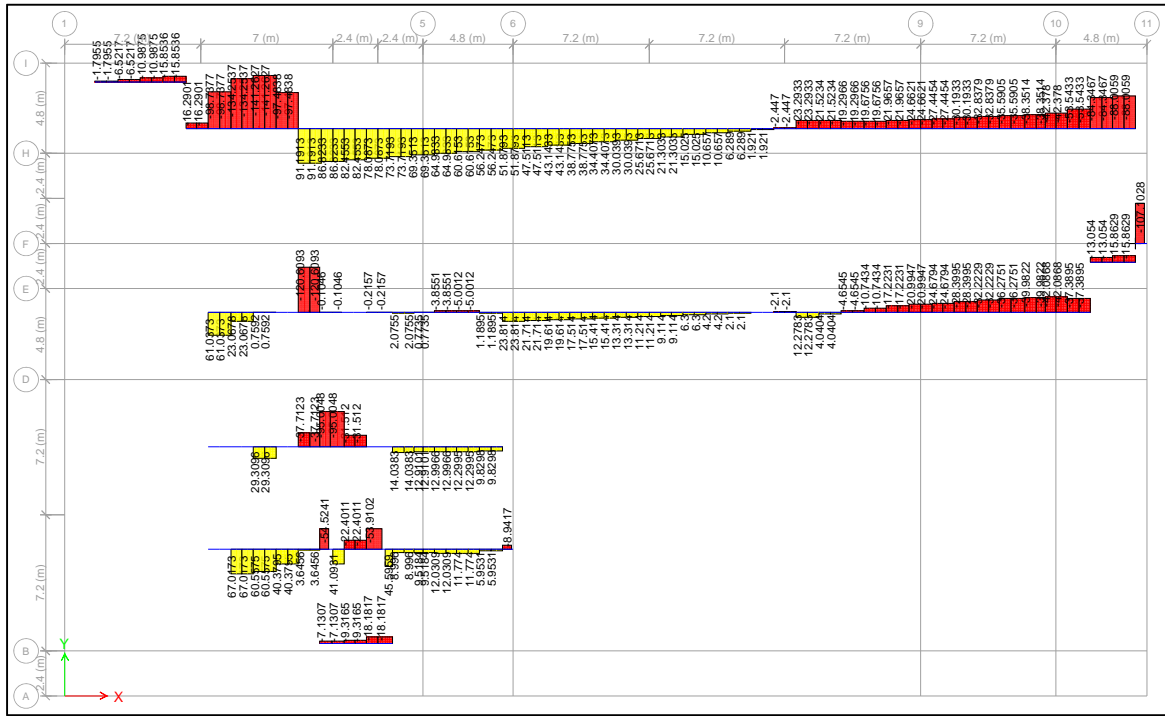
#### 4.4 SKJÆRKRAFT I SKJÆRSTAVER



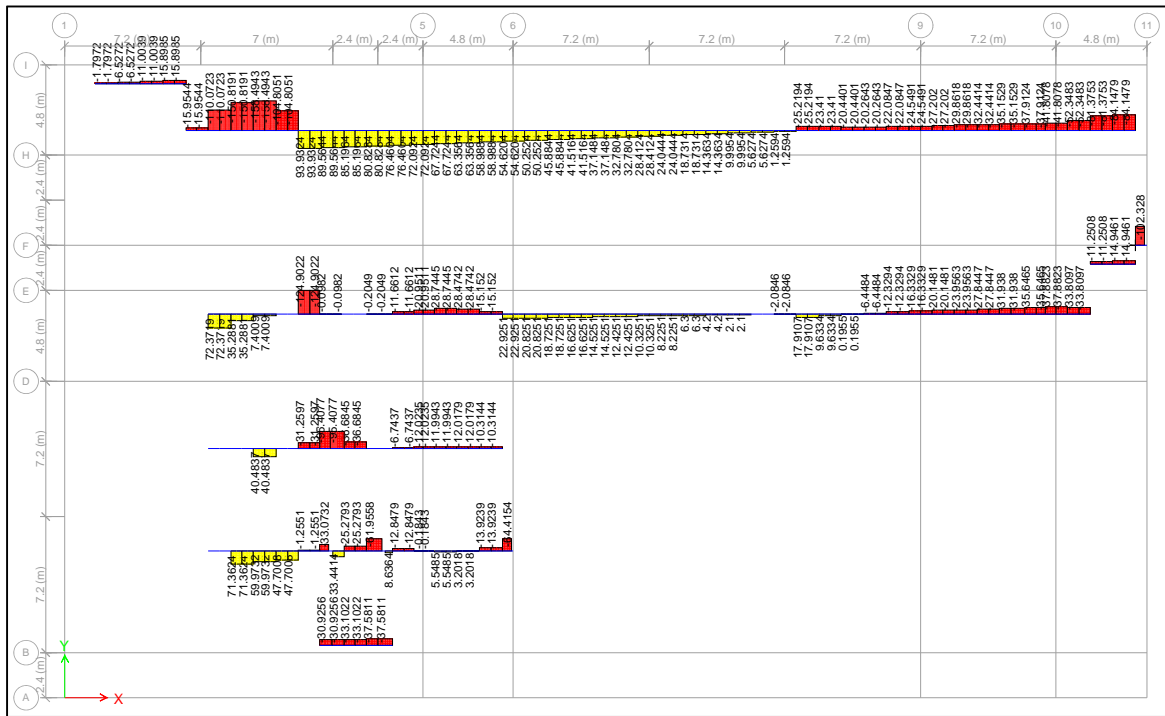
FIGUR A 23 SKJÆRKRAFT I SKJÆRSTAVER: DEKKE OVER 1.ETG



Tillegg A-40 | ETABS-resultater for SYSCO

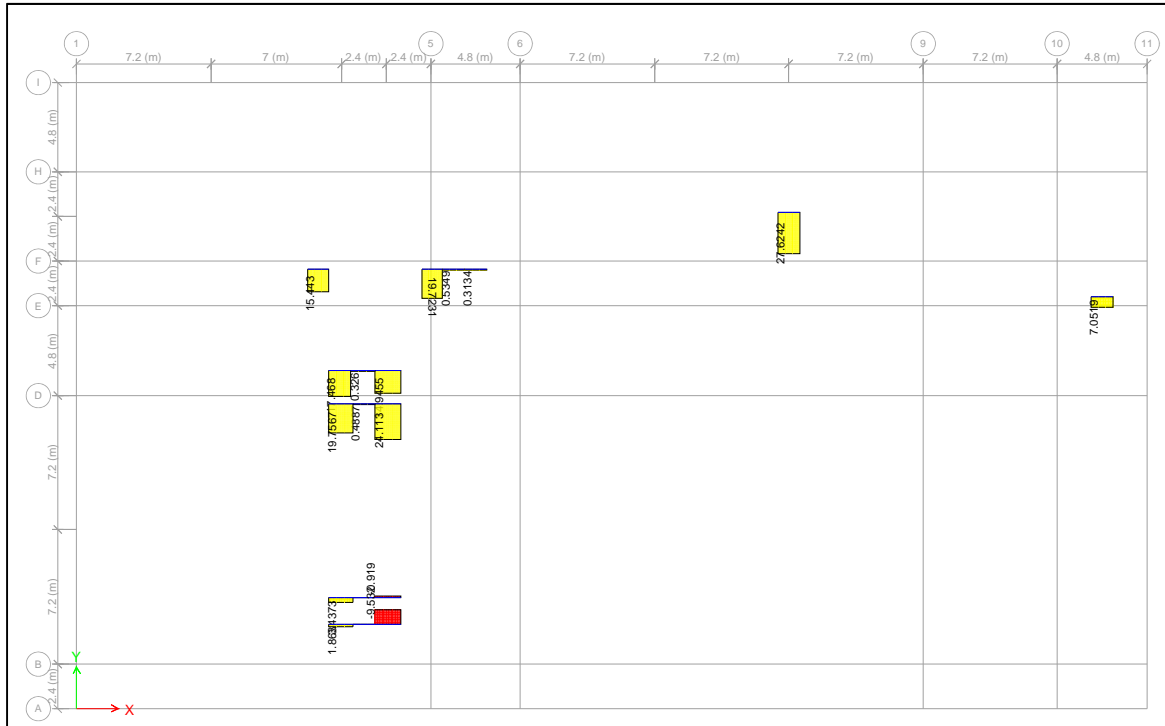


FIGUR A 24 SKJÆRKRAFT I SKJÆRSTAVER: DEKKE OVER 2.ETG

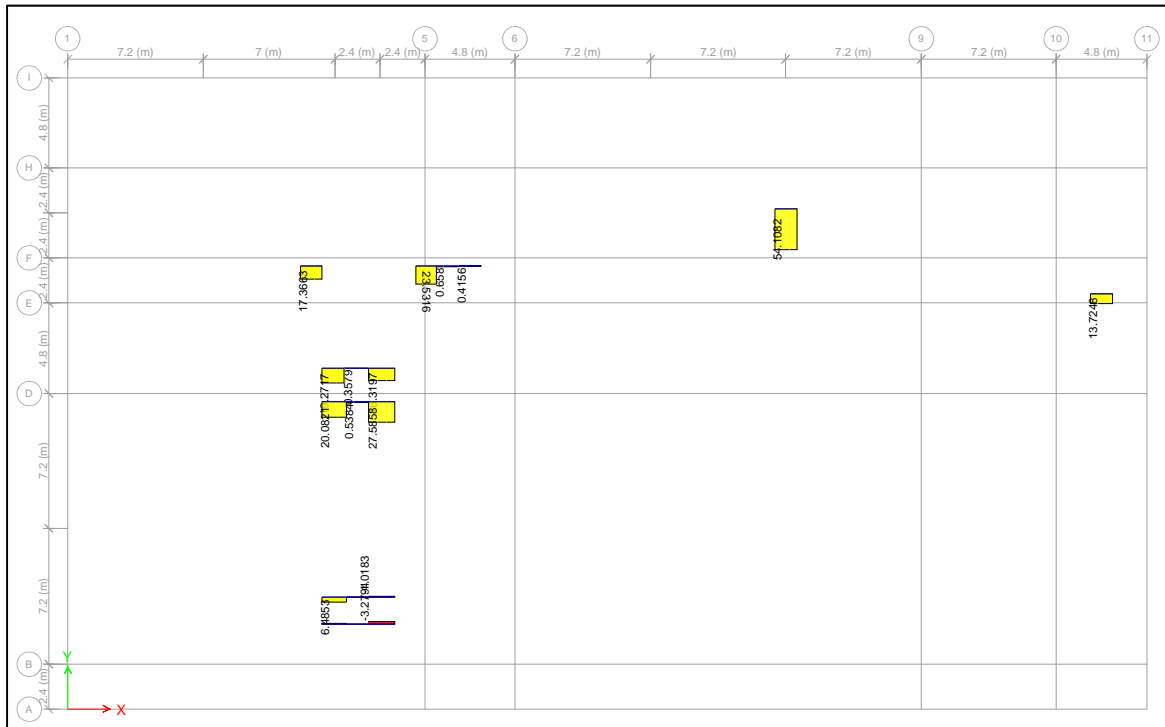


FIGUR A 25 SKJÆRKRAFT I SKJÆRSTAVER: DEKKE OVER 3.ETG

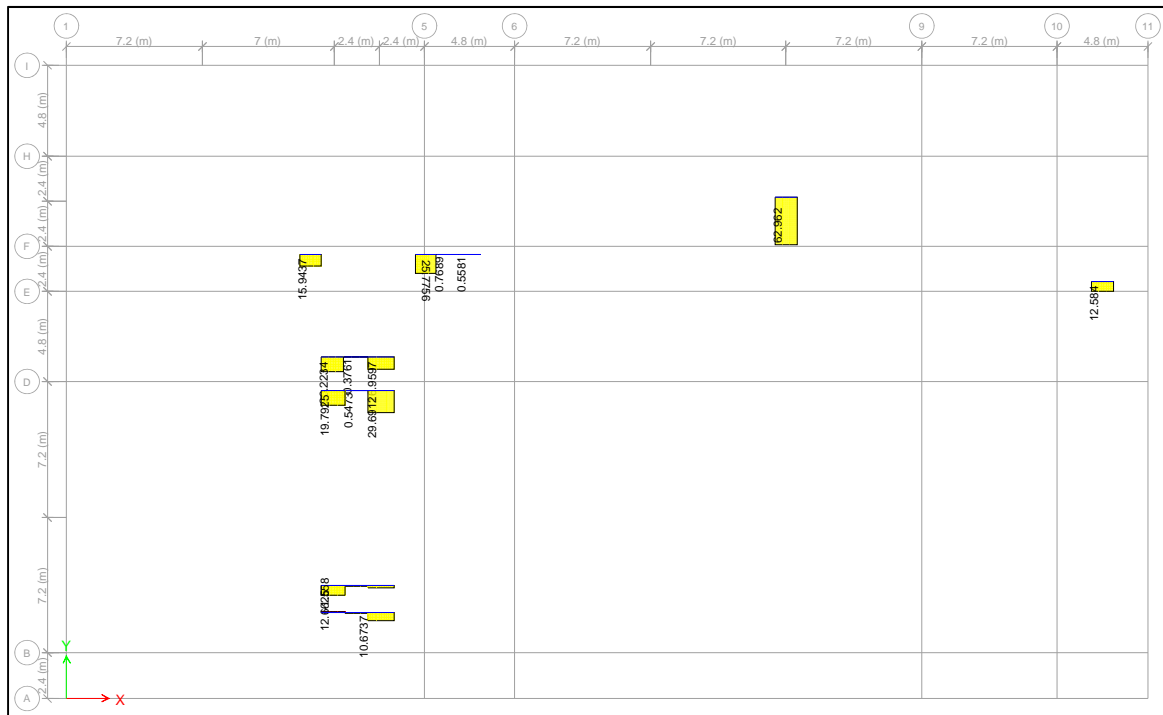
### 4.5 KRAFT I STREKKFORBINDELSER



FIGUR A 26 KRAFT I STREKKFORBINDELSER: DEKKE OVER 1.ETG



FIGUR A 27 KRAFT I STREKKFORBINDELSER: DEKKE OVER 2.ETG



FIGUR A 28 KRAFT I STREKKFORBINDELSER: DEKKE OVER 3.ETG

#### 4.6 HORIZONTALSKIVEELEMENTER: TABELL

Under dette punktet samles alle kraftvirkninger som påvirker elementene i hulldekkeskiven. Av hensyn til datamengdene er de representert med resultatene fra dekke over 1.etg. Dette kan forsvares med at etasjene er såpass likt utformet og med identisk last at resultatene vil få svært lite avvik etasjevis.

TABLE: Beam Forces, Story 1 for load case Vind-v					TABLE: Beam Forces, Story 1 for load case Vind-v					TABLE: Beam Forces, Story 1 for load case Vind-v					TABLE: Beam Forces, Story 1 for load case Vind-v				
Beam	Station	P	V3	M2	Beam	Station	P	V3	M2	Beam	Station	P	V3	M2	Beam	Station	P	V3	M2
	m	kN	kN	kN-m		m	kN	kN	kN-m		m	kN	kN	kN-m		m	kN	kN	kN-m
B11	0.0	2.2	0.0	0.0	B88	3.5	-4.4	-2.4	-8.4	B173	0.0	-44.3	2.2	0.0	B747	0.0	0.0	0.6	-2.9
B11	0.1	2.2	0.0	0.0	B88	7.0	-4.4	-2.4	0.0	B173	1.2	-44.3	-2.2	0.0	B747	0.6	0.0	0.6	-3.3
B11	0.1	9.4	9.1	45.2	B88	7.0	0.0	0.0	0.0	B174	0.0	-44.4	2.2	0.0	B748	0.0	0.0	-3.6	-3.0
B11	1.8	9.4	9.1	29.1	B88	7.0	0.0	0.0	0.0	B174	1.2	-44.4	-2.2	0.0	B748	0.6	0.0	-3.6	-0.8
B11	1.8	9.4	4.2	29.1	B90	0.0	0.0	0.0	0.0	B175	0.0	-42.7	2.2	0.0	B749	0.0	0.0	-7.7	-3.0
B11	3.3	9.4	4.2	23.1	B90	0.1	0.0	0.0	0.0	B175	1.2	-42.7	-2.2	0.0	B749	0.6	0.0	-7.7	1.7
B11	3.3	9.4	3.5	23.1	B90	0.1	0.0	-1.6	0.0	B177	0.0	-40.3	2.2	0.0	B750	0.0	0.0	-11.9	-2.8
B11	5.1	9.4	3.5	16.7	B90	3.5	0.0	-1.6	5.6	B177	1.2	-40.3	-2.2	0.0	B750	0.7	0.0	-11.9	5.8
B11	5.1	-27.8	3.5	6.1	B90	3.5	-4.4	-1.6	-5.6	B178	0.0	-38.6	2.2	0.0	B751	0.0	0.0	-15.6	-0.4
B11	6.8	-27.8	3.5	0.1	B90	7.0	-4.4	-1.6	0.0	B178	1.2	-38.6	-2.2	0.0	B751	0.5	0.0	-15.6	7.0
B11	6.8	-27.8	1.4	0.1	B90	7.0	0.0	0.0	0.0	B179	0.0	-37.0	2.2	0.0	B752	0.0	0.0	-18.5	0.4
B11	6.9	-27.8	1.4	0.0	B90	7.0	0.0	0.0	0.0	B179	1.2	-37.0	-2.2	0.0	B752	0.6	0.0	-18.5	11.5
B12	0.0	1.0	0.0	0.0	B91	0.0	0.0	0.0	0.0	B180	0.0	-35.0	2.2	0.0	B753	0.0	0.0	-17.3	4.5
B12	0.1	1.0	0.0	0.0	B91	0.1	0.0	0.0	0.0	B180	1.2	-35.0	-2.2	0.0	B753	0.6	0.0	-17.3	14.8

B12	0.1	1.9	-2.8	0.0	B91	0.1	0.0	-2.0	0.0	B181	0.0	-32.3	2.2	0.0	B754	0.0	0.0	-10.3	0.0
B12	5.1	1.9	-2.8	14.2	B91	3.5	0.0	-2.0	6.9	B181	1.2	-32.3	-2.2	0.0	B754	0.6	0.0	-10.3	6.2
B12	5.1	-1.7	-2.8	-5.0	B91	3.5	-4.4	-2.0	-6.9	B182	0.0	-29.0	2.2	0.0	B756	0.0	0.0	-3.1	-1.9
B12	6.8	-1.7	-2.8	0.0	B91	7.0	-4.4	-2.0	0.0	B182	1.2	-29.0	-2.2	0.0	B756	0.6	0.0	-3.1	0.0
B12	6.8	-1.7	-0.5	0.0	B91	7.0	0.0	0.0	0.0	B184	0.0	-24.9	2.2	0.0	B757	0.0	0.0	-3.1	0.0
B12	6.9	-1.7	-0.5	0.0	B91	7.0	0.0	0.0	0.0	B184	1.2	-24.9	-2.2	0.0	B757	0.6	0.0	-3.1	1.9
B13	0.0	0.0	0.0	0.0	B92	0.0	0.0	0.0	0.0	B185	0.0	-20.1	2.2	0.0	B760	0.0	0.0	-6.5	-3.3
B13	0.1	0.0	0.0	0.0	B92	0.1	0.0	0.0	0.0	B185	1.2	-20.1	-2.2	0.0	B760	0.6	0.0	-6.5	0.6
B13	0.1	2.0	-2.0	0.0	B92	0.1	0.0	-2.6	0.0	B186	0.0	-14.5	2.2	0.0	B767	0.0	0.0	-76.1	45.5
B13	5.1	2.0	-2.0	9.8	B92	3.5	0.0	-2.6	9.1	B186	1.2	-14.5	-2.2	0.0	B767	0.6	0.0	-76.1	91.2
B13	5.1	3.3	-2.0	-3.5	B92	3.5	-4.4	-2.6	-9.1	B187	0.0	-8.2	2.2	0.0	B768	0.0	0.0	74.1	41.7
B13	6.8	3.3	-2.0	-0.1	B92	7.0	-4.4	-2.6	0.0	B187	1.2	-8.2	-2.2	0.0	B768	0.6	0.0	74.1	-2.7
B13	6.8	3.3	-1.5	-0.1	B92	7.0	0.0	0.0	0.0	B188	0.0	-1.1	2.2	0.0	B769	0.0	0.0	69.7	12.7
B13	6.9	3.3	-1.5	0.0	B92	7.0	0.0	0.0	0.0	B188	1.2	-1.1	-2.2	0.0	B769	0.6	0.0	69.7	-29.1
B14	0.0	0.0	0.0	0.0	B93	0.0	0.0	0.0	0.0	B189	0.0	6.7	2.2	0.0	B770	0.0	0.0	65.4	3.6
B14	0.1	0.0	0.0	0.0	B93	0.1	0.0	0.0	0.0	B189	1.2	6.7	-2.2	0.0	B770	0.6	0.0	65.4	-35.6
B14	0.1	2.1	-1.7	0.0	B93	0.1	0.0	-3.3	0.0	B190	0.0	15.3	2.2	0.0	B771	0.0	0.0	61.0	0.2
B14	5.1	2.1	-1.7	8.4	B93	3.5	0.0	-3.3	11.6	B190	1.2	15.3	-2.2	0.0	B771	0.6	0.0	61.0	-36.4
B14	5.1	3.0	-1.7	-3.0	B93	3.5	-4.4	-3.3	-11.6	B191	0.0	24.6	2.2	0.0	B772	0.0	0.0	56.6	-1.4
B14	6.8	3.0	-1.7	-0.1	B93	7.0	-4.4	-3.3	0.0	B191	1.2	24.6	-2.2	0.0	B772	0.6	0.0	56.6	-35.3
B14	6.8	3.0	-1.9	-0.1	B93	7.0	0.0	0.0	0.0	B192	0.0	34.5	2.2	0.0	B773	0.0	0.0	52.3	-2.4
B14	6.9	3.0	-1.9	0.0	B93	7.0	0.0	0.0	0.0	B192	1.2	34.5	-2.2	0.0	B773	0.6	0.0	52.3	-33.8
B15	0.0	0.0	0.0	0.0	B94	0.0	0.0	0.0	0.0	B193	0.0	45.0	2.2	0.0	B774	0.0	0.0	47.9	-3.2
B15	0.1	0.0	0.0	0.0	B94	0.1	0.0	0.0	0.0	B193	1.2	45.0	-2.2	0.0	B774	0.6	0.0	47.9	-32.0
B15	0.1	2.1	-1.5	0.0	B94	0.1	0.0	-4.1	0.0	B194	0.0	55.4	2.2	0.0	B775	0.0	0.0	43.5	-3.9
B15	5.1	2.1	-1.5	7.6	B94	3.5	0.0	-4.1	14.1	B194	1.2	55.4	-2.2	0.0	B775	0.6	0.0	43.5	-30.0
B15	5.1	2.1	-1.5	-2.7	B94	3.5	-4.4	-4.1	-14.1	B195	0.0	63.7	2.2	0.0	B776	0.0	0.0	39.2	-4.6
B15	6.8	2.1	-1.5	-0.1	B94	7.0	-4.4	-4.1	0.0	B195	1.2	63.7	-2.2	0.0	B776	0.6	0.0	39.2	-28.1
B15	6.8	2.1	-1.8	-0.1	B94	7.0	0.0	0.0	0.0	B196	0.0	62.9	2.2	0.0	B777	0.0	0.0	34.8	-5.1
B15	6.9	2.1	-1.8	0.0	B94	7.0	0.0	0.0	0.0	B196	1.2	62.9	-2.2	0.0	B777	0.6	0.0	34.8	-26.0
B16	0.0	0.0	0.0	0.0	B95	0.0	0.0	0.0	0.0	B197	0.0	53.0	2.2	0.0	B778	0.0	0.0	26.0	-6.1
B16	0.1	0.0	0.0	0.0	B95	0.1	0.0	0.0	0.0	B197	1.2	53.0	-2.2	0.0	B778	0.6	0.0	26.0	-21.7
B16	0.1	1.1	-1.2	0.0	B95	0.1	0.0	-4.8	0.0	B198	0.0	42.0	2.2	0.0	B779	0.0	0.0	21.7	-6.4
B16	5.1	1.1	-1.2	5.8	B95	3.5	0.0	-4.8	16.7	B198	1.2	42.0	-2.2	0.0	B779	0.6	0.0	21.7	-19.4
B16	5.1	3.4	-1.2	-2.1	B95	3.5	-4.4	-4.8	-16.7	B199	0.0	29.8	2.2	0.0	B780	0.0	0.0	17.3	-6.6
B16	6.8	3.4	-1.2	-0.1	B95	7.0	-4.4	-4.8	0.0	B199	1.2	29.8	-2.2	0.0	B780	0.6	0.0	17.3	-17.0
B16	6.8	3.4	-1.3	-0.1	B95	7.0	0.0	0.0	0.0	B200	0.0	20.6	2.2	0.0	B781	0.0	0.0	12.9	-6.5
B16	6.9	3.4	-1.3	0.0	B95	7.0	0.0	0.0	0.0	B200	1.2	20.6	-2.2	0.0	B781	0.6	0.0	12.9	-14.3
B17	0.0	3.4	-1.3	0.0	B96	0.0	0.0	0.0	0.0	B201	0.0	12.6	2.2	0.0	B782	0.0	0.0	8.6	-5.6
B17	0.1	3.4	-1.3	0.1	B96	0.1	0.0	0.0	0.0	B201	1.2	12.6	-2.2	0.0	B782	0.6	0.0	8.6	-10.7
B17	0.1	3.4	-1.3	0.1	B96	0.1	0.0	-5.6	0.0	B202	0.0	9.4	2.2	0.0	B783	0.0	0.0	4.2	-2.0
B17	3.6	3.4	-1.3	4.5	B96	3.5	0.0	-5.6	19.3	B202	1.2	9.4	-2.2	0.0	B783	0.6	0.0	4.2	-4.6
B17	3.6	-9.5	-1.3	-5.5	B96	3.5	-4.4	-5.6	-19.3	B203	0.0	5.7	2.2	0.0	B784	0.0	0.0	19.8	-2.0
B17	7.2	-9.5	-1.3	-1.0	B96	7.0	-4.4	-5.6	0.0	B203	1.2	5.7	-2.2	0.0	B784	0.6	0.0	19.8	-13.8
B17	7.2	-8.5	-20.4	-1.0	B96	7.0	0.0	0.0	0.0	B204	0.0	2.5	2.2	0.0	B785	0.0	0.0	15.4	-6.3
B17	7.2	-8.5	-20.4	0.0	B96	7.0	0.0	0.0	0.0	B204	1.2	2.5	-2.2	0.0	B785	0.6	0.0	15.4	-15.6
B18	0.0	2.1	-1.8	0.0	B97	0.0	0.0	0.0	0.0	B213	0.0	-38.6	0.0	0.0	B786	0.0	0.0	11.0	-10.6
B18	0.1	2.1	-1.8	0.1	B97	0.1	0.0	0.0	0.0	B213	1.2	-38.6	0.0	0.0	B786	0.6	0.0	11.0	-17.3
B18	0.1	2.1	-2.1	0.1	B97	0.1	0.0	-6.3	0.0	B214	0.0	-46.0	0.0	0.0	B787	0.0	0.0	6.7	-21.9
B18	3.6	2.1	-2.1	7.7	B97	3.5	0.0	-6.3	21.9	B214	1.2	-46.0	0.0	0.0	B787	0.6	0.0	6.7	-25.9
B18	3.6	-1.1	-2.1	-7.8	B97	3.5	-4.4	-6.3	-21.9	B215	0.0	-37.7	0.0	0.0	B788	0.0	0.0	2.3	-59.2
B18	7.2	-1.1	-2.1	-0.2	B97	7.0	-4.4	-6.3	0.0	B215	1.2	-37.7	0.0	0.0	B788	0.6	0.0	2.3	-60.6
B18	7.2	-1.1	-3.7	-0.2	B97	7.0	0.0	0.0	0.0	B216	0.0	-27.3	0.0	0.0	B210	0.0	0.0	0.0	0.0
B18	7.2	-1.1	-3.7	0.0	B97	7.0	0.0	0.0	0.0	B216	1.2	-27.3	0.0	0.0	B210	0.0	0.0	0.0	0.0
B19	0.0	3.0	-1.9	0.0	B98	0.0	0.0	0.0	0.0	B217	0.0	-16.8	0.0	0.0	B210	0.0	2.1	-1.5	0.0
B19	0.1	3.0	-1.9	0.1	B98	0.1	0.0	0.0	0.0	B217	1.2	-16.8	0.0	0.0	B210	0.1	2.1	-1.5	0.1
B19	0.1	3.0	-2.4	0.1	B98	0.1	0.0	-7.1	0.0	B218	0.0	-6.9	0.0	0.0	B210	0.1	2.1	-1.5	0.1
B19	3.6	3.0	-2.4	8.7	B98	3.5	0.0	-7.1	24.5	B218	1.2	-6.9	0.0	0.0	B210	3.6	2.1	-1.5	5.3
B19	3.6	1.9	-2.4	-8.7	B98	3.5	-4.4	-7.1	-24.5	B219	0.0	2.4	0.0	0.0	B210	3.6	-1.1	-1.5	-5.5
B19	7.2	1.9	-2.4	-0.1	B98	7.0	-4.4	-7.1	0.0	B219	1.2	2.4	0.0	0.0	B210	7.2	-1.1	-1.5	-0.2
B19	7.2	1.9	-2.2	-0.1	B98	7.0	0.0	0.0	0.0	B220	0.0	11.0	0.0	0.0	B210	7.2	-1.1	-4.4	-0.2

B19	7.2	1.9	-2.2	0.0	B98	7.0	0.0	0.0	0.0	B220	1.2	11.0	0.0	0.0	B210	7.3	-1.1	-4.4	0.0
B20	0.0	3.3	-1.5	0.0	B99	0.0	0.0	0.0	0.0	B221	0.0	18.8	0.0	0.0	B208	0.0	0.0	-20.8	-61.1
B20	0.1	3.3	-1.5	0.1	B99	0.1	0.0	0.0	0.0	B221	1.2	18.8	0.0	0.0	B208	0.6	0.0	-20.8	-48.6
B20	0.1	3.3	-2.0	0.1	B99	0.1	0.0	-7.8	0.0	B222	0.0	25.9	0.0	0.0	B209	0.0	0.0	-24.1	-34.0
B20	3.6	3.3	-2.0	7.3	B99	3.5	0.0	-7.8	27.1	B222	1.2	25.9	0.0	0.0	B209	0.6	0.0	-24.1	-19.6
B20	3.6	2.6	-2.0	-7.5	B99	3.5	-4.4	-7.8	-27.1	B224	0.0	37.8	0.0	0.0	B282	0.0	0.0	-24.1	-22.3
B20	7.2	2.6	-2.0	-0.2	B99	7.0	-4.4	-7.8	0.0	B224	1.2	37.8	0.0	0.0	B282	0.6	0.0	-24.1	-7.8
B20	7.2	2.6	-4.5	-0.2	B99	7.0	0.0	0.0	0.0	B225	0.0	42.6	0.0	0.0	B286	0.0	0.0	-23.1	-16.9
B20	7.2	2.6	-4.5	0.0	B99	7.0	0.0	0.0	0.0	B225	1.2	42.6	0.0	0.0	B286	0.6	0.0	-23.1	-3.0
B21	0.0	-1.7	-0.5	0.0	B100	0.0	0.0	0.0	0.0	B226	0.0	46.7	0.0	0.0	B294	0.0	0.0	-19.7	-13.7
B21	0.1	-1.7	-0.5	0.0	B100	0.1	0.0	0.0	0.0	B226	1.2	46.7	0.0	0.0	B294	0.6	0.0	-19.7	-1.9
B21	0.1	-1.7	-0.6	0.0	B100	0.1	0.0	-8.6	0.0	B227	0.0	50.0	0.0	0.0	B414	0.0	0.0	-19.8	-14.6
B21	3.6	-1.7	-0.6	2.0	B100	3.5	0.0	-8.6	29.6	B227	1.2	50.0	0.0	0.0	B414	0.6	0.0	-19.8	-2.7
B21	3.6	-2.9	-0.6	-1.9	B100	3.5	-4.4	-8.6	-29.6	B228	0.0	52.7	0.0	0.0	B429	0.0	0.0	-21.5	-16.4
B21	7.2	-2.9	-0.6	0.0	B100	7.0	-4.4	-8.6	0.0	B228	1.2	52.7	0.0	0.0	B429	0.6	0.0	-21.5	-3.5
B21	7.2	-2.9	1.0	0.0	B100	7.0	0.0	0.0	0.0	B229	0.0	54.7	0.0	0.0	B479	0.0	0.0	-26.1	-20.2
B21	7.2	-2.9	1.0	0.0	B100	7.0	0.0	0.0	0.0	B229	1.2	54.7	0.0	0.0	B479	0.6	0.0	-26.1	-4.5
B22	0.0	-27.8	1.4	0.0	B101	0.0	0.0	0.0	0.0	B230	0.0	56.3	0.0	0.0	B509	0.0	0.0	-28.7	-22.8
B22	0.1	-27.8	1.4	-0.1	B101	0.1	0.0	0.0	0.0	B230	1.2	56.3	0.0	0.0	B509	0.6	0.0	-28.7	-5.6
B22	0.1	-27.8	2.8	-0.1	B101	0.1	0.0	-9.3	0.0	B231	0.0	28.2	0.0	0.0	B527	0.0	0.0	-31.4	-21.9
B22	3.6	-27.8	2.8	-9.9	B101	3.5	0.0	-9.3	32.1	B231	1.2	28.2	0.0	0.0	B527	0.6	0.0	-31.4	-3.0
B22	3.6	-8.5	2.8	18.7	B101	3.5	-4.4	-9.3	-32.1	B232	0.0	30.6	0.0	0.0	B528	0.0	0.0	-34.7	-29.2
B22	6.8	-8.5	2.8	10.0	B101	7.0	-4.4	-9.3	0.0	B232	1.2	30.6	0.0	0.0	B528	0.6	0.0	-34.7	-8.3
B22	6.8	-8.5	24.6	10.0	B101	7.0	0.0	0.0	0.0	B233	0.0	32.3	0.0	0.0	B529	0.0	0.0	-42.4	-37.0
B22	7.2	-8.5	24.6	0.2	B101	7.0	0.0	0.0	0.0	B233	1.2	32.3	0.0	0.0	B529	0.6	0.0	-42.4	-11.6
B22	7.2	-8.5	3.7	0.2	B102	0.0	0.0	0.0	0.0	B234	0.0	32.2	0.0	0.0	B550	0.0	0.0	-63.0	-48.4
B22	7.2	-8.5	3.7	0.0	B102	0.1	0.0	0.0	0.0	B234	1.2	32.2	0.0	0.0	B550	0.6	0.0	-63.0	-10.6
B25	0.0	-35.8	-1.4	0.0	B102	0.1	0.0	-10.0	0.0	B235	0.0	44.2	0.0	0.0	B561	0.0	0.0	-62.3	-46.2
B25	0.1	-35.8	-1.4	0.1	B102	3.5	0.0	-10.0	34.5	B235	1.2	44.2	0.0	0.0	B561	0.6	0.0	-62.3	-8.8
B25	0.1	-35.8	1.3	0.1	B102	3.5	-4.4	-10.0	-34.5	B236	0.0	39.9	0.0	0.0	B613	0.0	0.0	-20.8	-48.6
B25	3.6	-35.8	1.3	-4.7	B102	7.0	-4.4	-10.0	0.0	B236	1.2	39.9	0.0	0.0	B613	0.6	0.0	-20.8	-36.1
B25	3.6	-39.0	1.3	5.0	B102	7.0	0.0	0.0	0.0	B237	0.0	37.4	0.0	0.0	B629	0.0	0.0	-24.1	-19.6
B25	7.2	-39.0	1.3	0.2	B102	7.0	0.0	0.0	0.0	B237	1.2	37.4	0.0	0.0	B629	0.6	0.0	-24.1	-5.1
B25	7.2	-39.0	4.9	0.2	B103	0.0	0.0	0.0	0.0	B239	0.0	35.5	0.0	0.0	B661	0.0	0.0	-24.1	-7.8
B25	7.2	-39.0	4.9	0.0	B103	0.1	0.0	0.0	0.0	B239	1.2	35.5	0.0	0.0	B661	0.6	0.0	-24.1	6.6
B26	0.0	6.1	-3.3	0.0	B103	0.1	0.0	-10.5	0.0	B240	0.0	33.7	0.0	0.0	B696	0.0	0.0	-23.1	-3.0
B26	0.1	6.1	-3.3	0.2	B103	3.5	0.0	-10.5	36.2	B240	1.2	33.7	0.0	0.0	B696	0.6	0.0	-23.1	10.8
B26	0.1	6.1	0.3	0.2	B103	3.5	-4.4	-10.5	-36.2	B241	0.0	32.2	0.0	0.0	B706	0.0	0.0	-19.7	-1.9
B26	3.6	6.1	0.3	-0.8	B103	7.0	-4.4	-10.5	0.0	B241	1.2	32.2	0.0	0.0	B706	0.6	0.0	-19.7	9.9
B26	3.6	9.2	0.3	1.0	B103	7.0	0.0	0.0	0.0	B242	0.0	30.7	0.0	0.0	B755	0.0	0.0	-19.8	-2.7
B26	7.2	9.2	0.3	0.0	B103	7.0	0.0	0.0	0.0	B242	1.2	30.7	0.0	0.0	B755	0.6	0.0	-19.8	9.1
B26	7.2	9.2	0.9	0.0	B104	0.0	0.0	0.0	0.0	B243	0.0	29.5	0.0	0.0	B758	0.0	0.0	-21.5	-3.5
B26	7.2	9.2	0.9	0.0	B104	0.1	0.0	0.0	0.0	B243	1.2	29.5	0.0	0.0	B758	0.6	0.0	-21.5	9.4
B27	0.0	55.0	-2.3	0.0	B104	0.1	0.0	-10.4	0.0	B244	0.0	28.4	0.0	0.0	B806	0.0	0.0	-26.1	-4.5
B27	0.1	55.0	-2.3	0.1	B104	3.5	0.0	-10.4	35.9	B244	1.2	28.4	0.0	0.0	B806	0.6	0.0	-26.1	11.1
B27	0.1	55.0	0.1	0.1	B104	3.5	-4.4	-10.4	-35.9	B245	0.0	27.4	0.0	0.0	B808	0.0	0.0	-28.7	-5.6
B27	3.6	55.0	0.1	-0.3	B104	7.0	-4.4	-10.4	0.0	B245	1.3	27.4	0.0	0.0	B808	0.7	0.0	-28.7	15.2
B27	3.6	55.0	0.1	0.1	B104	7.0	0.0	0.0	0.0	B246	0.0	26.5	0.0	0.0	B810	0.0	0.0	-31.4	-3.0
B27	7.2	55.0	0.1	-0.3	B104	7.0	0.0	0.0	0.0	B246	1.1	26.5	0.0	0.0	B810	0.5	0.0	-31.4	11.9
B27	7.2	55.0	-6.1	-0.3	B105	0.0	0.0	0.0	0.0	B247	0.0	25.2	0.0	0.0	B811	0.0	0.0	-34.7	-8.3
B27	7.2	55.0	-6.1	0.0	B105	0.1	0.0	0.0	0.0	B247	1.2	25.2	0.0	0.0	B811	0.6	0.0	-34.7	12.5
B28	0.0	1.1	3.2	0.0	B105	0.1	0.0	-8.3	0.0	B248	0.0	18.5	0.0	0.0	B812	0.0	0.0	-42.4	-11.6
B28	0.1	1.1	3.4	-0.2	B105	3.5	0.0	-8.3	28.7	B248	1.2	18.5	0.0	0.0	B812	0.6	0.0	-42.4	13.8
B28	0.1	1.1	-14.7	-0.2	B105	3.5	-4.4	-8.3	-28.7	B249	0.0	8.2	0.0	0.0	B813	0.0	0.0	-63.0	-10.6
B28	3.6	1.1	0.0	25.9	B105	7.0	-4.4	-8.3	0.0	B249	1.2	8.2	0.0	0.0	B813	0.6	0.0	-63.0	27.2
B28	3.6	1.1	0.0	26.1	B105	7.0	0.0	0.0	0.0	B250	0.0	16.1	0.0	0.0	B814	0.0	0.0	-62.3	-8.8
B28	7.2	1.1	14.7	0.0	B105	7.0	0.0	0.0	0.0	B250	1.2	16.1	0.0	0.0	B814	0.6	0.0	-62.3	28.6
B28	7.2	1.1	0.8	0.0	B106	0.0	-154.6	-6.5	0.0	B251	0.0	3.6	0.0	0.0	B816	0.0	0.0	-23.7	-4.0
B28	7.2	1.1	1.0	0.0	B106	0.1	-154.6	-6.5	0.3	B251	1.2	3.6	0.0	0.0	B816	0.6	0.0	-23.7	10.2
B29	0.0	29.9	19.8	0.0	B106	0.1	-154.6	0.8	0.3	B252	0.0	15.1	0.0	0.0	B817	0.0	0.0	-23.7	-18.2
B29	8.0	29.9	-13.4	-25.4	B106	3.5	-154.6	0.8	-2.4	B252	1.2	15.1	0.0	0.0	B817	0.6	0.0	-23.7	-4.0

B29	8.0	1.1	-13.4	-72.3	B106	3.5	-4.4	0.8	2.7	B253	0.0	29.5	0.0	0.0	B842	0.0	0.0	-1.8	-2.9
B29	11.5	1.1	-27.9	0.1	B106	7.0	-4.4	0.8	0.0	B253	1.2	29.5	0.0	0.0	B842	0.6	0.0	-1.8	-1.8
B29	11.5	1.1	1.2	0.1	B106	7.0	0.0	0.0	0.0	B254	0.0	25.6	0.0	0.0	B843	0.0	0.0	-1.8	-1.8
B29	11.6	1.1	1.0	0.0	B106	7.0	0.0	0.0	0.0	B254	1.2	25.6	0.0	0.0	B843	0.6	0.0	-1.8	-0.8
B30	0.0	16.2	2.1	0.0	B107	0.0	-20.7	1.0	0.0	B255	0.0	26.1	0.0	0.0	B844	0.0	0.0	-10.9	-9.6
B30	7.2	16.2	2.1	-15.4	B107	0.1	-20.7	1.0	0.0	B255	1.1	26.1	0.0	0.0	B844	0.6	0.0	-10.9	-3.1
B30	7.2	55.0	2.1	7.2	B107	0.1	-20.7	39.6	0.0	B256	0.0	27.0	0.0	0.0	B845	0.0	0.0	-10.9	-3.1
B30	10.7	55.0	2.1	-0.3	B107	0.2	-20.7	39.6	-5.6	B256	1.3	27.0	0.0	0.0	B845	0.6	0.0	-10.9	3.5
B30	10.7	55.0	-6.1	-0.3	B107	0.2	-20.7	9.9	-5.6	B257	0.0	28.0	0.0	0.0	B846	0.0	0.0	-15.7	-7.8
B30	10.8	55.0	-6.1	0.0	B107	3.5	-20.7	9.9	-38.5	B257	1.2	28.0	0.0	0.0	B846	0.6	0.0	-15.7	1.7
B31	0.0	9.2	0.9	0.0	B107	3.5	-4.4	9.9	34.2	B258	0.0	29.2	0.0	0.0	B847	0.0	0.0	-15.7	1.7
B31	0.1	9.2	0.9	0.0	B107	7.0	-4.4	9.9	0.0	B258	1.2	29.2	0.0	0.0	B847	0.6	0.0	-15.7	11.1
B31	0.1	9.2	1.4	0.0	B107	7.0	0.0	0.0	0.0	B259	0.0	30.5	0.0	0.0	B848	0.0	0.0	-92.5	-38.4
B31	3.6	9.2	1.4	-4.9	B107	7.0	0.0	0.0	0.0	B259	1.2	30.5	0.0	0.0	B848	0.6	0.0	-92.5	17.0
B31	3.6	1.0	1.4	8.9	B110	0.0	1.0	31.1	0.0	B260	0.0	32.2	0.0	0.0	B849	0.0	0.0	-92.5	17.0
B31	10.0	1.0	1.4	0.0	B110	0.8	1.0	31.1	-24.9	B260	1.2	32.2	0.0	0.0	B849	0.6	0.0	-92.5	72.5
B35	0.0	-8.5	3.7	0.0	B110	0.8	1.0	11.0	-24.9	B261	0.0	34.3	0.0	0.0	B850	0.0	0.0	-87.1	-51.9
B35	0.1	-8.5	3.7	-0.2	B110	3.3	1.0	11.0	-52.8	B261	1.2	34.3	0.0	0.0	B850	0.6	0.0	-87.1	0.3
B35	0.1	-8.5	-17.3	-0.2	B110	3.3	-4.4	11.0	38.3	B262	0.0	35.4	0.0	0.0	B851	0.0	0.0	-87.1	0.3
B35	1.3	-8.5	-17.3	22.0	B110	6.8	-4.4	11.0	0.0	B262	1.2	35.4	0.0	0.0	B851	0.6	0.0	-87.1	52.6
B35	1.3	-8.5	-2.4	22.0	B110	6.8	0.0	0.0	0.0	B263	0.0	36.7	0.0	0.0	B852	0.0	0.0	-66.5	-51.2
B35	3.6	-8.5	-2.4	27.4	B110	6.8	0.0	0.0	0.0	B263	1.2	36.7	0.0	0.0	B852	0.6	0.0	-66.5	-11.3
B35	3.6	0.1	-2.4	-7.8	B111	0.0	16.2	22.2	0.0	B264	0.0	37.1	0.0	0.0	B853	0.0	0.0	-66.5	-11.3
B35	6.8	0.1	-2.4	0.0	B111	0.8	16.2	22.2	-17.8	B264	1.2	37.1	0.0	0.0	B853	0.6	0.0	-66.5	28.6
B35	6.8	0.0	0.0	0.0	B111	0.8	16.2	12.1	-17.8	B265	0.0	34.1	0.0	0.0	B854	0.0	0.0	-17.2	-24.2
B35	6.8	0.0	0.0	0.0	B111	2.5	16.2	12.1	-38.6	B265	1.2	34.1	0.0	0.0	B854	0.6	0.0	-17.2	-13.8
B36	0.0	0.0	0.0	0.0	B111	2.5	-4.4	12.1	41.9	B266	0.0	59.1	0.0	0.0	B855	0.0	0.0	-17.2	-13.8
B36	0.1	0.0	0.0	0.0	B111	6.0	-4.4	12.1	0.0	B266	1.2	59.1	0.0	0.0	B855	0.6	0.0	-17.2	-3.5
B36	0.1	0.0	-6.0	0.0	B111	6.0	0.0	0.0	0.0	B267	0.0	59.0	0.0	0.0	B856	0.0	0.0	14.4	6.7
B36	3.3	0.0	-6.0	19.4	B111	6.0	0.0	0.0	0.0	B267	1.2	59.0	0.0	0.0	B856	0.6	0.0	14.4	-1.9
B36	3.3	-2.9	-6.0	-21.1	B112	0.0	0.0	0.0	0.0	B268	0.0	59.5	0.0	0.0	B857	0.0	0.0	14.4	-1.9
B36	6.8	-2.9	-6.0	0.0	B112	0.1	0.0	0.0	0.0	B268	1.2	59.5	0.0	0.0	B857	0.6	0.0	14.4	-10.5
B36	6.8	-2.9	1.0	0.0	B112	0.1	-4.4	9.2	0.0	B269	0.0	60.1	0.0	0.0	B858	0.0	0.0	28.8	46.9
B36	6.8	-2.9	1.0	0.0	B112	3.5	-4.4	9.2	-31.9	B269	1.2	60.1	0.0	0.0	B858	0.6	0.0	28.8	29.7
B37	0.0	2.6	-4.5	0.0	B112	3.5	44.9	9.2	15.8	B270	0.0	60.9	0.0	0.0	B859	0.0	0.0	-10.0	-10.3
B37	0.1	2.6	-4.5	0.2	B112	5.2	44.9	9.2	0.0	B270	1.2	60.9	0.0	0.0	B859	0.6	0.0	-10.0	-4.2
B37	0.1	2.6	0.7	0.2	B113	0.0	-2.9	8.1	0.0	B271	0.0	6.0	0.0	0.0	B860	0.0	0.0	-18.3	-12.0
B37	3.6	2.6	0.7	-2.1	B113	0.9	-2.9	8.1	-7.4	B271	1.2	6.0	0.0	0.0	B860	0.6	0.0	-18.3	-1.0
B37	3.6	0.0	0.7	6.2	B113	0.9	-20.1	8.1	16.8	B272	0.0	6.7	0.0	0.0	B861	0.0	0.0	0.0	0.3
B37	6.8	0.0	0.7	4.1	B113	3.4	-20.1	8.1	-3.3	B272	1.2	6.7	0.0	0.0	B861	0.6	0.0	0.0	0.3
B37	6.8	0.0	19.7	4.1	B113	3.4	-4.4	8.1	7.8	B273	0.0	7.6	0.0	0.0	B862	0.0	0.0	-101.5	-43.3
B37	7.0	0.0	19.7	0.2	B113	4.4	-4.4	8.1	0.0	B273	1.2	7.6	0.0	0.0	B862	0.6	0.0	-101.5	17.6
B37	7.0	0.0	0.3	0.2	B113	4.4	0.0	0.0	0.0	B274	0.0	8.7	0.0	0.0	B863	0.0	0.0	-0.1	-19.1
B37	7.6	0.0	0.3	0.0	B113	4.4	0.0	0.0	0.0	B274	1.2	8.7	0.0	0.0	B863	0.7	0.0	-0.1	-19.1
B37	7.6	0.0	0.0	0.0	B114	0.0	0.4	3.2	0.0	B275	0.0	10.2	0.0	0.0	B864	0.0	0.0	0.0	-13.1
B37	7.6	0.0	0.0	0.0	B114	2.6	0.4	3.2	-8.3	B275	1.2	10.2	0.0	0.0	B864	0.6	0.0	0.0	-13.1
B38	0.0	1.9	-2.2	0.0	B114	2.6	-4.4	3.2	3.0	B276	0.0	12.0	0.0	0.0	B865	0.0	0.0	-0.2	-32.6
B38	0.1	1.9	-2.2	0.1	B114	3.6	-4.4	3.2	0.0	B276	1.2	12.0	0.0	0.0	B865	0.6	0.0	-0.2	-32.5
B38	0.1	1.9	-0.6	0.1	B114	3.6	0.0	0.0	0.0	B278	0.0	16.8	0.0	0.0	B866	0.0	0.0	8.4	2.9
B38	3.6	1.9	-0.6	2.0	B114	3.6	0.0	0.0	0.0	B278	1.2	16.8	0.0	0.0	B866	0.6	0.0	8.4	-2.2
B38	3.6	0.0	-0.6	-2.0	B115	0.0	0.1	3.7	0.0	B279	0.0	18.5	0.0	0.0	B867	0.0	0.0	11.3	34.1
B38	6.8	0.0	-0.6	-0.2	B115	1.8	0.1	3.7	-6.7	B279	1.2	18.5	0.0	0.0	B867	0.5	0.0	11.3	28.4
B38	6.8	0.0	-0.3	-0.2	B115	1.8	-4.4	3.7	3.5	B280	0.0	19.4	0.0	0.0	B868	0.0	0.0	8.8	13.3
B38	7.0	0.0	-0.3	-0.2	B115	2.8	-4.4	3.7	0.0	B280	1.2	19.4	0.0	0.0	B868	0.6	0.0	8.8	8.0
B38	7.0	0.0	-0.3	-0.2	B115	2.8	0.0	0.0	0.0	B281	0.0	19.5	0.0	0.0	B869	0.0	0.0	6.9	6.8
B38	7.6	0.0	-0.3	0.0	B115	2.8	0.0	0.0	0.0	B281	1.2	19.5	0.0	0.0	B869	0.6	0.0	6.9	2.7
B38	7.6	0.0	0.0	0.0	B116	0.0	0.3	3.3	0.0	B283	0.0	25.6	0.0	0.0	B870	0.0	0.0	8.0	7.3
B38	7.6	0.0	0.0	0.0	B116	1.0	0.3	3.3	-3.3	B283	1.1	25.6	0.0	0.0	B870	0.6	0.0	8.0	2.5
B39	0.0	-1.1	-3.7	0.0	B116	1.0	-4.4	3.3	3.1	B287	0.0	3.8	0.0	0.0	B871	0.0	0.0	16.5	10.3
B39	0.1	-1.1	-3.7	0.2	B116	2.0	-4.4	3.3	0.0	B287	1.2	3.8	0.0	0.0	B871	0.6	0.0	16.5	0.5
B39	0.1	-1.1	-1.2	0.2	B116	2.0	0.0	0.0	0.0	B290	0.0	-1.2	1.1	0.0	B872	0.0	0.0	28.8	29.7

B39	3.6	-1.1	-1.2	4.5	B116	2.0	0.0	0.0	0.0	B290	1.2	-1.2	-1.1	0.0	B872	0.6	0.0	28.8	12.4
B39	3.6	0.0	-1.2	-4.2	B117	0.0	-0.4	2.5	0.0	B291	0.0	-2.7	1.1	0.0	B873	0.0	0.0	-10.0	-4.2
B39	6.8	0.0	-1.2	-0.2	B117	0.2	-0.4	2.5	-0.5	B291	1.2	-2.7	-1.1	0.0	B873	0.6	0.0	-10.0	1.8
B39	6.8	0.0	-0.9	-0.2	B117	0.2	-2.2	2.5	2.4	B292	0.0	-4.3	1.1	0.0	B874	0.0	0.0	-18.3	-1.0
B39	7.0	0.0	-0.9	0.0	B117	1.2	-2.2	2.5	0.0	B292	1.2	-4.3	-1.1	0.0	B874	0.6	0.0	-18.3	9.9
B39	7.0	0.0	0.0	0.0	B117	1.2	0.0	0.0	0.0	B293	0.0	-6.3	1.0	0.0	B875	0.0	0.0	0.0	0.3
B39	7.0	0.0	0.0	0.0	B117	1.2	0.0	0.0	0.0	B293	1.1	-6.3	-1.0	0.0	B875	0.6	0.0	0.0	0.3
B40	0.0	-8.5	-20.4	0.0	B120	0.0	-46.8	2.7	0.0	B295	0.0	21.1	0.0	0.0	B876	0.0	0.0	-101.5	17.6
B40	0.1	-8.5	-20.4	1.0	B120	0.1	-46.8	2.7	-0.1	B295	1.1	21.1	0.0	0.0	B876	0.5	0.0	-101.5	68.4
B40	0.1	-8.5	-1.7	1.0	B120	0.1	-46.8	3.6	-0.1	B296	0.0	28.1	0.0	0.0	B877	0.0	0.0	-0.1	-19.1
B40	3.6	-8.5	-1.7	6.9	B120	1.2	-46.8	3.6	-4.2	B296	1.1	28.1	0.0	0.0	B877	0.5	0.0	-0.1	-19.0
B40	3.6	0.0	-1.7	-5.8	B120	1.2	0.0	3.6	12.6	B297	0.0	22.9	0.0	0.0	B878	0.0	0.0	0.0	-13.1
B40	7.0	0.0	-1.7	0.0	B120	4.3	0.0	3.6	1.2	B297	1.2	22.9	0.0	0.0	B878	0.7	0.0	0.0	-13.1
B40	7.0	0.0	0.0	0.0	B120	4.3	0.0	24.9	1.2	B298	0.0	21.2	0.0	0.0	B879	0.0	0.0	-0.2	-32.5
B40	7.0	0.0	0.0	0.0	B120	4.4	0.0	24.9	0.0	B298	1.2	21.2	0.0	0.0	B879	0.8	0.0	-0.2	-32.3
B41	0.0	0.0	0.0	0.0	B120	4.4	0.0	0.0	0.0	B299	0.0	18.7	0.0	0.0	B880	0.0	0.0	8.4	-2.2
B41	0.0	0.0	0.0	0.0	B120	4.4	0.0	0.0	0.0	B299	1.2	18.7	0.0	0.0	B880	0.5	0.0	8.4	-6.4
B41	0.0	2.1	-2.3	0.0	B121	0.0	-35.8	-2.7	0.0	B301	0.0	23.2	0.0	0.0	B881	0.0	0.0	11.3	28.4
B41	0.1	2.1	-2.3	0.1	B121	0.1	-35.8	-2.7	0.1	B301	1.2	23.2	0.0	0.0	B881	0.6	0.0	11.3	21.6
B41	0.1	2.1	-2.3	0.1	B121	0.1	-35.8	-3.6	0.1	B302	0.0	21.6	0.0	0.0	B882	0.0	0.0	8.8	8.0
B41	3.6	2.1	-2.3	8.3	B121	1.2	-35.8	-3.6	4.2	B302	1.2	21.6	0.0	0.0	B882	0.6	0.0	8.8	2.8
B41	3.6	0.0	-2.3	-7.8	B121	1.2	0.0	-3.6	-12.6	B303	0.0	21.8	0.0	0.0	B883	0.0	0.0	6.9	2.7
B41	7.1	0.0	-2.3	0.0	B121	4.3	0.0	-3.6	-1.2	B303	1.2	21.8	0.0	0.0	B883	0.6	0.0	6.9	-1.5
B41	7.1	0.0	0.0	0.0	B121	4.3	0.0	-24.9	-1.2	B304	0.0	19.3	0.0	0.0	B884	0.0	0.0	8.0	2.5
B41	7.1	0.0	0.0	0.0	B121	4.4	0.0	-24.9	0.0	B304	1.1	19.3	0.0	0.0	B884	0.6	0.0	8.0	-2.3
B52	0.0	0.0	0.0	0.0	B121	4.4	0.0	0.0	0.0	B305	0.0	20.9	0.0	0.0	B885	0.0	0.0	16.5	0.5
B52	0.0	0.0	0.0	0.0	B121	4.4	0.0	0.0	0.0	B305	1.1	20.9	0.0	0.0	B885	0.6	0.0	16.5	-9.4
B52	0.0	2.1	0.0	0.0	B155	0.0	0.0	0.0	0.0	B306	0.0	18.1	0.0	0.0	B886	0.0	0.0	11.0	-8.7
B52	0.1	2.1	0.0	0.0	B155	0.1	0.0	0.0	0.0	B306	1.2	18.1	0.0	0.0	B886	0.6	0.0	11.0	-15.3
B52	0.1	2.1	0.0	0.0	B155	0.1	0.0	12.0	0.0	B307	0.0	15.6	0.0	0.0	B887	0.0	0.0	7.3	-1.6
B52	3.6	2.1	0.0	-0.1	B155	0.2	0.0	12.0	-2.0	B307	1.2	15.6	0.0	0.0	B887	0.5	0.0	7.3	-5.3
B52	3.6	-0.2	0.0	0.1	B155	0.2	0.0	-2.5	-2.0	B308	0.0	12.1	0.0	0.0	B888	0.0	0.0	8.6	3.7
B52	7.2	-0.2	0.0	0.0	B155	3.6	0.0	-2.5	6.5	B308	1.2	12.1	0.0	0.0	B888	0.6	0.0	8.6	-1.5
B52	7.2	0.0	0.0	0.0	B155	3.6	2.1	-2.5	-9.0	B309	0.0	9.3	0.0	0.0	B889	0.0	0.0	9.5	4.8
B52	7.3	0.0	0.0	0.0	B155	7.2	2.1	-2.5	-0.1	B309	1.2	9.3	0.0	0.0	B889	0.6	0.0	9.5	-1.0
B53	0.0	0.0	0.0	0.0	B155	7.2	2.1	-2.5	-0.1	B310	0.0	6.8	0.0	0.0	B890	0.0	0.0	9.6	3.6
B53	0.0	0.0	0.0	0.0	B155	7.2	2.1	-2.5	0.0	B310	1.1	6.8	0.0	0.0	B890	0.6	0.0	9.6	-2.1
B53	0.0	2.1	-1.0	0.0	B155	7.2	0.0	0.0	0.0	B312	0.0	-1.4	0.0	0.0	B891	0.0	0.0	11.0	-15.3
B53	0.1	2.1	-1.0	0.0	B155	7.3	0.0	0.0	0.0	B312	1.1	-1.4	0.0	0.0	B891	0.5	0.0	11.0	-20.8
B53	0.1	2.1	-1.0	0.0	B156	0.0	0.0	0.0	0.0	B313	0.0	-1.3	0.0	0.0	B892	0.0	0.0	7.3	-5.3
B53	3.6	2.1	-1.0	3.5	B156	0.1	0.0	0.0	0.0	B313	1.1	-1.3	0.0	0.0	B892	0.6	0.0	7.3	-9.7
B53	3.6	18.7	-1.0	-2.3	B156	0.1	0.0	-1.8	0.0	B314	0.0	-0.8	0.0	0.0	B893	0.0	0.0	8.6	-1.5
B53	7.2	18.7	-1.0	1.2	B156	3.6	0.0	-1.8	6.4	B314	1.2	-0.8	0.0	0.0	B893	0.6	0.0	8.6	-6.7
B53	7.2	18.7	24.0	1.2	B156	3.6	2.1	-1.8	-6.5	B315	0.0	-0.3	0.0	0.0	B894	0.0	0.0	9.5	-1.0
B53	7.3	18.7	24.0	0.0	B156	7.2	2.1	-1.8	-0.1	B315	1.2	-0.3	0.0	0.0	B894	0.6	0.0	9.5	-6.7
B55	0.0	0.0	0.0	0.0	B156	7.2	2.1	-1.8	-0.1	B316	0.0	0.1	0.0	0.0	B895	0.0	0.0	9.6	-2.1
B55	0.0	0.0	0.0	0.0	B156	7.2	2.1	-1.8	0.0	B316	1.2	0.1	0.0	0.0	B895	0.6	0.0	9.6	-7.9
B55	0.0	2.1	-1.2	0.0	B156	7.2	0.0	0.0	0.0	B317	0.0	-0.2	0.0	0.0	B896	0.0	0.0	0.0	-12.9
B55	0.1	2.1	-1.2	0.1	B156	7.3	0.0	0.0	0.0	B317	1.2	-0.2	0.0	0.0	B896	0.6	0.0	0.0	-12.9
B55	0.1	2.1	-1.2	0.1	B157	0.0	0.0	0.0	0.0	B318	0.0	-0.4	0.0	0.0	B897	0.0	0.0	52.9	32.8
B55	3.6	2.1	-1.2	4.2	B157	0.1	0.0	0.0	0.0	B318	1.2	-0.4	0.0	0.0	B897	0.6	0.0	52.9	1.0
B55	3.6	-4.4	-1.2	-4.2	B157	0.1	0.0	-1.5	0.0	B319	0.0	-0.6	0.0	0.0	B898	0.0	0.0	56.9	15.9
B55	7.2	-4.4	-1.2	0.0	B157	3.6	0.0	-1.5	5.4	B319	1.2	-0.6	0.0	0.0	B898	0.6	0.0	56.9	-18.2
B55	7.2	-4.4	-0.7	0.0	B157	3.6	2.1	-1.5	-5.4	B320	0.0	-0.2	0.0	0.0	B899	0.0	0.0	19.0	-17.4
B55	7.3	-4.4	-0.7	0.0	B157	7.2	2.1	-1.5	-0.1	B320	1.1	-0.2	0.0	0.0	B899	0.6	0.0	19.0	-28.8
B56	0.0	0.0	0.0	0.0	B157	7.2	2.1	-1.5	-0.1	B321	0.0	2.1	0.0	0.0	B900	0.0	0.0	8.7	-23.7
B56	0.0	0.0	0.0	0.0	B157	7.2	2.1	-1.5	0.0	B321	1.1	2.1	0.0	0.0	B900	0.6	0.0	8.7	-28.9
B56	0.0	2.1	-0.6	0.0	B157	7.2	0.0	0.0	0.0	B323	0.0	7.6	0.0	0.0	B901	0.0	0.0	0.0	-12.9
B56	0.1	2.1	-0.6	0.0	B157	7.3	0.0	0.0	0.0	B323	1.1	7.6	0.0	0.0	B901	0.6	0.0	0.0	-12.9
B56	0.1	2.1	-0.6	0.0	B158	0.0	0.0	0.0	0.0	B324	0.0	11.9	0.0	0.0	B902	0.0	0.0	52.9	1.0
B56	3.6	2.1	-0.6	2.3	B158	0.1	0.0	0.0	0.0	B324	1.2	11.9	0.0	0.0	B902	0.6	0.0	52.9	-30.7

B56	3.6	-5.3	-0.6	-2.3	B158	0.1	0.0	-1.2	0.0	B325	0.0	14.1	0.0	0.0	B903	0.0	0.0	56.9	-18.2
B56	7.2	-5.3	-0.6	0.0	B158	3.6	0.0	-1.2	4.2	B325	1.2	14.1	0.0	0.0	B903	0.6	0.0	56.9	-52.4
B56	7.2	-5.3	0.6	0.0	B158	3.6	2.1	-1.2	-4.2	B326	0.0	15.7	0.0	0.0	B904	0.0	0.0	19.0	-28.8
B56	7.3	-5.3	0.6	0.0	B158	7.2	2.1	-1.2	-0.1	B326	1.2	15.7	0.0	0.0	B904	0.6	0.0	19.0	-40.2
B58	0.0	0.0	0.0	0.0	B158	7.2	2.1	-1.2	-0.1	B327	0.0	18.2	0.0	0.0	B905	0.0	0.0	8.7	-28.9
B58	0.0	0.0	0.0	0.0	B158	7.2	2.1	-1.2	0.0	B327	1.2	18.2	0.0	0.0	B905	0.5	0.0	8.7	-33.2
B58	0.0	2.1	-1.0	0.0	B158	7.2	0.0	0.0	0.0	B329	0.0	29.2	0.0	0.0	B906	0.0	0.0	-82.6	-86.5
B58	0.1	2.1	-1.0	0.1	B158	7.3	0.0	0.0	0.0	B329	1.2	29.2	0.0	0.0	B906	0.6	0.0	-82.6	-37.0
B58	0.1	2.1	-1.0	0.1	B159	0.0	0.0	0.0	0.0	B330	0.0	20.9	0.0	0.0	B908	0.0	0.0	-82.6	-37.0
B58	3.6	2.1	-1.0	3.6	B159	0.1	0.0	0.0	0.0	B330	1.2	20.9	0.0	0.0	B908	0.7	0.0	-82.6	20.8
B58	3.6	-4.3	-1.0	-3.6	B159	0.1	0.0	-0.9	0.0	B331	0.0	20.4	0.0	0.0	B910	0.0	0.0	-35.8	4.1
B58	7.2	-4.3	-1.0	0.1	B159	3.6	0.0	-0.9	3.2	B331	1.2	20.4	0.0	0.0	B910	0.6	0.0	-35.8	25.6
B58	7.2	-4.3	1.1	0.1	B159	3.6	2.1	-0.9	-3.2	B332	0.0	24.3	0.0	0.0	B911	0.0	0.0	-35.8	25.6
B58	7.3	-4.3	1.1	0.0	B159	7.2	2.1	-0.9	0.0	B332	1.2	24.3	0.0	0.0	B911	0.6	0.0	-35.8	47.1
B59	0.0	0.0	0.0	0.0	B159	7.2	2.1	-0.9	0.0	B333	0.0	22.6	0.0	0.0	B914	0.0	0.0	0.0	63.8
B59	0.0	0.0	0.0	0.0	B159	7.2	2.1	-0.9	0.0	B333	1.1	22.6	0.0	0.0	B914	0.6	0.0	0.0	63.8
B59	0.0	2.1	-0.4	0.0	B159	7.2	0.0	0.0	0.0	B334	0.0	13.5	0.0	0.0	B915	0.0	0.0	0.0	63.8
B59	0.1	2.1	-0.4	0.0	B159	7.3	0.0	0.0	0.0	B334	1.1	13.5	0.0	0.0	B915	0.8	0.0	0.0	63.8
B59	0.1	2.1	-0.4	0.0	B160	0.0	0.0	0.0	0.0	B335	0.0	15.9	0.0	0.0	B921	0.0	-10.1	0.0	0.0
B59	3.6	2.1	-0.4	1.6	B160	0.1	0.0	0.0	0.0	B335	1.2	15.9	0.0	0.0	B921	1.2	-10.1	0.0	0.0
B59	3.6	-2.7	-0.4	-1.5	B160	0.1	0.0	-0.7	0.0	B336	0.0	19.5	0.0	0.0	B922	0.0	-20.0	0.0	0.0
B59	7.2	-2.7	-0.4	0.1	B160	3.6	0.0	-0.7	2.5	B336	1.2	19.5	0.0	0.0	B922	1.2	-20.0	0.0	0.0
B59	7.2	-2.7	1.2	0.1	B160	3.6	2.1	-0.7	-2.5	B337	0.0	20.1	0.0	0.0	B923	0.0	-29.7	0.0	0.0
B59	7.3	-2.7	1.2	0.0	B160	7.2	2.1	-0.7	0.0	B337	1.2	20.1	0.0	0.0	B923	1.2	-29.7	0.0	0.0
B60	0.0	0.0	0.0	0.0	B160	7.2	2.1	-0.7	0.0	B338	0.0	13.9	0.0	0.0	B8	0.0	0.0	-58.9	-29.5
B60	0.0	0.0	0.0	0.0	B160	7.2	2.1	-0.7	0.0	B338	1.2	13.9	0.0	0.0	B8	0.5	0.0	-58.9	0.0
B60	0.0	2.1	0.2	0.0	B160	7.2	0.0	0.0	0.0	B413	0.0	3.2	1.1	0.0	B144	0.0	19.6	0.0	0.0
B60	0.1	2.1	0.2	0.0	B160	7.3	0.0	0.0	0.0	B413	1.2	3.2	-1.1	0.0	B144	1.1	19.6	0.0	0.0
B60	0.1	2.1	0.2	0.0	B162	0.0	0.0	0.0	0.0	B555	0.0	-4.9	0.0	0.0	B148	0.0	0.0	0.2	-16.7
B60	3.6	2.1	0.2	-0.9	B162	0.0	0.0	0.0	0.0	B555	3.9	-4.9	0.0	0.0	B148	0.6	0.0	0.2	-16.8
B60	3.6	-2.1	0.2	1.0	B162	0.0	2.1	-0.8	0.0	B556	0.0	-0.7	0.0	0.0	B152	0.1	0.0	47.0	0.0
B60	7.2	-2.1	0.2	0.1	B162	0.1	2.1	-0.8	0.0	B556	3.9	-0.7	0.0	0.0	B152	0.7	0.0	47.0	-28.2
B60	7.2	-2.1	1.6	0.1	B162	0.1	2.1	-0.8	0.0	B558	0.0	21.8	0.0	0.0	B154	0.0	0.0	0.2	-16.8
B60	7.3	-2.1	1.6	0.0	B162	3.6	2.1	-0.8	2.8	B558	1.3	21.8	0.0	0.0	B154	0.6	0.0	0.2	-16.9
B61	0.0	0.0	0.0	0.0	B162	3.6	0.0	-0.8	-2.8	B559	0.0	0.5	0.0	0.0	B54	0.0	1.1	-18.4	0.0
B61	0.0	0.0	0.0	0.0	B162	7.2	0.0	-0.8	0.0	B559	1.2	0.5	0.0	0.0	B54	7.8	1.1	13.9	17.8
B61	0.0	2.1	0.9	0.0	B162	7.2	0.0	0.0	0.0	B560	0.0	21.8	0.0	0.0	B54	7.8	1.1	13.9	30.8
B61	0.1	2.1	0.9	0.0	B162	7.3	0.0	0.0	0.0	B560	1.4	21.8	0.0	0.0	B54	9.6	1.1	21.1	0.2
B61	0.1	2.1	0.9	0.0	B163	0.0	0.0	0.0	0.0	B562	0.0	17.4	0.0	0.0	B54	9.6	1.1	2.9	0.2
B61	3.6	2.1	0.9	-3.4	B163	0.0	0.0	0.0	0.0	B562	1.2	17.4	0.0	0.0	B54	9.6	1.1	3.2	0.0
B61	3.6	-2.0	0.9	3.4	B163	0.0	2.1	-0.6	0.0	B563	0.0	0.3	0.0	0.0	B430	0.0	55.0	-2.3	0.0
B61	7.2	-2.0	0.9	0.1	B163	0.1	2.1	-0.6	0.0	B563	1.3	0.3	0.0	0.0	B430	0.1	55.0	-2.3	0.1
B61	7.2	-2.0	2.1	0.1	B163	0.1	2.1	-0.6	0.0	B564	0.0	14.9	0.0	0.0	B430	0.1	55.0	-4.8	0.1
B61	7.3	-2.0	2.1	0.0	B163	3.6	2.1	-0.6	2.0	B564	1.4	14.9	0.0	0.0	B430	1.8	55.0	-4.8	8.5
B62	0.0	0.0	0.0	0.0	B163	3.6	0.0	-0.6	-2.0	B567	0.0	0.5	0.0	0.0	B430	1.8	2.1	-4.8	-37.3
B62	0.0	0.0	0.0	0.0	B163	7.2	0.0	-0.6	0.0	B567	1.2	0.5	0.0	0.0	B430	9.6	2.1	-4.8	0.0
B62	0.0	2.2	1.6	0.0	B163	7.2	0.0	0.0	0.0	B568	0.0	0.3	0.0	0.0	B531	0.0	6.1	-3.3	0.0
B62	0.1	2.2	1.6	-0.1	B163	7.3	0.0	0.0	0.0	B568	1.2	0.3	0.0	0.0	B531	0.1	6.1	-3.3	0.2
B62	0.1	2.2	1.6	-0.1	B164	0.0	0.0	0.0	0.0	B530	0.0	0.0	12.0	0.0	B531	0.1	6.1	-4.9	0.2
B62	3.6	2.2	1.6	-5.8	B164	0.0	0.0	0.0	0.0	B530	0.5	0.0	12.0	-6.0	B531	1.8	6.1	-4.9	8.7
B62	3.6	-2.0	1.6	5.9	B164	0.0	2.1	-0.5	0.0	B65	0.0	32.2	0.0	0.0	B531	1.8	2.1	-4.9	-38.0
B62	7.2	-2.0	1.6	0.1	B164	0.1	2.1	-0.5	0.0	B65	1.2	32.2	0.0	0.0	B531	9.6	2.1	-4.9	0.0
B62	7.2	-2.0	2.5	0.1	B164	0.1	2.1	-0.5	0.0	B183	0.0	0.3	0.0	0.0	B533	0.0	-35.8	-1.4	0.0
B62	7.3	-2.0	2.5	0.0	B164	3.6	2.1	-0.5	1.8	B183	1.2	0.3	0.0	0.0	B533	0.1	-35.8	-1.4	0.1
B67	0.0	0.0	0.0	0.0	B164	3.6	0.2	-0.5	-1.8	B288	0.0	0.0	-6.5	-7.2	B533	0.1	-35.8	-3.7	0.1
B67	0.1	0.0	0.0	0.0	B164	7.2	0.2	-0.5	0.0	B288	0.6	0.0	-6.5	-3.3	B533	1.8	-35.8	-3.7	6.5
B67	0.1	2.1	3.9	0.0	B164	7.2	0.0	0.0	0.0	B574	0.0	0.0	-76.1	-0.1	B533	1.8	2.1	-3.7	-28.5
B67	1.0	2.1	3.9	-3.6	B164	7.3	0.0	0.0	0.0	B574	0.6	0.0	-76.1	45.5	B533	9.6	2.1	-3.7	0.0
B67	1.0	-5.1	3.9	4.4	B169	0.0	0.0	0.0	0.0	B575	0.0	0.0	74.1	86.2	B535	0.0	2.0	-1.7	0.0
B67	1.9	-5.1	3.9	0.8	B169	0.0	0.0	0.0	0.0	B575	0.6	0.0	74.1	41.7	B535	7.8	2.0	-1.7	13.6
B67	1.9	-5.1	15.5	0.8	B169	0.0	2.1	2.1	0.0	B576	0.0	0.0	69.7	54.6	B535	7.8	-8.4	-1.7	-2.9



B67	1.9	-5.1	15.5	0.0	B169	0.1	2.1	2.1	-0.1	B576	0.6	0.0	69.7	12.7	B535	9.6	-8.4	-1.7	0.1
B68	0.0	0.0	0.0	0.0	B169	0.1	2.1	2.1	-0.1	B577	0.0	0.0	65.4	42.8	B535	9.6	-8.4	2.6	0.1
B68	0.1	0.0	0.0	0.0	B169	3.6	2.1	2.1	-7.7	B577	0.6	0.0	65.4	3.6	B535	9.6	-8.4	2.6	0.0
B68	0.1	1.1	3.2	0.0	B169	3.6	-1.6	2.1	7.9	B578	0.0	0.0	61.0	36.8	B537	0.0	-63.5	6.1	0.0
B68	1.0	1.1	3.2	-2.9	B169	7.2	-1.6	2.1	0.2	B578	0.6	0.0	61.0	0.2	B537	0.1	-63.5	6.1	-0.3
B68	1.0	11.3	3.2	3.3	B169	7.2	-1.6	3.0	0.2	B579	0.0	0.0	56.6	32.6	B537	0.1	-63.5	-1.5	-0.3
B68	1.9	11.3	3.2	0.3	B169	7.3	-1.6	3.0	0.0	B579	0.6	0.0	56.6	-1.4	B537	1.8	-63.5	-1.5	2.3
B68	1.9	11.3	6.8	0.3	B170	0.0	0.0	0.0	0.0	B580	0.0	0.0	52.3	29.0	B537	1.8	4.1	-1.5	-1.5
B68	1.9	11.3	6.8	0.0	B170	0.0	0.0	0.0	0.0	B580	0.6	0.0	52.3	-2.4	B537	3.6	4.1	-1.5	1.2
B69	0.0	-64.5	6.8	0.0	B170	0.0	2.0	2.4	0.0	B581	0.0	0.0	47.9	25.5	B537	3.6	4.1	-2.2	1.2
B69	0.1	-64.5	6.6	-0.3	B170	0.1	2.0	2.4	-0.1	B581	0.6	0.0	47.9	-3.2	B537	5.1	4.1	-2.2	4.4
B69	0.1	-64.5	22.6	-0.3	B170	0.1	2.0	2.4	-0.1	B582	0.0	0.0	43.5	22.2	B537	5.1	4.1	-7.1	4.4
B69	6.1	-64.5	-2.4	-61.6	B170	3.6	2.0	2.4	-8.8	B582	0.6	0.0	43.5	-3.9	B537	6.8	4.1	-7.1	17.0
B69	6.1	-2.2	-2.4	-33.0	B170	3.6	-0.8	2.4	8.9	B583	0.0	0.0	39.2	18.9	B537	6.8	2.1	-7.1	-19.7
B69	9.6	-2.2	-16.7	0.0	B170	7.2	-0.8	2.4	0.1	B583	0.6	0.0	39.2	-4.6	B537	9.6	2.1	-7.1	0.0
B69	9.6	0.0	0.2	0.0	B170	7.2	-0.8	3.0	0.1	B584	0.0	0.0	34.8	15.7	B539	0.0	2.2	3.8	0.0
B69	9.6	0.0	0.0	0.0	B170	7.3	-0.8	3.0	0.0	B584	0.6	0.0	34.8	-5.1	B539	2.8	2.2	3.8	-10.5
B70	0.0	-5.1	15.5	0.0	B171	0.0	0.0	0.0	0.0	B585	0.0	0.0	30.4	12.6	B539	2.8	0.0	3.8	7.1
B70	0.1	-5.1	15.5	-0.8	B171	0.0	0.0	0.0	0.0	B585	0.6	0.0	30.4	-5.6	B539	4.6	0.0	3.8	0.0
B70	0.1	-5.1	7.6	-0.8	B171	0.0	2.1	2.4	0.0	B586	0.0	0.0	30.4	-5.6	B539	4.6	0.0	0.0	0.0
B70	6.1	-5.1	7.6	-47.0	B171	0.1	2.1	2.4	-0.1	B586	0.6	0.0	30.4	-23.9	B539	4.7	0.0	0.0	0.0
B70	6.1	-4.4	7.6	26.5	B171	0.1	2.1	2.4	-0.1	B587	0.0	0.0	26.0	9.6	B543	0.0	2.2	0.0	0.0
B70	9.6	-4.4	7.6	0.0	B171	3.6	2.1	2.4	-8.7	B587	0.6	0.0	26.0	-6.1	B543	2.7	2.2	0.0	0.0
B70	9.6	0.0	0.0	0.0	B171	3.6	3.3	2.4	8.6	B588	0.0	0.0	21.7	6.6	B545	0.0	1.0	0.0	0.0
B70	9.6	0.0	0.0	0.0	B171	7.2	3.3	2.4	-0.1	B588	0.6	0.0	21.7	-6.4	B545	2.7	1.0	0.0	0.0
B71	0.0	16.3	-3.7	0.0	B171	7.2	3.3	-1.5	-0.1	B589	0.0	0.0	17.3	3.8	B547	0.0	18.4	1.1	0.0
B71	0.1	16.3	-3.7	0.2	B171	7.3	3.3	-1.5	0.0	B589	0.6	0.0	17.3	-6.6	B547	1.2	18.4	-1.1	0.0
B71	0.1	16.3	6.6	0.2	B172	0.0	0.0	0.0	0.0	B590	0.0	0.0	12.9	1.3	B548	0.0	23.2	1.0	0.0
B71	6.1	16.3	6.6	-39.5	B172	0.0	0.0	-0.2	0.0	B590	0.6	0.0	12.9	-6.5	B548	1.2	23.2	-1.0	0.0
B71	6.1	-4.4	6.6	22.7	B172	0.0	1.1	19.1	0.0	B591	0.0	0.0	8.6	-0.5	B549	0.0	28.1	1.0	0.0
B71	9.6	-4.4	6.6	0.0	B172	3.6	1.1	4.1	-41.8	B591	0.6	0.0	8.6	-5.6	B549	1.2	28.1	-1.0	0.0
B71	9.6	0.0	0.0	0.0	B172	3.6	18.3	4.1	-27.0	B592	0.0	0.0	4.2	0.5	B553	0.0	31.7	1.0	0.0
B71	9.6	0.0	0.0	0.0	B172	5.4	18.3	-3.1	-27.9	B592	0.6	0.0	4.2	-2.0	B553	1.2	31.7	-1.0	0.0
B72	0.0	-2.0	2.5	0.0	B172	5.4	19.4	-10.2	-27.9	B593	0.0	0.0	19.8	9.9	B557	0.0	33.5	1.0	0.0
B72	0.1	-2.0	2.5	-0.1	B172	6.3	19.4	-14.0	-16.7	B593	0.6	0.0	19.8	-2.0	B557	1.1	33.5	-1.0	0.0
B72	0.1	-2.0	3.6	-0.1	B172	6.3	16.3	-14.0	-14.9	B594	0.0	0.0	15.4	2.9	B566	0.0	40.6	1.1	0.0
B72	6.1	-2.0	3.6	-21.6	B172	7.2	16.3	-17.9	-0.2	B594	0.6	0.0	15.4	-6.3	B566	1.3	40.6	-1.1	0.0
B72	6.1	-4.6	3.6	12.3	B172	7.2	16.3	-3.4	-0.2	B595	0.0	0.0	11.0	-4.0	B570	0.0	36.8	1.1	0.0
B72	9.6	-4.6	3.6	0.0	B172	7.3	16.3	-3.7	0.0	B595	0.6	0.0	11.0	-10.6	B570	1.2	36.8	-1.1	0.0
B72	9.6	0.0	0.0	0.0	B42	0.0	-63.5	6.1	0.0	B596	0.0	0.0	6.7	-17.9	B571	0.0	0.0	1.2	0.0
B72	9.6	0.0	0.0	0.0	B42	0.1	-63.5	6.1	-0.3	B596	0.6	0.0	6.7	-21.9	B571	1.4	0.0	-1.2	0.0
B73	0.0	3.3	-1.5	0.0	B42	0.1	-63.5	12.9	-0.3	B597	0.0	0.0	2.3	-57.8	B572	0.0	0.0	1.0	0.0
B73	0.1	3.3	-1.5	0.1	B42	3.6	-63.5	12.9	-46.0	B597	0.6	0.0	2.3	-59.2	B572	1.1	0.0	-1.0	0.0
B73	0.1	3.3	5.2	0.1	B42	3.6	-101.4	12.9	37.2	B631	0.0	0.0	12.3	4.9	B608	0.0	42.3	1.1	0.0
B73	6.1	3.3	5.2	-31.5	B42	6.8	-101.4	12.9	-3.4	B631	0.6	0.0	12.3	-2.4	B608	1.2	42.3	-1.1	0.0
B73	6.1	-4.4	5.2	18.1	B42	6.8	-101.4	-9.0	-3.4	B632	0.0	0.0	10.2	3.1	B609	0.0	44.6	1.1	0.0
B73	9.6	-4.4	5.2	0.0	B42	7.2	-101.4	-9.0	0.2	B632	0.6	0.0	10.2	-3.0	B609	1.2	44.6	-1.1	0.0
B73	9.6	0.0	0.0	0.0	B42	7.2	-101.4	4.5	0.2	B633	0.0	0.0	8.1	1.7	B610	0.0	47.1	1.1	0.0
B73	9.6	0.0	0.0	0.0	B42	7.2	-101.4	4.5	0.0	B633	0.6	0.0	8.1	-3.2	B610	1.2	47.1	-1.1	0.0
B74	0.0	-0.8	3.0	0.0	B43	0.0	-8.4	2.6	0.0	B634	0.0	0.0	6.0	0.4	B611	0.0	48.9	1.1	0.0
B74	0.1	-0.8	3.0	-0.1	B43	0.1	-8.4	2.6	-0.1	B634	0.6	0.0	6.0	-3.2	B611	1.2	48.9	-1.1	0.0
B74	0.1	-0.8	4.3	-0.1	B43	0.1	-8.4	5.1	-0.1	B635	0.0	0.0	3.9	-0.4	B612	0.0	50.4	1.1	0.0
B74	6.1	-0.8	4.3	-26.1	B43	3.6	-8.4	5.1	-18.2	B635	0.6	0.0	3.9	-2.7	B612	1.2	50.4	-1.1	0.0
B74	6.1	-4.1	4.3	14.9	B43	3.6	-53.1	5.1	18.4	B636	0.0	0.0	1.8	0.0	B614	0.0	51.6	1.1	0.0
B74	9.6	-4.1	4.3	0.0	B43	7.2	-53.1	5.1	0.4	B636	0.6	0.0	1.8	-1.0	B614	1.2	51.6	-1.1	0.0
B74	9.6	0.0	0.0	0.0	B43	7.2	-53.1	7.6	0.4	B637	0.0	0.0	6.1	3.3	B615	0.0	52.5	1.1	0.0
B74	9.6	0.0	0.0	0.0	B43	7.2	-53.1	7.6	0.0	B637	0.6	0.0	6.1	-0.3	B615	1.2	52.5	-1.1	0.0
B75	0.0	-1.6	3.0	0.0	B45	0.0	-101.4	4.5	0.0	B638	0.0	0.0	4.0	1.7	B616	0.0	53.2	1.1	0.0
B75	0.1	-1.6	3.0	-0.2	B45	0.1	-101.4	4.5	-0.2	B638	0.6	0.0	4.0	-0.7	B616	1.2	53.2	-1.1	0.0
B75	0.1	-1.6	3.9	-0.2	B45	0.1	-101.4	27.0	-0.2	B639	0.0	0.0	1.9	1.0	B617	0.0	53.1	1.1	0.0
B75	6.1	-1.6	3.9	-23.6	B45	1.3	-101.4	27.0	-34.8	B639	0.6	0.0	1.9	-0.1	B617	1.2	53.1	-1.1	0.0

B75	6.1	-4.4	3.9	13.5	B45	1.3	-101.4	9.7	-34.8	B640	0.0	0.0	0.0	2.4	B618	0.0	53.9	1.1	0.0
B75	9.6	-4.4	3.9	0.0	B45	3.6	-101.4	9.7	-56.3	B640	0.6	0.0	0.0	2.4	B618	1.2	53.9	-1.1	0.0
B75	9.6	0.0	0.0	0.0	B45	3.6	0.0	9.7	31.2	B641	0.0	0.0	-2.3	2.2	B619	0.0	54.5	1.1	0.0
B75	9.6	0.0	0.0	0.0	B45	6.8	0.0	9.7	0.0	B641	0.6	0.0	-2.3	3.6	B619	1.2	54.5	-1.1	0.0
B76	0.0	-2.0	2.1	0.0	B45	6.8	0.0	0.0	0.0	B642	0.0	0.0	14.3	10.8	B620	0.0	55.0	1.1	0.0
B76	0.1	-2.0	2.1	-0.1	B45	6.8	0.0	0.0	0.0	B642	0.6	0.0	14.3	2.3	B620	1.2	55.0	-1.1	0.0
B76	0.1	-2.0	3.2	-0.1	B46	0.0	0.0	0.0	0.0	B644	0.0	0.0	11.1	4.4	B621	0.0	55.0	1.1	0.0
B76	6.1	-2.0	3.2	-19.3	B46	0.1	0.0	0.0	0.0	B644	0.6	0.0	11.1	-2.3	B621	1.2	55.0	-1.1	0.0
B76	6.1	-4.4	3.2	11.0	B46	0.1	0.0	-18.0	0.0	B645	0.0	0.0	4.6	-0.5	B622	0.0	55.9	1.1	0.0
B76	9.6	-4.4	3.2	0.0	B46	0.1	0.0	-18.0	0.9	B645	0.6	0.0	4.6	-3.3	B622	1.2	55.9	-1.1	0.0
B76	9.6	0.0	0.0	0.0	B46	0.1	0.0	-0.9	0.9	B646	0.0	0.0	-2.8	-1.5	B623	0.0	57.4	1.1	0.0
B76	9.6	0.0	0.0	0.0	B46	2.3	0.0	-0.9	2.9	B646	0.6	0.0	-2.8	0.2	B623	1.2	57.4	-1.1	0.0
B77	0.0	-2.1	1.6	0.0	B46	2.3	0.1	-0.9	-3.0	B647	0.0	0.0	11.8	7.7	B624	0.0	58.6	1.1	0.0
B77	0.1	-2.1	1.6	-0.1	B46	5.5	0.1	-0.9	0.0	B647	0.6	0.0	11.8	0.7	B624	1.2	58.6	-1.1	0.0
B77	0.1	-2.1	2.9	-0.1	B46	5.5	0.0	0.0	0.0	B648	0.0	0.0	5.4	0.8	B625	0.0	59.2	1.1	0.0
B77	6.1	-2.1	2.9	-17.6	B46	5.6	0.0	0.0	0.0	B648	0.6	0.0	5.4	-2.4	B625	1.2	59.2	-1.1	0.0
B77	6.1	-4.4	2.9	10.0	B47	0.0	-20.7	1.0	0.0	B649	0.0	0.0	0.6	-2.6	B626	0.0	27.6	1.1	0.0
B77	9.6	-4.4	2.9	0.0	B47	6.2	-20.7	1.0	-6.0	B649	0.6	0.0	0.6	-2.9	B626	1.2	27.6	-1.1	0.0
B77	9.6	0.0	0.0	0.0	B47	6.2	-39.0	1.0	3.6	B650	0.0	0.0	-3.6	-5.2	B627	0.0	28.6	1.1	0.0
B77	9.6	0.0	0.0	0.0	B47	9.7	-39.0	1.0	0.2	B650	0.6	0.0	-3.6	-3.0	B627	1.2	28.6	-1.1	0.0
B78	0.0	-2.7	1.2	0.0	B47	9.7	-39.0	4.9	0.2	B651	0.0	0.0	-7.7	-7.6	B628	0.0	29.0	1.1	0.0
B78	0.1	-2.7	1.2	-0.1	B47	9.8	-39.0	4.9	0.0	B651	0.6	0.0	-7.7	-3.0	B628	1.2	29.0	-1.1	0.0
B78	0.1	-2.7	2.7	-0.1	B48	0.0	-53.1	7.6	0.0	B652	0.0	0.0	-11.9	-10.0	B630	0.0	28.8	1.1	0.0
B78	6.1	-2.7	2.7	-16.2	B48	0.1	-53.1	7.6	-0.4	B652	0.6	0.0	-11.9	-2.8	B630	1.2	28.8	-1.1	0.0
B78	6.1	-4.4	2.7	9.3	B48	0.1	-53.1	9.4	-0.4	B653	0.0	0.0	-15.6	-9.8	B643	0.0	27.8	1.1	0.0
B78	9.6	-4.4	2.7	0.0	B48	3.6	-53.1	9.4	-33.1	B653	0.6	0.0	-15.6	-0.4	B643	1.2	27.8	-1.1	0.0
B78	9.6	0.0	0.0	0.0	B48	3.6	-154.6	9.4	10.5	B654	0.0	0.0	-18.5	-10.7	B663	0.0	26.2	1.2	0.0
B78	9.6	0.0	0.0	0.0	B48	6.8	-154.6	9.4	-19.6	B654	0.6	0.0	-18.5	0.4	B663	1.3	26.2	-1.2	0.0
B79	0.0	-4.3	1.1	0.0	B48	6.8	-154.6	-6.5	-19.6	B655	0.0	0.0	-17.3	-5.9	B664	0.0	24.1	0.9	0.0
B79	0.1	-4.3	1.1	-0.1	B48	9.8	-154.6	-6.5	0.0	B655	0.6	0.0	-17.3	4.5	B664	1.1	24.1	-0.9	0.0
B79	0.1	-4.3	2.6	-0.1	B49	0.0	0.0	0.0	0.0	B656	0.0	0.0	-10.3	-6.2	B665	0.0	21.7	1.1	0.0
B79	6.1	-4.3	2.6	-15.6	B49	0.1	0.0	0.0	0.0	B656	0.6	0.0	-10.3	0.0	B665	1.2	21.7	-1.1	0.0
B79	6.1	-4.4	2.6	8.9	B49	0.1	0.0	-1.9	0.0	B657	0.0	0.0	0.0	-0.2	B671	0.0	19.2	1.1	0.0
B79	9.6	-4.4	2.6	0.0	B49	2.0	0.0	-1.9	3.7	B657	0.6	0.0	0.0	-0.2	B671	1.2	19.2	-1.1	0.0
B79	9.6	0.0	0.0	0.0	B49	2.0	-46.8	-1.9	-7.8	B658	0.0	0.0	0.0	-0.7	B4	0.1	0.0	48.2	0.0
B79	9.6	0.0	0.0	0.0	B49	6.2	-46.8	-1.9	0.1	B658	0.6	0.0	0.0	-0.7	B4	0.5	0.0	48.2	-19.3
B80	0.0	-7.8	0.7	0.0	B49	6.2	-46.8	2.7	0.1	B659	0.0	0.0	3.2	-2.5	B5	0.0	0.0	-35.6	-28.5
B80	0.1	-7.8	0.7	0.0	B49	6.2	-46.8	2.7	0.0	B659	0.6	0.0	3.2	-4.4	B5	0.8	0.0	-35.6	0.0
B80	0.1	-7.8	2.6	0.0	B50	0.0	0.0	0.0	0.0	B660	0.0	0.0	0.0	-15.9	B6	0.0	14.5	0.0	0.0
B80	6.1	-7.8	2.6	-15.6	B50	0.1	0.0	0.0	0.0	B660	0.6	0.0	0.0	-15.9	B6	1.2	14.5	0.0	0.0
B80	6.1	-4.4	2.6	8.9	B50	0.1	0.0	1.9	0.0	B662	0.0	0.0	-44.7	-52.5	B7	0.1	-19.9	-29.8	0.0
B80	9.6	-4.4	2.6	0.0	B50	2.0	0.0	1.9	-3.7	B662	0.6	0.0	-44.7	-25.7	B7	0.2	-19.9	-29.8	2.4
B80	9.6	0.0	0.0	0.0	B50	2.0	-35.8	1.9	7.8	B666	0.0	0.0	19.2	35.2	B7	0.2	-19.9	-1.7	2.4
B80	9.6	0.0	0.0	0.0	B50	6.2	-35.8	1.9	-0.1	B666	0.6	0.0	19.2	23.7	B7	3.6	-19.9	-1.7	8.4
B81	0.0	-5.3	0.6	0.0	B50	6.2	-35.8	-2.7	-0.1	B667	0.0	0.0	18.1	18.0	B7	3.6	-4.4	-1.7	-6.0
B81	0.1	-5.3	0.6	0.0	B50	6.2	-35.8	-2.7	0.0	B667	0.5	0.0	18.1	9.0	B7	7.1	-4.4	-1.7	0.0
B81	0.1	-5.3	2.5	0.0	B51	0.0	0.0	0.0	0.0	B668	0.0	0.0	17.3	12.9	B7	7.1	0.0	0.0	0.0
B81	6.1	-5.3	2.5	-14.9	B51	0.1	0.0	0.0	0.0	B668	0.6	0.0	17.3	2.5	B7	7.2	0.0	0.0	0.0
B81	6.1	-4.4	2.5	8.5	B51	0.1	0.0	18.0	0.0	B669	0.0	0.0	16.2	9.5	B10	0.1	4.8	-40.6	0.0
B81	9.6	-4.4	2.5	0.0	B51	0.1	0.0	18.0	-0.9	B669	0.6	0.0	16.2	-0.2	B10	0.1	4.8	-40.6	0.6
B81	9.6	0.0	0.0	0.0	B51	0.1	0.0	3.4	-0.9	B670	0.0	0.0	12.9	5.6	B10	0.1	7.0	-3.8	0.6
B81	9.6	0.0	0.0	0.0	B51	2.3	0.0	3.4	-8.5	B670	0.6	0.0	12.9	-2.2	B10	2.9	7.0	-3.8	11.1
B82	0.0	-4.4	-0.7	0.0	B51	2.3	-0.2	3.4	11.0	B701	0.0	0.0	0.0	-0.2	B10	2.9	0.0	-3.8	-7.1
B82	0.1	-4.4	-0.7	0.0	B51	5.6	-0.2	3.4	0.0	B701	0.6	0.0	0.0	-0.2	B10	4.7	0.0	-3.8	0.0
B82	0.1	-4.4	1.8	0.0	B51	5.6	0.0	0.0	0.0	B702	0.0	0.0	0.0	-0.7	B10	4.7	0.0	0.0	0.0
B82	6.1	-4.4	1.8	-10.9	B51	5.6	0.0	0.0	0.0	B702	0.6	0.0	0.0	-0.7	B10	4.8	0.0	0.0	0.0
B82	6.1	-4.4	1.8	6.3	B64	0.0	1.9	0.0	0.0	B703	0.0	0.0	3.2	-4.4	B23	0.1	-24.5	-32.0	0.0
B82	9.6	-4.4	1.8	0.0	B64	1.2	1.9	0.0	0.0	B703	0.6	0.0	3.2	-6.3	B23	0.2	-24.5	-32.0	3.2
B82	9.6	0.0	0.0	0.0	B108	0.0	-0.9	0.0	0.0	B704	0.0	0.0	0.0	-15.9	B23	0.2	-22.4	-0.4	3.2
B82	9.6	0.0	0.0	0.0	B108	1.2	-0.9	0.0	0.0	B704	0.6	0.0	0.0	-15.9	B23	0.3	-22.4	-0.4	3.2
B83	0.0	-1.1	-4.4	0.0	B118	0.0	18.0	0.0	0.0	B705	0.0	0.0	-44.7	-25.7	B23	0.3	-22.4	-0.4	3.2

B83	0.1	-1.1	-4.4	0.2	B118	1.3	18.0	0.0	0.0	B705	0.5	0.0	-44.7	-3.3	B23	3.8	-22.4	-0.4	4.5
B83	0.1	-1.1	-0.2	0.2	B122	0.0	24.9	0.0	0.0	B707	0.0	0.0	19.2	23.7	B23	3.8	-7.8	-0.4	-1.3
B83	6.1	-1.1	-0.2	1.4	B122	1.2	24.9	0.0	0.0	B707	0.5	0.0	19.2	14.1	B23	7.4	-7.8	-0.4	0.0
B83	6.1	-4.4	-0.2	-0.7	B124	0.0	-4.6	0.0	0.0	B708	0.0	0.0	18.1	9.0	B23	7.4	-7.8	0.7	0.0
B83	9.6	-4.4	-0.2	0.0	B124	1.2	-4.6	0.0	0.0	B708	0.6	0.0	18.1	-1.9	B23	7.5	-7.8	0.7	0.0
B83	9.6	0.0	0.0	0.0	B125	0.0	28.1	0.0	0.0	B709	0.0	0.0	17.3	2.5	B2	0.0	0.0	0.0	0.0
B83	9.6	0.0	0.0	0.0	B125	1.4	28.1	0.0	0.0	B709	0.6	0.0	17.3	-7.9	B2	0.0	0.0	0.0	0.0
B84	0.0	18.7	24.0	0.0	B126	0.0	24.7	0.0	0.0	B710	0.0	0.0	16.2	-0.2	B2	0.0	2.1	0.0	0.0
B84	0.1	18.7	24.0	-1.2	B126	1.3	24.7	0.0	0.0	B710	0.6	0.0	16.2	-9.9	B2	0.1	2.1	0.0	0.0
B84	0.1	18.7	-20.2	-1.2	B127	0.0	25.6	0.0	0.0	B712	0.0	0.0	12.9	-2.2	B2	0.1	2.1	0.0	0.0
B84	2.6	18.7	-20.2	50.8	B127	1.2	25.6	0.0	0.0	B712	0.6	0.0	12.9	-10.0	B2	3.6	2.1	0.0	0.0
B84	2.6	18.7	7.4	50.8	B129	0.0	-9.1	0.0	0.0	B730	0.0	0.0	12.3	-2.4	B2	3.6	6.4	0.0	-5.4
B84	6.1	18.7	7.4	25.1	B129	1.1	-9.1	0.0	0.0	B730	0.6	0.0	12.3	-9.8	B2	7.2	6.4	0.0	-5.5
B84	6.1	-4.4	7.4	25.7	B130	0.0	16.9	2.2	0.0	B731	0.0	0.0	10.2	-3.0	B2	7.2	6.4	-54.9	-5.5
B84	9.6	-4.4	7.4	0.0	B130	1.2	16.9	-2.2	0.0	B731	0.6	0.0	10.2	-9.1	B2	7.3	6.4	-54.9	0.0
B84	9.6	0.0	0.0	0.0	B131	0.0	9.2	2.2	0.0	B732	0.0	0.0	8.1	-3.2	B44	0.0	0.0	-75.8	0.0
B84	9.6	0.0	0.0	0.0	B131	1.2	9.2	-2.2	0.0	B732	0.6	0.0	8.1	-8.0	B44	0.5	0.0	-75.8	37.9
B85	0.0	0.0	0.0	0.0	B132	0.0	2.7	2.2	0.0	B733	0.0	0.0	6.0	-3.2	B1	0.0	-2.3	1.1	0.0
B85	0.1	0.0	0.0	0.0	B132	1.2	2.7	-2.2	0.0	B733	0.6	0.0	6.0	-6.7	B1	1.4	-3.7	-1.1	0.0
B85	0.1	0.0	4.6	0.0	B133	0.0	-2.5	2.2	0.0	B734	0.0	0.0	3.9	-2.7	B57	0.0	-6.2	1.1	0.0
B85	3.5	0.0	4.6	-16.0	B133	1.2	-2.5	-2.2	0.0	B734	0.6	0.0	3.9	-5.0	B57	1.4	-7.6	-1.1	0.0
B85	3.5	-4.4	4.6	16.0	B134	0.0	-6.9	2.0	0.0	B735	0.0	0.0	1.8	-1.0	B66	0.0	-10.6	1.1	0.0
B85	7.0	-4.4	4.6	0.0	B134	1.1	-6.9	-2.0	0.0	B735	0.6	0.0	1.8	-2.1	B66	1.4	-12.0	-1.1	0.0
B85	7.0	0.0	0.0	0.0	B135	0.0	-10.7	2.4	0.0	B736	0.0	0.0	6.1	-0.3	B109	0.0	-14.4	1.1	0.0
B85	7.0	0.0	0.0	0.0	B135	1.3	-10.7	-2.4	0.0	B736	0.6	0.0	6.1	-3.9	B109	1.4	-15.8	-1.1	0.0
B86	0.0	0.0	0.0	0.0	B139	0.0	-14.3	2.2	0.0	B737	0.0	0.0	4.0	-0.7	B119	0.0	-24.1	1.1	0.0
B86	0.1	0.0	0.0	0.0	B139	1.2	-14.3	-2.2	0.0	B737	0.6	0.0	4.0	-3.1	B119	1.4	-25.5	-1.1	0.0
B86	0.1	0.0	0.1	0.0	B140	0.0	-17.5	2.2	0.0	B738	0.0	0.0	1.9	-0.1	B123	0.0	7.1	1.1	0.0
B86	3.5	0.0	0.1	-0.3	B140	1.2	-17.5	-2.2	0.0	B738	0.6	0.0	1.9	-1.2	B123	1.2	7.1	-1.1	0.0
B86	3.5	-4.4	0.1	0.3	B141	0.0	-20.4	2.2	0.0	B739	0.0	0.0	0.0	2.4	B128	0.0	27.6	0.0	0.0
B86	7.0	-4.4	0.1	0.0	B141	1.2	-20.4	-2.2	0.0	B739	0.6	0.0	0.0	2.4	B128	1.2	27.6	0.0	0.0
B86	7.0	0.0	0.0	0.0	B142	0.0	-23.1	2.2	0.0	B740	0.0	0.0	-2.3	3.6	B136	0.0	15.9	0.0	0.0
B86	7.0	0.0	0.0	0.0	B142	1.2	-23.1	-2.2	0.0	B740	0.6	0.0	-2.3	5.0	B136	1.1	15.9	0.0	0.0
B87	0.0	0.0	0.0	0.0	B143	0.0	-25.6	2.2	0.0	B741	0.0	0.0	14.3	2.3	B145	0.0	0.0	-0.2	16.5
B87	0.1	0.0	0.0	0.0	B143	1.2	-25.6	-2.2	0.0	B741	0.6	0.0	14.3	-6.3	B145	0.6	0.0	-0.2	16.6
B87	0.1	0.0	-1.7	0.0	B153	0.0	-28.2	2.2	0.0	B742	0.0	0.0	11.1	-2.3	B146	0.0	0.0	-7.3	35.0
B87	3.5	0.0	-1.7	5.8	B153	1.2	-28.2	-2.2	0.0	B742	0.6	0.0	11.1	-9.0	B146	0.6	0.0	-7.3	39.4
B87	3.5	-4.4	-1.7	-5.8	B165	0.0	-30.7	2.2	0.0	B743	0.0	0.0	4.6	-3.3	B147	0.0	0.0	2.0	36.7
B87	7.0	-4.4	-1.7	0.0	B165	1.2	-30.7	-2.2	0.0	B743	0.6	0.0	4.6	-6.1	B147	0.7	0.0	2.0	35.4
B87	7.0	0.0	0.0	0.0	B166	0.0	-32.5	2.2	0.0	B744	0.0	0.0	-2.8	0.2	B149	0.0	0.0	2.0	35.4
B87	7.0	0.0	0.0	0.0	B166	1.2	-32.5	-2.2	0.0	B744	0.6	0.0	-2.8	1.9	B149	0.7	0.0	2.0	34.2
B88	0.0	0.0	0.0	0.0	B167	0.0	-32.3	2.2	0.0	B745	0.0	0.0	11.8	0.7	B150	0.0	0.0	-0.2	16.6
B88	0.1	0.0	0.0	0.0	B167	1.2	-32.3	-2.2	0.0	B745	0.6	0.0	11.8	-6.4	B150	0.6	0.0	-0.2	16.8
B88	0.1	0.0	-2.4	0.0	B168	0.0	-39.7	2.2	0.0	B746	0.0	0.0	5.4	-2.4	B151	0.0	0.0	-7.3	39.4
B88	3.5	0.0	-2.4	8.4	B168	1.2	-39.7	-2.2	0.0	B746	0.6	0.0	5.4	-5.6	B151	0.8	0.0	-7.3	45.2

TABELL A 7 KREFTER PÅ ELEMENTER I DEKKE OVER 1.ETG

# TILLEGG B

## BEVIS AV RASK-METODEN

### 1 FIGURER OG TABELLER

#### Figurer

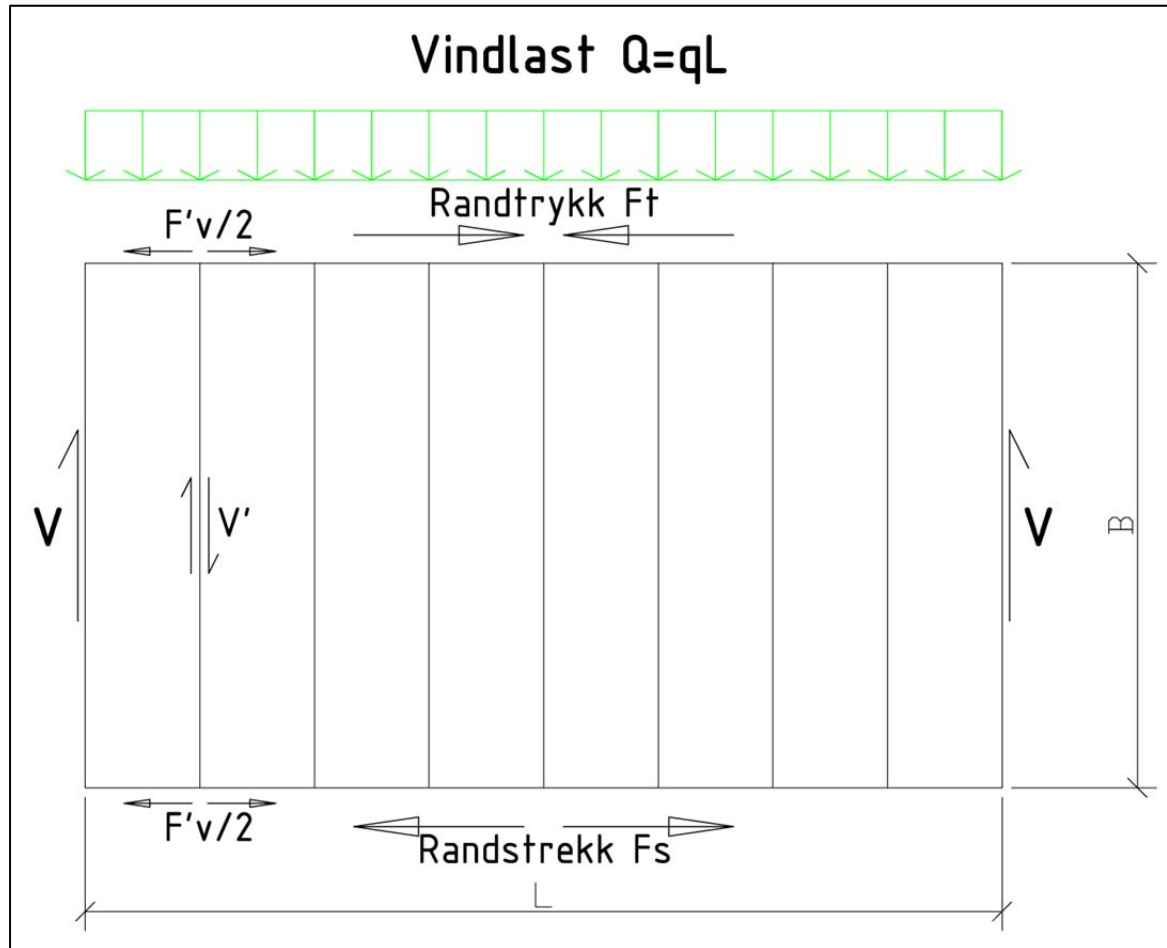
FIGUR B 1 KRAFTMODELL FOR HD-SKIVE .....	2	FIGUR B 5 ELEMENTNUMMER I ETABS .....	9
FIGUR B 2 FUGEFORANKRING .....	5	FIGUR B 6 KRAFT I RANDSTRINGER ALENE.....	12
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FIGUR B 4 LASTER OG LASTVIRKNING PÅ TESTBYGG .....	6	FIGUR B 8 FUGER MED BEHOV FOR FUGEARMERING .....	14

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## 2 TESTOPPSETT

For å finne ut om skivemodell modellert med rammer av staver (RaSk) blir det gjort en sammenlikning mot analytisk beregning av en testskive.



FIGUR B 1 KRAFTMODELL FOR HD-SKIVE

## 3 SKIVETEORI

Vi tar utgangspunkt i generell skiveteori som er presentert i kapittel 5 i Bind 1. Ved hjelp av disse metodene skal det bestemmes randarmering, gjøres skjærkontroll av fuger og forbindelser samt forankring av strekkarmering til elementdekket.

### 3.1 KRAFT OG KRAFTVIRKNING

Kreftene finnes som for en bjelke:

Moment  $M_{max} = \frac{qL^2}{8}$

Med randstrekk  $F_s = \frac{M}{z}$

Skjærkraft  $V_{max} = \frac{qL}{2}$

Som også gir et bidrag på armeringsmengden for randstrekk (sammenholding av «løse» elementer)

Friksjonskraft i fuger  $F_v = \frac{V}{\mu}$

Der:

$\mu$  er friksjonskoeffisient for utstøpingen av fugen – 1.0.

### 3.2 RANDARMERING (RANDSTRINGER)

Armeringsmengde for opptredende moment  $A_M = \frac{F_{sd}}{f_{yd}}$

Randstrekk pga moment  $F_s = \frac{M_d}{z}$

Momentvirkning for vilkårlig x  $M_d = \frac{qLx}{2} - \frac{qx^2}{2} = \frac{qx}{2}(L - x)$

$$\therefore A_M = \frac{qx(L - x)}{2f_{yd}z}$$

Arealtillegg i stål fra skjær  $A_{vt} = \frac{F_v}{f_{yd}}$

som fordeles likt over antall fuger,  $n$ .

Skjærkraft for vilkårlig x  $V_d = q\left(\frac{L}{2} - x\right)$

Armeringsmengde pr fuge fra skjærkraft  $A_V = \frac{A_{vt}}{n} = \frac{q\left(\frac{L}{2} - x\right)}{nf_{yd}\mu} = \frac{q(L - 2x)}{2nf_{yd}\mu}$

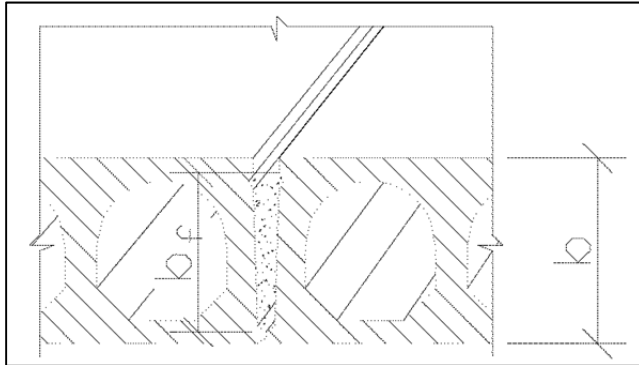
Total armering pr fuge  $A_t = A_M + A_V$

$$A_t = \frac{q}{2f_{yd}} \left( \frac{xL}{z} - \frac{x^2}{z} + \frac{L}{n\mu} - \frac{2x}{n\mu} \right)$$

Største  $A_t$  finnes ved derivasjon med hensyn på  $x$ :  $A_{t,max}$  for  $\frac{dA_t}{dx} = 0$ ;

$$\frac{dA_t}{dx} = \frac{q}{2f_{yd}} \left( \frac{L}{z} - \frac{2x}{z} - \frac{2}{n\mu} \right) = 0 \Rightarrow x = \frac{L}{2} - \frac{z}{n\mu} = \frac{L}{2} - \frac{z}{n}$$

### 3.3 SKJÆRFORBINDELSER



I tillegg til å ha armeringsmengder i randstringerne nok til å oppta skjærkrefter fra fugene, må selve fugens skjærkapasitet kontrolleres.

Skjærspenning langs en fuge pga. opptredende skjærkraft  $V'$  blir  $\tau = \frac{V'_d}{z} b_f \not\leq f_{vd}$

Der

$$b_f = \text{fugehøyde}$$

$$f_{vd} = 0.2N/mm^2 \text{ for glatte fuger}$$

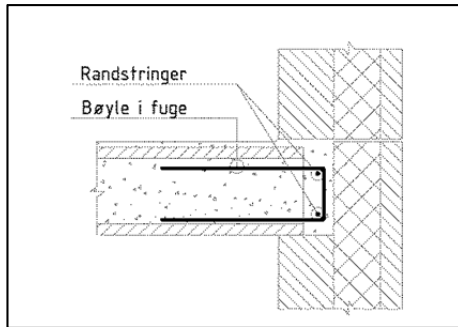
### 3.4 FORANKRING AV STRINGER VED GAVL

Randarmeringen må forankres til det ytterste hulldekket mot gavlen. Dette holder også elementet igjen mot utglidning. Dette gjøres med 90 graders forankringsbøyle fra randarmering og inn i det ytterste elementet.

Kraft i over fugelengden  $F'_{Vd} = \frac{V'_d}{\mu}$

Skjærarmeringsmengde  $A_V = \frac{F'_{Vd}}{f_{yd}n}$

### 3.5 FORANKRING AV STRINGER TIL HD-SKIVE

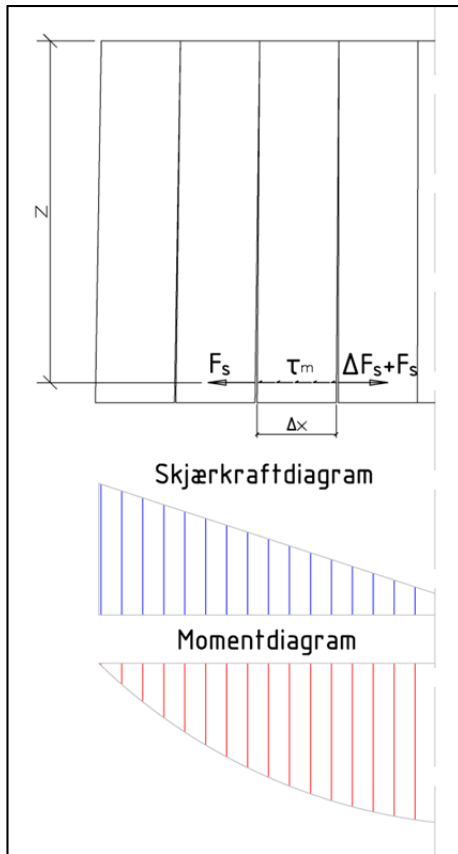


FIGUR B 2 FUGEFORANKRING

Strekkermeringen må forankres til selve dekket. For HD-skiver benyttes bøyer i elementfugene som omfarer randarmeringen.

Den midlere skjærspenningen finnes fra enkel skjærteori som ble introdusert innledningsvis i kapittel 5:

$$\tau_m = \frac{\Delta F_s}{b\Delta x}$$



FIGUR B 3 SKJÆRTILLEGG PÅ RANDARMERING

Kraftøkningen i randstringer

$$\Delta F_s = \frac{\Delta M}{z}$$

Som gir forholdet skjærkraft i et vilkårlig snitt.

$$\frac{\Delta M}{\Delta x} = \frac{dM}{dx} = V =$$

$$\therefore \tau_m = \frac{\Delta M}{b\Delta x z} = \frac{V}{bz}$$

Med hulldekkeelementer som er 1200mm brede får vi horisontal skjærkraft over dekkebredden:

$$V_{hd} = 1.2m \cdot b\tau_m = \frac{1.2V_d}{z} [kN/element]$$

Armeringsmengde

$$A_f = \frac{V_{hd}}{\mu f_{yd}} = \frac{V_{hd}}{f_{yd}}$$

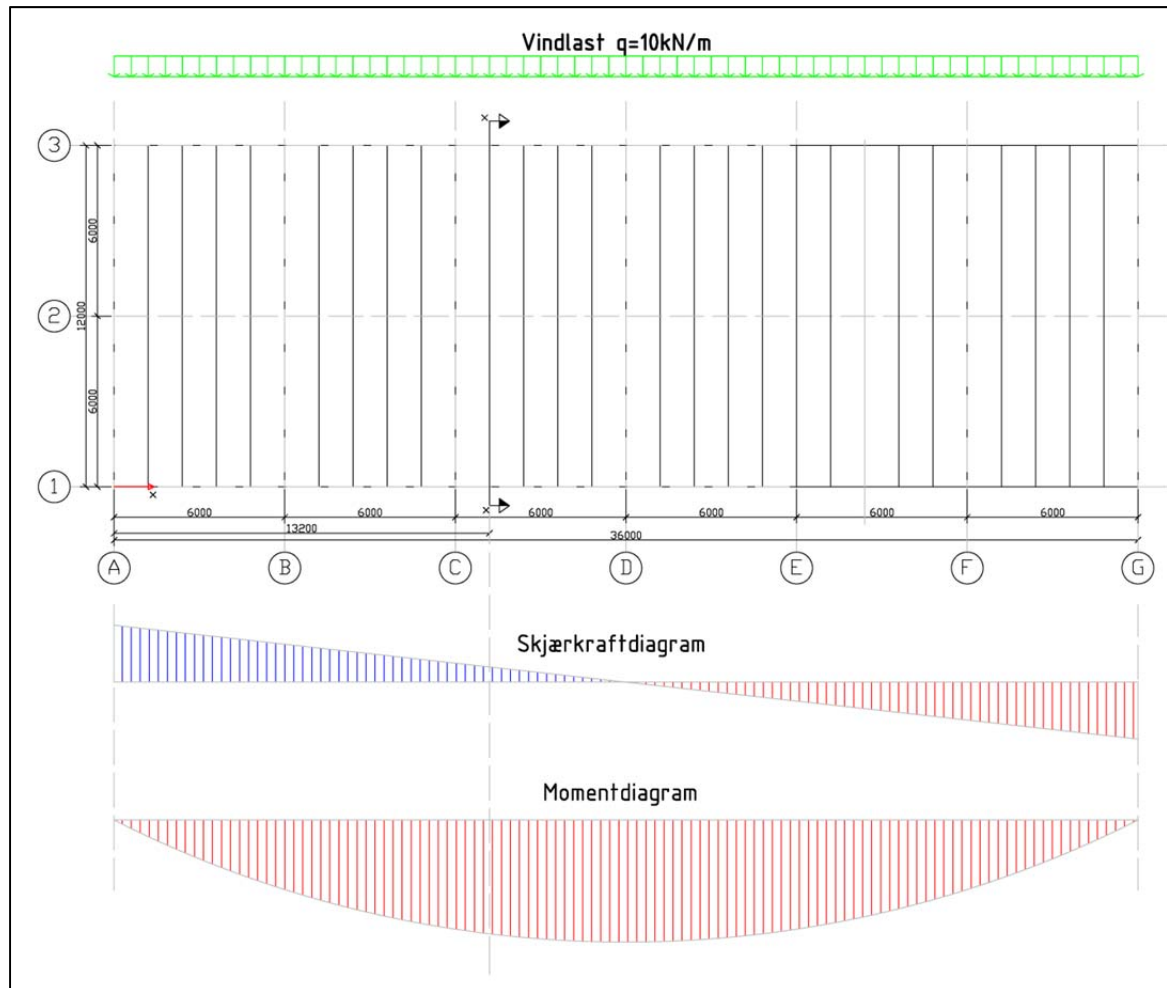
I tillegg vil vindsug på gavlf gi direkte bidrag på armeringsmengden.



## 4 EKSEMPELBYGG: ANALYTISK LØSNING

### 4.1 GEOMETRI OG MATERIALE:

- Hulldekke HD320
- $L=36\text{m}$
- $B=12\text{m}$
- Armering B500NC,  $f_{yk}=500\text{N/mm}^2$
- $Z=0.8B=9.6\text{m}$  (Walraven)



FIGUR B 4 LASTER OG LASTVIRKNING PÅ TESTBYGG

Det regnes uten partialfaktorer.

## 4.2 RANDARMERING (RANDSTRINGER)

Kontrollsnitt for randarmering  $x = \frac{L}{2} - \frac{z}{n} = \frac{36m}{2} - \frac{9.6m}{2} = 13.2m$

Armeringsmengde ved x  $A_t = \frac{10 \times 10^3}{2 \cdot 500} \left( \frac{13.2 \cdot 36}{9.6} - \frac{13.2^2}{9.6} + \frac{36}{2} - \frac{2 \cdot 13.2}{2} \right) = 361.5mm^2$

$$A_t = 2\phi 16 = 402mm^2$$

Armeringsmengde for  $M_{max}$  alene  $A_{tM} = \frac{qL^2}{8zf_{yk}} = \frac{10kN/m \cdot (36m)^2}{8 \cdot 9.6m \cdot 500N/mm^2} = 337.5mm^2$

## 4.3 SKJÆRFORBINDELSER

Skjær i den første fugen  $V_{f1} = q \left( \frac{L}{2} - x \right) = 10 \frac{kN}{m} \left( \frac{36m}{2} - 1.2m \right) = 168kN$

Skjærspenning i fugen  $\tau_{f1} = \frac{V_{f1}}{z b_f} = \frac{168kN}{9.6m \cdot 0.29m} = 0.06 \frac{N}{mm^2} < 0.2 \frac{N}{mm^2}$

Nødvendig randarmering for å holde siste element på plass mot utglidning:

$$A_1 = \frac{V_{f1}}{f_{yk} n} = \frac{168kN}{500N/mm^2 \cdot 2} = 168mm^2$$

Armering pga gavlsug  $A_{sug} = \frac{qB}{n f_{yk}} = \frac{10 \frac{kN}{m} \cdot 12m}{2 \cdot 500 \frac{N}{mm^2}} = 120mm^2$

Total armeringsmengde pr side  $A_V = A_1 + A_{sug} = 288mm^2 = 2\phi 12$

## 4.4 FORANKRING VED GAVL

Opptredende skjærkraft ved gavler  $V = \frac{qL}{2} = \frac{10 \frac{kN}{m} \cdot 36m}{2} = 180kN$

Kraft som må forankres  $F_{G1} = \frac{V}{\mu} = V = 180kN$

Sug på gavl, formfaktor 1.0  $F_{sug} = qB = 10 \frac{kN}{m} \cdot 12m = 120kN$

Det må forankres for  $F_G = 180 + 120 = 300kN$

Regnemessig kapasitet pr. forbindelse er 30kN og avstand mellom forbindelser bør være min. 1m. Da har vi 11 forbindelser til rådighet langs dekkanten og en forbindelse i hver ende av fugen mot naboelementet: 13 forbindelser totalt. Vi trenger kun 10: 8 i sidekant og 2 i fugen.

$$\frac{300kN}{10 \text{ forbindelser}} = 30kN/\text{forbindelse} = OK!$$

#### 4.5 FORANKRING AV STRINGER TIL HD-SKIVE

Det er nødvendig med forankring av randarmering dersom midlere skjærspenning er større enn  $0.5N/mm^2$ :

$$\text{Midlere skjærspenning over HD-bredden } \tau_m = \tau_{f1} = 0.06 \frac{N}{mm^2} > 0.05 \frac{N}{mm^2}$$

Nødvendig forankringsarmering ved skjærfriksjonsberegning blir da

$$A_B = \frac{1.2V}{z} / f_{yk} n = \frac{1.2m \cdot 168kN}{9.6m} / 500 \frac{N}{mm^2} \cdot 2 = 21mm^2$$

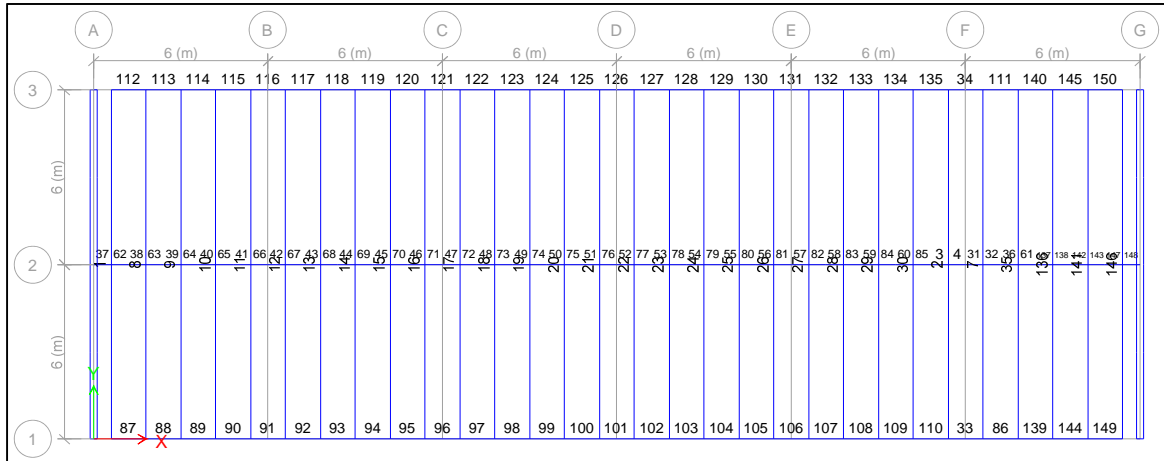
$$\text{Armeringsmengde pga vindsug på lagnvegg: } A_{sug} = q \mu_{\text{overtrykk}} 1.2m / f_{yk} = 10 \frac{kN}{m} \cdot 0.7 \cdot 1.2m / 500 \frac{N}{mm^2} = 16.8mm^2$$

$$\text{Total forankringsarmering } A_3 = A_B + A_{sug} = 37.8mm^2 / fuge = 1\emptyset 10 / 3. fuge$$

## 5 EKSEMPELBYGG: RASK-LØSNING

### 5.1 GEOMETRI OG MATERIALER

Tilsvarende oppsett som i kapittel 4 ovenfor.



FIGUR B 5 ELEMENTNUMMER I ETABS

TABLE: Frame Assignments - Summary			TABLE: Frame Assignments - Summary		
Unique Name	Length	Design Section	Unique Name	Length	Design Section
	mm			mm	
1	12000	HD32	20	12000	HD32
2	12000	HD32	21	12000	HD32
7	12000	HD32	22	12000	HD32
8	12000	HD32	23	12000	HD32
9	12000	HD32	24	12000	HD32
10	12000	HD32	25	12000	HD32
11	12000	HD32	26	12000	HD32
12	12000	HD32	27	12000	HD32
13	12000	HD32	28	12000	HD32
14	12000	HD32	29	12000	HD32
15	12000	HD32	30	12000	HD32
16	12000	HD32	35	12000	HD32
17	12000	HD32	136	12000	HD32
18	12000	HD32	141	12000	HD32
19	12000	HD32	146	12000	HD32

TABELL B 1 HD-STAVER I ETABS

TABLE: Frame Assignments - Summary			TABLE: Frame Assignments - Summary		
Unique Name	Length	Design Section	Unique Name	Length	Design Section
	mm			mm	
85	600	HD32Skjær	61	600	HD32Skjær
3	600	HD32Skjær	62	600	HD32Skjær
4	600	HD32Skjær	63	600	HD32Skjær
31	600	HD32Skjær	64	600	HD32Skjær
32	600	HD32Skjær	65	600	HD32Skjær
36	600	HD32Skjær	66	600	HD32Skjær
37	600	HD32Skjær	67	600	HD32Skjær
38	600	HD32Skjær	68	600	HD32Skjær
39	600	HD32Skjær	69	600	HD32Skjær
40	600	HD32Skjær	70	600	HD32Skjær
41	600	HD32Skjær	71	600	HD32Skjær
42	600	HD32Skjær	72	600	HD32Skjær
43	600	HD32Skjær	73	600	HD32Skjær
44	600	HD32Skjær	74	600	HD32Skjær
45	600	HD32Skjær	75	600	HD32Skjær
46	600	HD32Skjær	76	600	HD32Skjær
47	600	HD32Skjær	77	600	HD32Skjær
48	600	HD32Skjær	78	600	HD32Skjær
49	600	HD32Skjær	79	600	HD32Skjær
50	600	HD32Skjær	80	600	HD32Skjær
51	600	HD32Skjær	81	600	HD32Skjær
52	600	HD32Skjær	82	600	HD32Skjær
53	600	HD32Skjær	83	600	HD32Skjær
54	600	HD32Skjær	84	600	HD32Skjær
55	600	HD32Skjær	137	600	HD32Skjær
56	600	HD32Skjær	138	600	HD32Skjær
57	600	HD32Skjær	142	600	HD32Skjær
58	600	HD32Skjær	143	600	HD32Skjær
59	600	HD32Skjær	147	600	HD32Skjær
60	600	HD32Skjær	148	600	HD32Skjær

TABELL B 2 SKJÆRSTAVER I ETABS

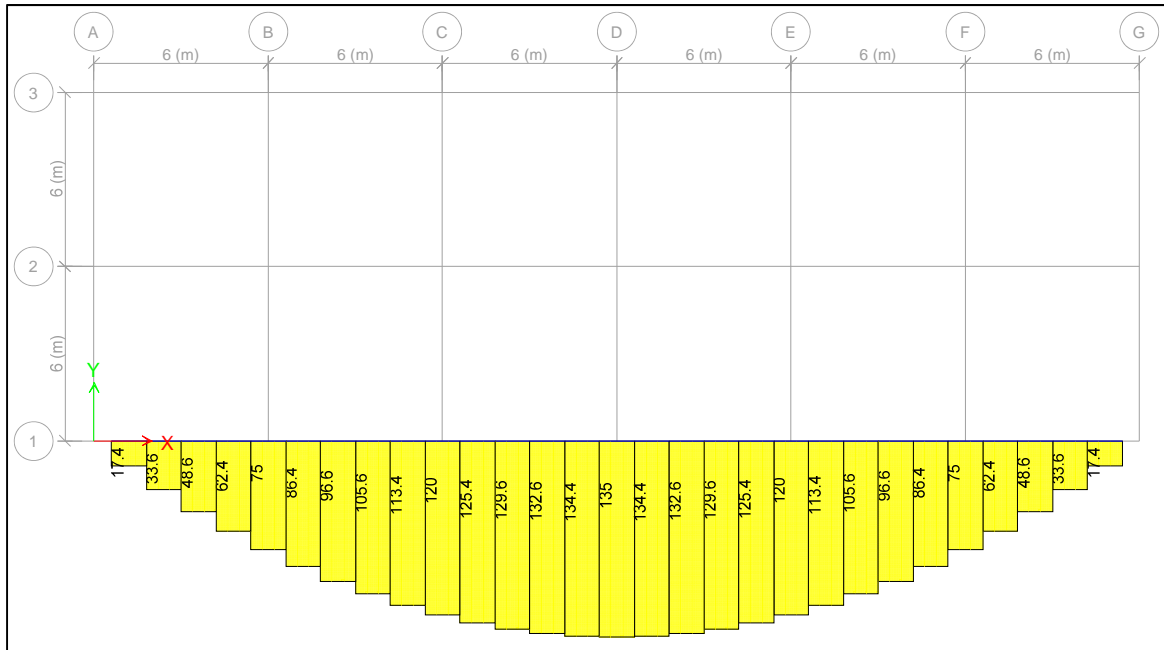
TABLE: Frame Assignments - Summary				TABLE: Frame Assignments - Summary			
Unique Name	Design Type	Lengt	Design Section	Unique Name	Design Type	Lengt	Design Section
		mm				mm	
99	Beam	1200	Stringer	128	Beam	1200	Stringer
98	Beam	1200	Stringer	127	Beam	1200	Stringer
97	Beam	1200	Stringer	126	Beam	1200	Stringer
96	Beam	1200	Stringer	125	Beam	1200	Stringer
95	Beam	1200	Stringer	124	Beam	1200	Stringer
94	Beam	1200	Stringer	123	Beam	1200	Stringer
93	Beam	1200	Stringer	122	Beam	1200	Stringer
92	Beam	1200	Stringer	121	Beam	1200	Stringer
91	Beam	1200	Stringer	120	Beam	1200	Stringer
90	Beam	1200	Stringer	119	Beam	1200	Stringer
89	Beam	1200	Stringer	118	Beam	1200	Stringer
88	Beam	1200	Stringer	117	Beam	1200	Stringer
87	Beam	1200	Stringer	116	Beam	1200	Stringer
86	Beam	1200	Stringer	115	Beam	1200	Stringer
34	Beam	1200	Stringer	114	Beam	1200	Stringer
33	Beam	1200	Stringer	113	Beam	1200	Stringer
150	Beam	1200	Stringer	112	Beam	1200	Stringer
149	Beam	1200	Stringer	111	Beam	1200	Stringer
145	Beam	1200	Stringer	110	Beam	1200	Stringer
144	Beam	1200	Stringer	109	Beam	1200	Stringer
140	Beam	1200	Stringer	108	Beam	1200	Stringer
139	Beam	1200	Stringer	107	Beam	1200	Stringer
135	Beam	1200	Stringer	106	Beam	1200	Stringer
134	Beam	1200	Stringer	105	Beam	1200	Stringer
133	Beam	1200	Stringer	104	Beam	1200	Stringer
132	Beam	1200	Stringer	103	Beam	1200	Stringer
131	Beam	1200	Stringer	102	Beam	1200	Stringer
130	Beam	1200	Stringer	101	Beam	1200	Stringer
129	Beam	1200	Stringer	100	Beam	1200	Stringer

TABELL B 3 STRINGERER I ETABS

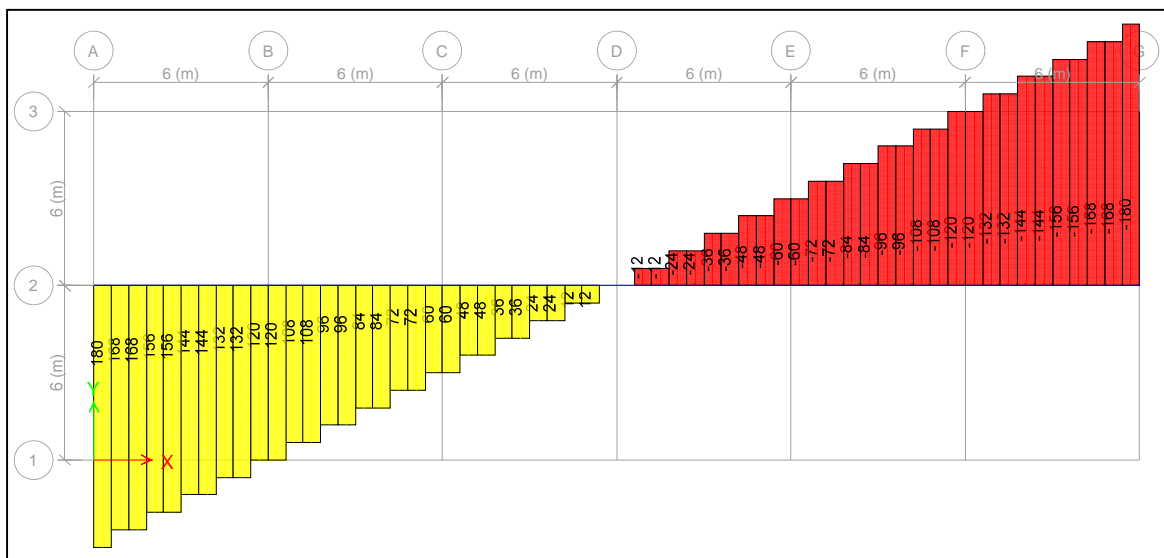
## 5.2 RANDARMERING (RANDSTRINGER)

Krefter på strekkside i skiven som optas i randarmering:

- Akse 1: Kraft i randstringer
- Akse 2: Skjær som superponeres sammen med randstrekk



FIGUR B 6 KRAFT I RANDSTRINGER ALENE



FIGUR B 7 SKJÆRKRAFT I SKJÆRSTAV ALENE

Vi sjekker for  $x=13.2\text{m}$  som funnet i kapittel 4.2 ovenfor, altså den ellefte HD-staven fra akse A:

Fra figurene leser vi av randstrekk = 135kN, skjær = 48kN. Randarmering blir da

$$A_t = 135kN + \frac{48kN}{2} / 500 N/mm^2 = 318mm^2 = 2\phi 16$$

### 5.3 SKJÆRFORBINDELSER

Skjær i den første fugen leses av Figur B 7 Skjærkraft i skjærstaver alene Figur B 7

$$V_{f1} = 168kN$$

Nødvendig randarmering for å holde siste element på plass mot utglidning:

$$A_1 = \frac{V_{f1}}{f_{yk}n} = \frac{168kN}{500N/mm^2 \cdot 2} = 168mm^2$$

Armering pga gavlsug

$$A_{sug} = \frac{qB}{nf_{yk}} = \frac{10 \frac{kN}{m} \cdot 12m}{2 \cdot 500 \frac{N}{mm^2}} = 120mm^2$$

Total armeringsmengde pr side

$$A_V = A_1 + A_{sug} = 288mm^2 = 2\phi 12$$

### 5.4 FORANKRING VED GAVL

Opptredende skjærkraft ved gavler avlest  $V = 180kN$

Kraft som må forankres

$$F_{G1} = \frac{V}{\mu} = V = 180kN$$

Sug på gavl, formfaktor 1.0

$$F_{sug} = qB = 10 \frac{kN}{m} \cdot 12m = 120kN$$

Det må forankres for

$$F_G = 180 + 120 = 300kN$$

$$\frac{300kN}{10 \text{ forbindelser}} = 30kN/\text{forbindelse} = OK!$$

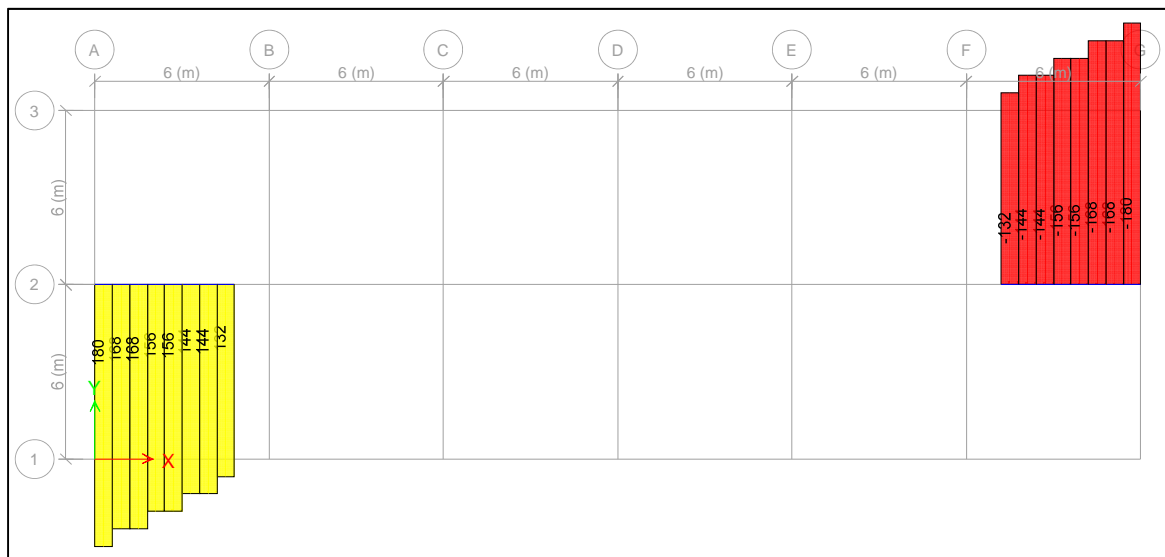


## 5.5 FORANKRING AV STRINGER TIL HD-SKIVE

For å etterkomme kravet om at største skjærspenning uten armering ikke skal være større enn 0.05MPa setter vi opp relasjonen i forhold til skjærkraften:

$$\tau_{f1} = \frac{V_{f1}}{zb_f} < 0.05 \frac{N}{mm^2} \Rightarrow V_{f1} < 0.05zb_f = 0.05 \frac{N}{mm^2} \cdot 0.8 \cdot 12m \cdot 0.29m = 139.2kN$$

Altså vil det ikke være regnemessig behov for forankringsarmering dersom avlest skjærkraft er mindre enn 139.2kN: Området mellom akse B og F vil ikke ha behov for fugearmering



FIGUR B 8 FUGER MED BEHOV FOR FUGEARMERING

## 6 SAMMENLIKNING AV RESULTATER: ANALYTISK VS. RASK

### 6.1 GEOMETRI OG MATERIALE

Global geometri er identisk i de to regnemodellene. Den store forskjellen ligger i at den analytiske modellen regnes med ett element: nemlig én bjelke. RammeSkive-metoden regnes med 148 elementer som representerer skivevirkning.

### 6.2 RANDARMERING (RANDSTRINGER)

Den analytiske regnemodellen forutsetter bjelkevirkning for skiven. Indre momentarm,  $z$ , tilsvarer da samme høyde som i bjelkemekanikk for et betongtverrsnitt, med Walravens foreslåtte forhold;  $z = 0.8B$ .

RaSk-metoden lar kreftene virke i ytterpunktene av stavene, altså blir  $z = B$ .

Dersom vi ser på randarmering pga moment alene ( $V=0$ ) skal denne faktoren finnes igjen:

$$A_{tM,analytisk} = 337.5 \text{ mm}^2$$

$$A_{tM,RaSk} = 135 \text{ kN} / 500 \frac{\text{N}}{\text{mm}^2} = 270 \text{ mm}^2$$

$$\therefore \frac{A_{tM,RaSk}}{A_{tM,analytisk}} = \frac{270}{337.5} = 0.8 \text{ Q.E.D.}$$

### 6.3 SKJÆRFORBINDELSER

Her finnes det at resultatene er identiske: skjærkreftene i RaSk-metoden fordeler seg over lengden på akkurat samme måte som i analytisk bjelketeori; lineært mellom opplagerreaksjonene.

### 6.4 FORANKRING VED GAVL

I og med at denne beregningen henger direkte sammen med hvordan skjærforløpet er, får vi også her identisk resultat i de to metodene.

### 6.5 FORANKRING AV STRINGER TIL HD-SKIVE

Da skjærkreftene leses rett av i ETABS-modellen er det unødvendig å gå veien om skjærspenningsberegning pga. friksjon i fugen. Nødvendig bøylearmering kan finnes direkte ved å lese av kreftene i hver fuge (kraften i skjærstaven tilhørende fugen.)

# TILLEGG C

## GARASJEEFFEKTEN

### 1 FIGURER OG TABELLER

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FIGUR C 2 MOMENT, RASK-METODEN..... 9	FIGUR C 6 SKJÆRKREFTER, RASK-METODEN .... 20
FIGUR C 3 SKJÆRKREFTER, RASK-METODEN .... 10	FIGUR C 7 STRINGERE, RASK-METODEN ..... 20
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TABELL C 2 VERTIKALSKIVER, RASK-METODEN ..... 19	

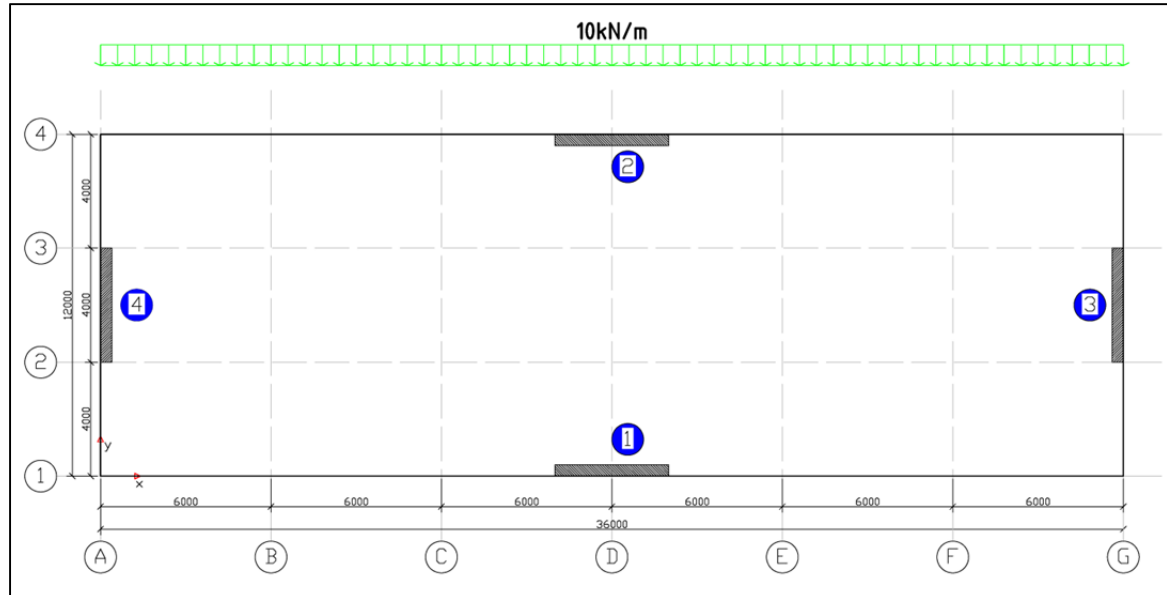
### 2 GENERELT

Som nevnt i kapittel 6.2 i Bind 1 har vertikalskivenes stivhet stor innflytelse på kraftfordelingen i globalanalysen. Vi skal her vise med eksempler hvordan dette slår ut ved å bruke program V-skive fra Sletten Byggdata kontra RaSk-metoden i ETABS.

V-skive benytter tradisjonell håndregningsmetode med uendelig stiv horisontalskive, mens RaSk-metoden med sitt rammebaserte prinsipp danner en deformerbar horisontalskive. Det er derfor forventningen at RaSk-metoden skal kunne dra større nytte av skiver som ikke er stive enn hva V-skive klarer.

### 3 TESTOPPSETT

Vi benytter samme bygningskropp som ble benyttet i beviset for RaSk-metoden i Tillegg B. Vertikalskivene nummereres fra 1-4.



FIGUR C 1 TESTSKIVE FOR STIVHETS BETYDNING

### 4 KJØRING 1: LIKE STIVHETER

Alle fire vertikalskivene modelleres med lik stivhet. For å oppnå dette velges veggtykkelse 200mm og lengde 3m.

#### 4.1 V-SKIVE

Resultater fra V-skive følger på de seks neste sidene.

**Kjøring 1: Like stivheter**

Tittel Identiske vertikalskiver		Side 4-1	
Prosjekt Masteroppgave UiS 2014	Oslo Tillegg C	Sign. OKRP	Dato 08-06-2014

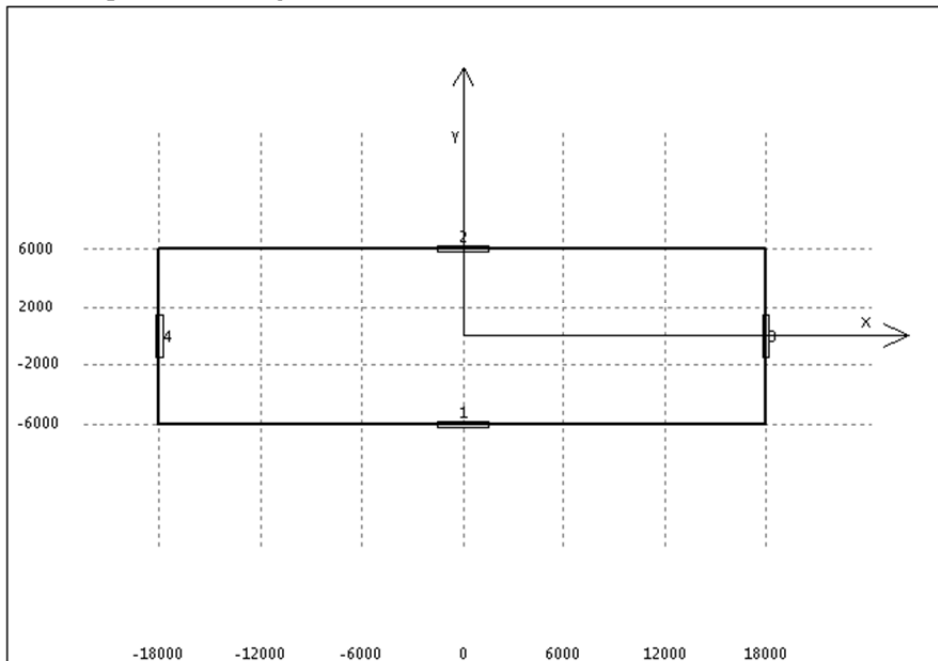
Dataprogram: V-SKIVE versjon 6.1.0 Laget av sivilingeniør Ove Sletten  
 Beregning av forskyvninger er basert på E-modul = 25000 N/mm<sup>2</sup>  
 Stivhetsmatrise for veggskiver: Bjelkemodell er benyttet

Antall etasjer:	1
Antall skiver:	4
Antall lasttilfeller:	1
Antall lastkombinasjoner:	1
Antall utspringer:	0

**Etasjehøyder**

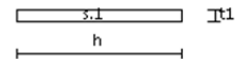
Etasje nr	Etasjehøyde
1	4000

**Plassering av skiver i etasje nr. 1**



**Skive nr 1**

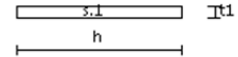
Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	0	1	3000	200
Y (mm)	-6000			
V (grader)	0.0			
Fra etasje	1			
Til etasje	1			



Tittel Identiske vertikalskiver		Side 4-2	
Prosjekt Masteroppgave UiS 2014		Oppgave Tillegg C	Sig. ØKRP
			Dato 08-06-2014

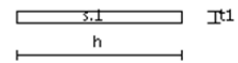
### Skive nr 2

Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	0	1	3000	200
Y (mm)	6000			
V (grader)	0.0			
Fra etasje	1			
Til etasje	1			



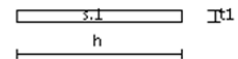
### Skive nr 3

Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	18000	1	3000	200
Y (mm)	0			
V (grader)	90.0			
Fra etasje	1			
Til etasje	1			



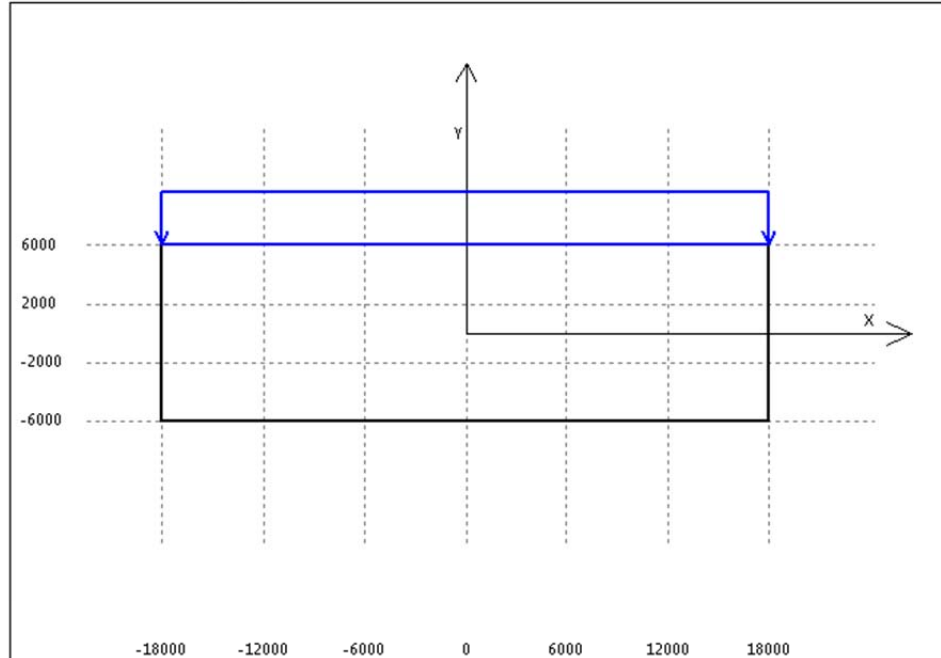
### Skive nr 4

Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	-18000	1	3000	200
Y (mm)	0			
V (grader)	90.0			
Fra etasje	1			
Til etasje	1			



Tittel Identiske vertikalskiver			Side 4-3
Prosjekt Masteroppgave UiS 2014	Oslo Tillegg C	Sign. ØKRP	Dato 08-06-2014

**Lasttilfelle nr 1: Vind -y**



**Lastdata for lasttilfelle nr 1: Vind -y**

Retning	$q$ (kN/m)	$x_1$	$x_2$	$y_1$	$y_2$	Fra etasje	Til etasje
Y	-10.0	-18000	18000	6000	6000	1	1

**Lastkombinasjoner**

Lastkombinasjon	Lasttilfelle nr
1	1

**Lastfaktorer for horisontallast**

Lasttilfelle	Bruksgrense	Bruddgrense
1 Vind -y	1	1.5

**Påført vertikallast (kN)**

Skive nr	over etasje nr 1	
	egenvekt	nyttelast
1	0	0
2	0	0
3	0	0
4	0	0

Tittel Identiske vertikalskiver			Side 4-4
Prosjekt Masteroppgave UiS 2014		Ordre Tillegg C	Sign. OKRP
			Dato 08-06-2014

**Lastfaktorer for vertikallast**

	Bruksgrense	Bruddgrense
Egenvekt	1.00	1.20
Nyttelast	1.00	1.50

Egenvekt vertikalskiver: 2500 kg/m<sup>3</sup>

**Beregningsresultater**

**Aksialkraft i skive nr 1 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	60	0	60	72	0	72

**Aksialkraft i skive nr 2 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	60	0	60	72	0	72

**Aksialkraft i skive nr 3 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	60	0	60	72	0	72

**Aksialkraft i skive nr 4 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	60	0	60	72	0	72

**Lastkombinasjon nr 1 Horisontale tilleggskrefter på grunn av utbøyning**

Px(kN)	Py(kN)	X(mm)	Y(mm)	Etasje nr	Skive nr
0.0	0.0	0	-6000	1	1
0.0	0.0	0	6000	1	2
0.0	0.0	18000	0	1	3
0.0	0.0	-18000	0	1	4

**Lastkombinasjon nr 1 Bruksgrense**

Etasje nr	Lastvektor			Forskyvningsvektor		
	Rx(kN)	Ry(kN)	Rz(kNm)	Vx(mm)	Vy(mm)	Vz(grader)
1	0.0	-360.0	0.0	0	0	0.0000

**Lastkombinasjon nr 1 : Skive nr 1 Bruksgrense**

H(kN)	Forskyvning(mm)	Skjærkraft(kN)	Moment(kNm)
0.0	0.0	0.0	0.0

1.etg

**Lastkombinasjon nr 1 : Skive nr 2 Bruksgrense**

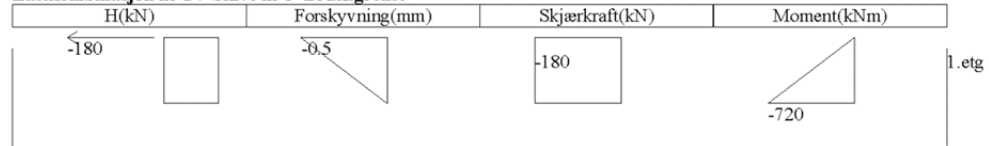
H(kN)	Forskyvning(mm)	Skjærkraft(kN)	Moment(kNm)
0.0	0.0	0.0	0.0

1.etg

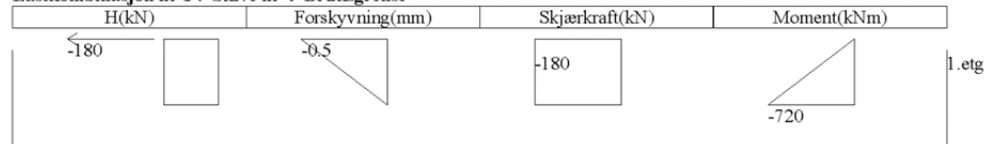


Tittel Identiske vertikalskiver		Side 4- 5	
Prosjekt Masteroppgave UiS 2014		Ordrer Tillegg C	Sign. ØKRP
		Dato 08-06-2014	

**Lastkombinasjon nr 1 : Skive nr 3 Bruksgrense**



**Lastkombinasjon nr 1 : Skive nr 4 Bruksgrense**



**Maksimum og minimum snittkrefter for plane skiver**

**Skive nr 1 Bruksgrense**

Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.talverdi	Maks.talverdi
1	60	60	0	0

**Skive nr 2 Bruksgrense**

Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.talverdi	Maks.talverdi
1	60	60	0	0

**Skive nr 3 Bruksgrense**

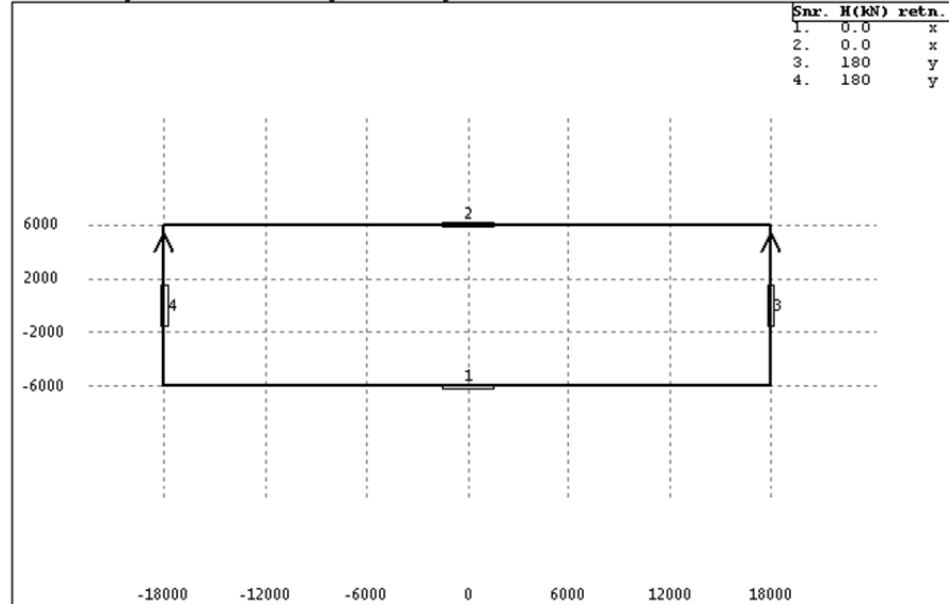
Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.talverdi	Maks.talverdi
1	60	60	-720	-180

**Skive nr 4 Bruksgrense**

Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.talverdi	Maks.talverdi
1	60	60	-720	-180

Tittel Identiske vertikalskiver		Side 4-6	
Prosjekt Masteroppgave Uis 2014		Oslo Tillegg C	Sig OKRP
		Dato 08-06-2014	

**Lastkombinasjon nr 1: Dekke over etasje nr 1: Reaksjonskrefter fra vertikalskiver**



**Maksimum snittkrefter i dekker**

**Dekke nr 1 Bruksgrense**

Modullinjer i Y-retning			Modullinjer i X-retning		
X-koord. (mm)	Moment (kNm) Maks.talverdi	Skjærkraft (kN) Maks.talverdi	Y-koord. (mm)	Moment (kNm) Maks.talverdi	Skjærkraft (kN) Maks.talverdi
-18000	0	0	-6000	0	0
-12000	900	120	-2000	0	0
-6000	1440	60	2000	0	0
0	1620	0	6000	0	0
6000	1440	-60			
12000	900	-120			
18000	0	-180			

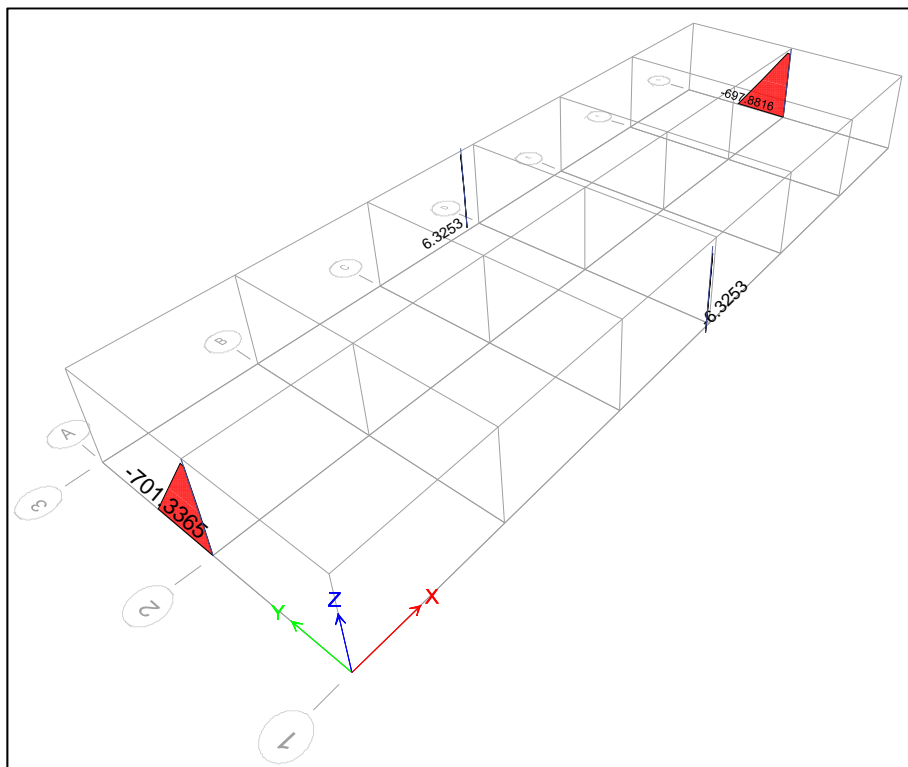
## 4.2 RASK-METODEN I ETABS

Tilsvarende kjøring gjort i ETABS.

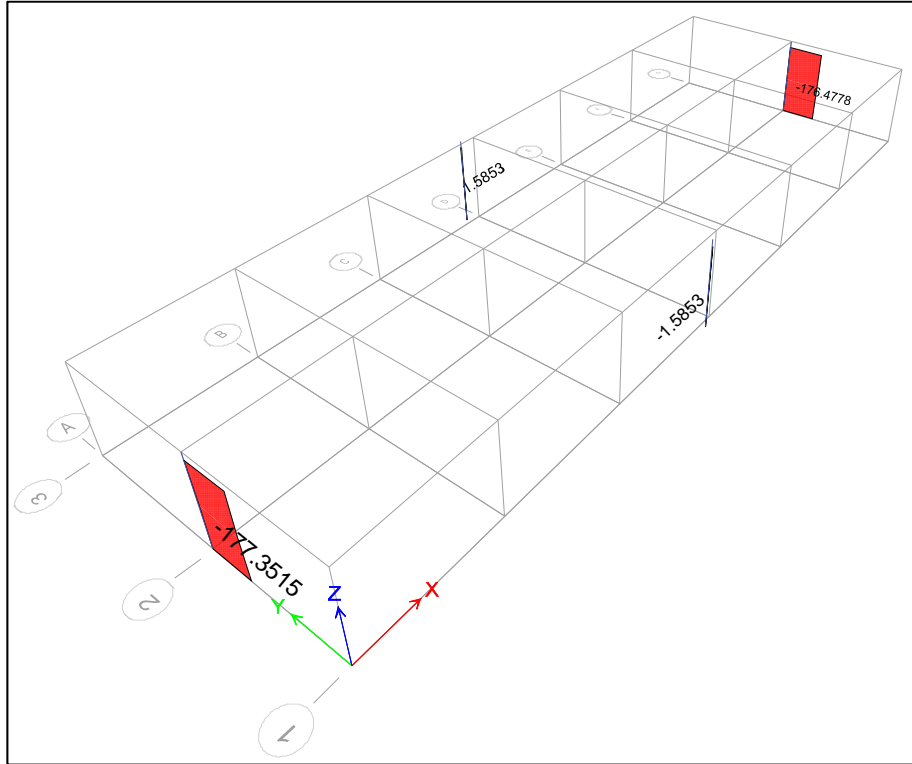
Kraftvirkninger på vertikalskiver:

Column	P	V2	M3
	kN	kN	kN-m
1	-123.3	-1.6	-6.3
2	123.5	1.6	6.3
3	0.0	-176.5	-697.9
4	0.0	-177.4	-701.3

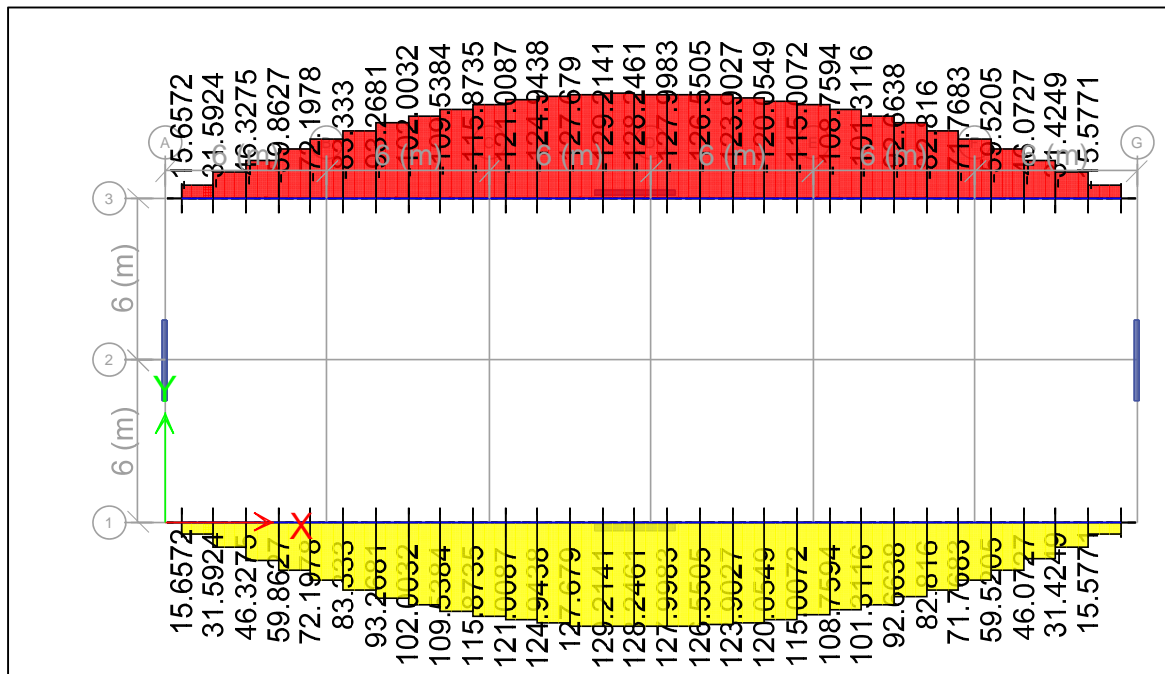
TABELL C 1 VERTIKALSKIVER, RASK-METODEN



FIGUR C 2 MOMENT, RASK-METODEN



FIGUR C 3 SKJÆRKRFTER, RASK-METODEN



FIGUR C 4 STRINGERE, RASK-METODEN

### 4.3 KJØRING 1: RESULTATBETRAKTNINGER

Sammenlikning av resultater viser at det er svært liten forskjell i oppførselen til skivene – som forventet

I RaSk-modellen får skive 1 og 2 ca. 6kNm i bidrag. Dette avlaster gavlene 3 og 4 slik at disse får omtrent 700kNm i momentbelastning. V-skive legger hele belastningen på gavlene og gir følgelig 720kNm i moment – mindre enn 3 % forskjell.

En kjapp håndregning bekrefter resultatene:

$$\text{Skjærkrefter på gavler/opplagerreaksjoner } R_3 = R_4 = \frac{qL}{2} = \frac{10 \frac{\text{kN}}{\text{m}} \cdot 36\text{m}}{2} = 180\text{kN}$$

$$\text{Momentvirkning på gavler } M_3 = M_4 = RH = 180\text{kN} \cdot 4\text{m} = 720\text{kNm}$$

Håndregning stemmer altså 100 % overens med V-skive, og gir et forventet avvik i forhold til RaSk-metoden som klarer å aktivisere langveggene.

Krefter i horisontalskive:

Største moment funnet i V-skive midt på lengden L:

$$M_{max} = 1620\text{kNm}$$

Tilsvarende stringerkraft

$$F_{S,V-skive} = \frac{M_{max}}{z} = \frac{1620\text{kNm}}{0.8 \cdot 12\text{m}} = 168.75\text{kN}$$

Største avleste kraft i RaSk-metoden

$$F_{S,RaSk} = 129.2\text{kN}$$

Forhold mellom strekkrefter

$$\frac{F_{S,RaSk}}{F_{S,V-skive}} = \frac{129.2}{168.75} = 0.771 \cong 0.8$$

som bevist i kap5 i tillegg B.

<sup>1</sup> Bidrag fra langvegger i RaSk-modellen gir dette avviket på 4 %

## 5 KJØRING 2: STIVE SKIVER 1,2 OG 4

Stivheten økes i skive 1, 2 og 4 ved å øke lengden til 12m. Minner om at stivhet øker i tredje potens ved økning av vegg lengden:

Stivheten til en skive  $I_{skive} = \frac{bB^3}{12}$

Slik at økningen da blir  $\frac{12^3}{3^3} = \left(\frac{12}{3}\right)^3 = 4^3 = 64$

12m skive er 64 ganger stivere enn 3m skive.

### 5.1 V-SKIVE

Resultater fra V-skive følger på de seks neste sidene.

**Kjøring 2: Ulike stivheter**

Tittel Vertikalskive 4 med stor stivhet		Side 5-1	
Prosjekt Masteroppgave UiS 2014	Oslo Tillegg C	Sjef ØKRP	Dato 08-06-2014

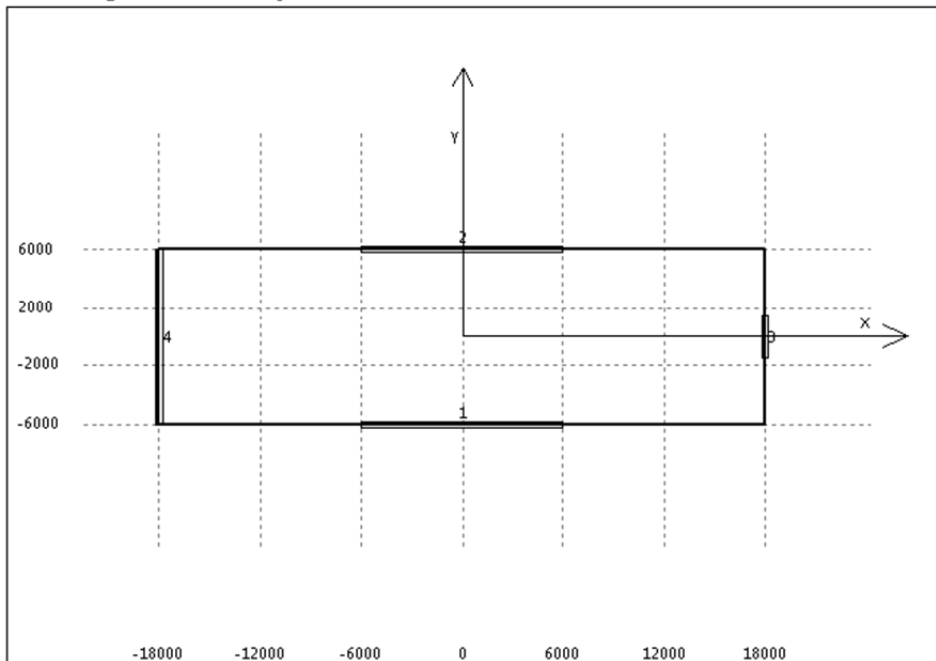
Dataprogram: V-SKIVE versjon 6.1.0 Laget av sivilingeniør Ove Sletten  
 Beregning av forskyvninger er basert på E-modul = 25000 N/mm<sup>2</sup>  
 Stivhetsmatrise for veggskiver: Bjelkemodell er benyttet

Antall etasjer:	1
Antall skiver:	4
Antall lasttilfeller:	1
Antall lastkombinasjoner:	1
Antall utspringer:	0

**Etasjehøyder**

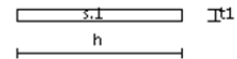
Etasje nr	Etasjehøyde
1	4000

**Plassering av skiver i etasje nr. 1**



**Skive nr 1**

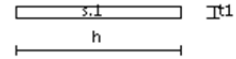
Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	0	1	12000	200
Y (mm)	-6000			
V (grader)	0.0			
Fra etasje	1			
Til etasje	1			



Tittel Vertikalskive 4 med stor stivhet			Side 5-2
Prosjekt Masteroppgave UiS 2014	Oslo Tillegg C	Sign. ØKRP	Dato 08-06-2014

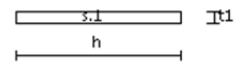
### Skive nr 2

Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	0	1	12000	200
Y (mm)	6000			
V (grader)	0.0			
Fra etasje	1			
Til etasje	1			



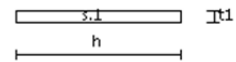
### Skive nr 3

Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	18000	1	3000	200
Y (mm)	0			
V (grader)	90.0			
Fra etasje	1			
Til etasje	1			



### Skive nr 4

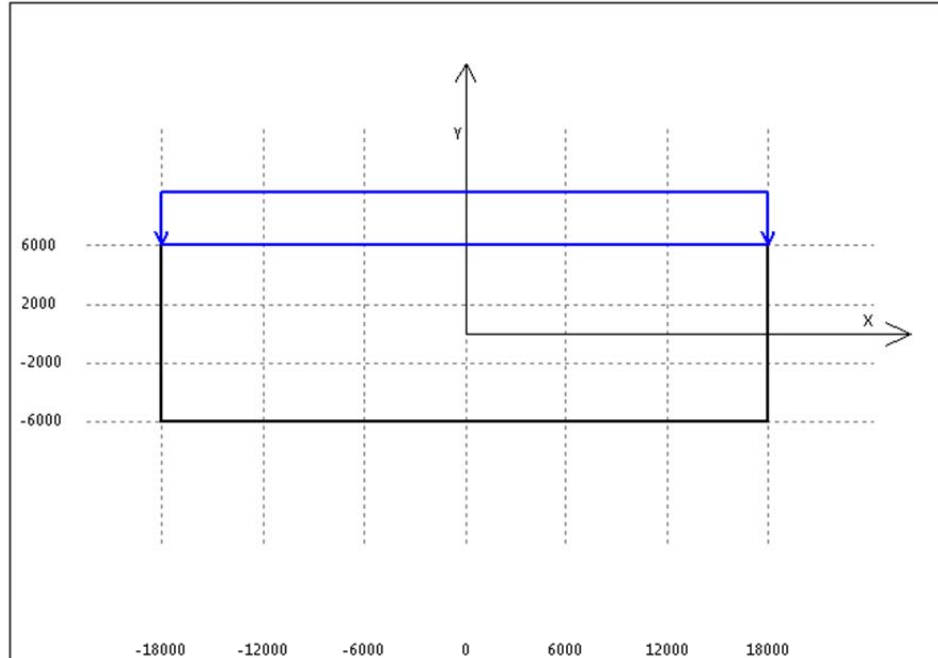
Posisjonsdata:		Etasje	h(mm)	t1(mm)
x (mm)	-18000	1	12000	200
Y (mm)	0			
V (grader)	90.0			
Fra etasje	1			
Til etasje	1			





Tittel Vertikalskive 4 med stor stivhet			Side 5-3
Prosjekt Masteroppgave UiS 2014	Oslo Tillegg C	Sjef ØKRP	Dato 08-06-2014

**Lasttilfelle nr 1: Vind -y**



**Lastdata for lasttilfelle nr 1: Vind -y**

Retning	$q$ (kN/m)	$x_1$	$x_2$	$y_1$	$y_2$	Fra etasje	Til etasje
Y	-10.0	-18000	18000	6000	6000	1	1

**Lastkombinasjoner**

Lastkombinasjon	Lasttilfelle nr
1	1

**Lastfaktorer for horisontallast**

Lasttilfelle	Bruksgrense	Bruddgrense
1 Vind -y	1	1.5

**Påført vertikallast (kN)**

Skive nr	over etasje nr 1	
	egenvekt	nyttelast
1	0	0
2	0	0
3	0	0
4	0	0

Titel Vertikalskive 4 med stor stivhet			Side 5- 4
Prosjekt Masteroppgave UiS 2014	Ordre Tillegg C	Sign. ØKRP	Dato 08-06-2014

**Lastfaktorer for vertikallast**

	Bruksgrense	Bruddgrense
Egenvekt	1.00	1.20
Nyttelast	1.00	1.50

Egenvekt vertikalskiver: 2500 kg/m<sup>3</sup>

**Beregningsresultater**

**Aksialkraft i skive nr 1 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	240	0	240	288	0	288

**Aksialkraft i skive nr 2 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	240	0	240	288	0	288

**Aksialkraft i skive nr 3 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	60	0	60	72	0	72

**Aksialkraft i skive nr 4 (kN)**

Etasje nr	Bruksgrense			Bruddgrense		
	Egenvekt	Nyttelast	Totallast	Egenvekt	Nyttelast	Totallast
1	240	0	240	288	0	288

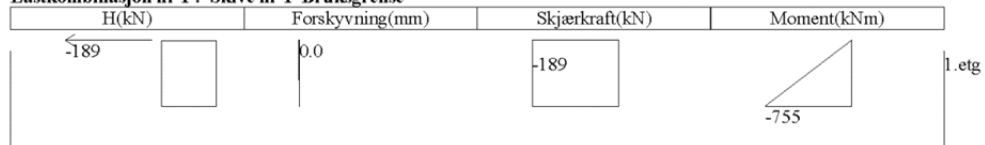
**Lastkombinasjon nr 1 Horisontale tilleggskrefter på grunn av utbøyning**

Px(kN)	Py(kN)	X(mm)	Y(mm)	Etasje nr	Skive nr
0.0	0.0	0	-6000	1	1
0.0	0.0	0	6000	1	2
0.0	0.0	18000	0	1	3
0.0	0.0	-18000	0	1	4

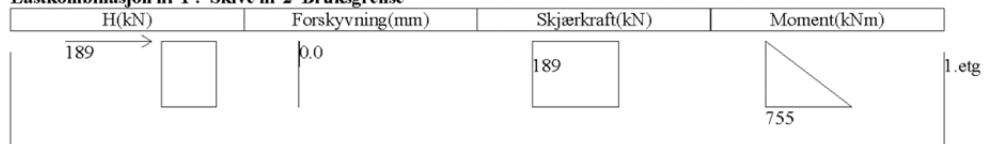
**Lastkombinasjon nr 1 Bruksgrense**

Etasje nr	Lastvektor			Forskyvningsvektor		
	Rx(kN)	Ry(kN)	Rz(kNm)	Vx(mm)	Vy(mm)	Vz(grader)
1	0.0	-360.0	0.0	0	0	-0.0004

**Lastkombinasjon nr 1 : Skive nr 1 Bruksgrense**

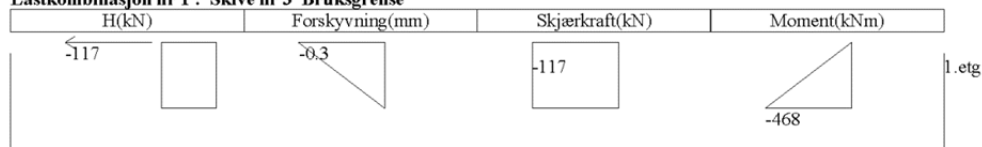


**Lastkombinasjon nr 1 : Skive nr 2 Bruksgrense**

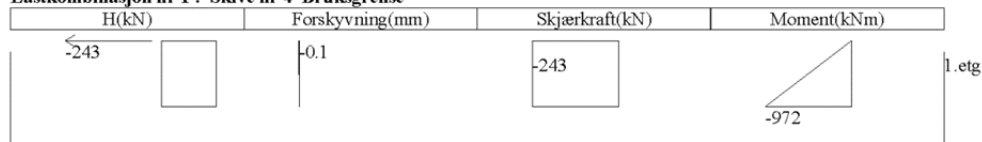


Tittel Vertikalskive 4 med stor stivhet		Side 5- 5	
Prosjekt Masteroppgave UiS 2014	Ordre Tillegg C	Sign. ØKRP	Dato 08-06-2014

**Lastkombinasjon nr 1 : Skive nr 3 Bruksgrense**



**Lastkombinasjon nr 1 : Skive nr 4 Bruksgrense**



**Maksimum og minimum snittkrefter for plane skiver**

**Skive nr 1 Bruksgrense**

Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.tallverdi	Maks.tallverdi
1	240	240	-755	-189

**Skive nr 2 Bruksgrense**

Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.tallverdi	Maks.tallverdi
1	240	240	755	189

**Skive nr 3 Bruksgrense**

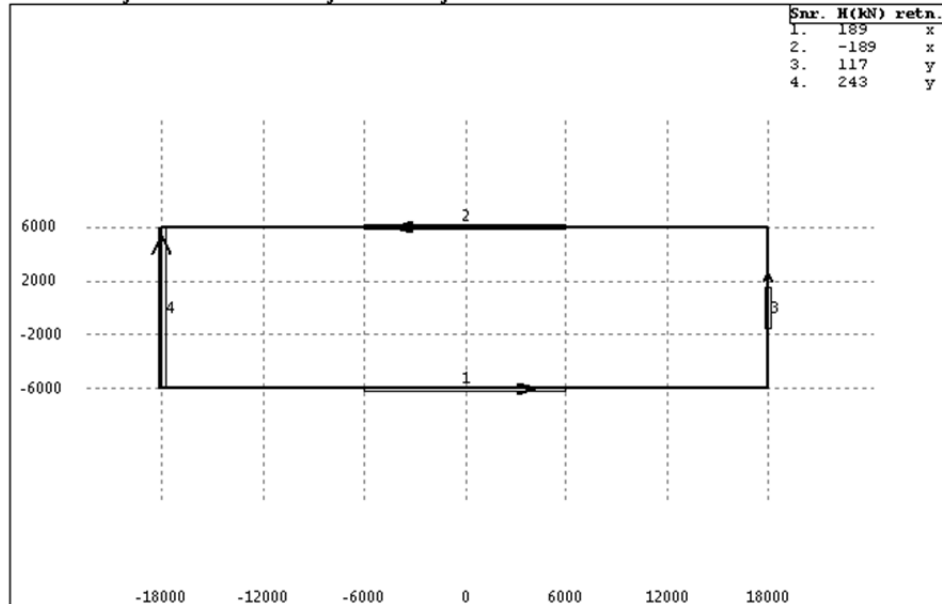
Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.tallverdi	Maks.tallverdi
1	60	60	-468	-117

**Skive nr 4 Bruksgrense**

Etasje nr	Aksialkraft (kN)		Moment (kNm)	Skjærkraft (kN)
	Maks.	Min.	Maks.tallverdi	Maks.tallverdi
1	240	240	-972	-243

Tittel Vertikalskive 4 med stor stivhet		Side 5-6	
Prosjekt Masteroppgave Uis 2014		Oslo Tillegg C	Sig OKRP
		Dato 08-06-2014	

**Lastkombinasjon nr 1: Dekke over etasje nr 1: Reaksjonskrefter fra vertikalskiver**



**Maksimum snittkrefter i dekker**

**Dekke nr 1 Bruksgrense**

Modulinjer i Y-retning			Modulinjer i X-retning		
X-koord. (mm)	Moment (kNm) Maks.talverdi	Skjærkraft (kN) Maks.talverdi	Y-koord. (mm)	Moment (kNm) Maks.talverdi	Skjærkraft (kN) Maks.talverdi
-18000	0	0	-6000	0	0
-12000	1277	183	-2000	-703	189
-6000	2195	123	2000	703	189
0	1620	63	6000	0	189
6000	685	3			
12000	523	-57			
18000	0	-117			

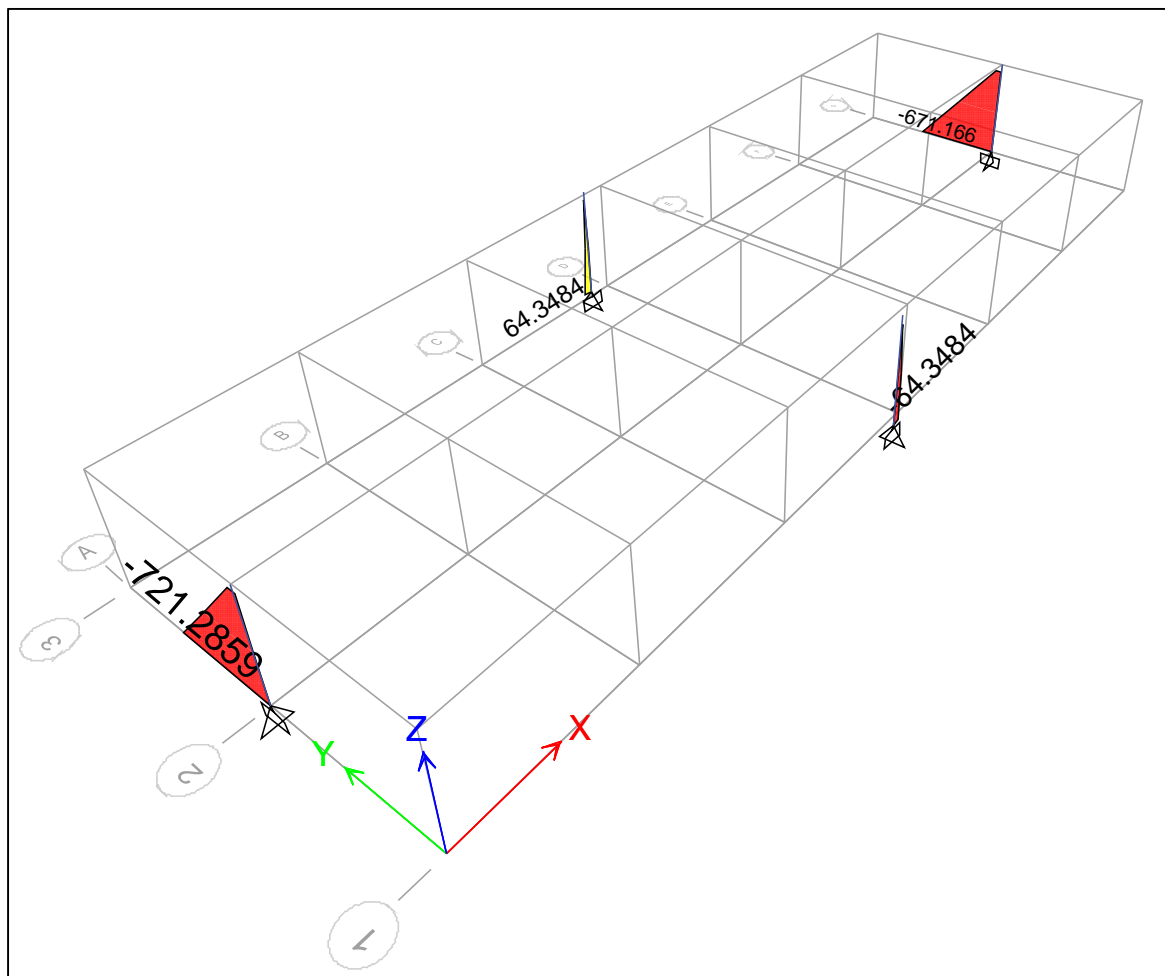
## 5.2 RASK-METODEN I ETABS

Tilsvarende kjøring gjort i ETABS.

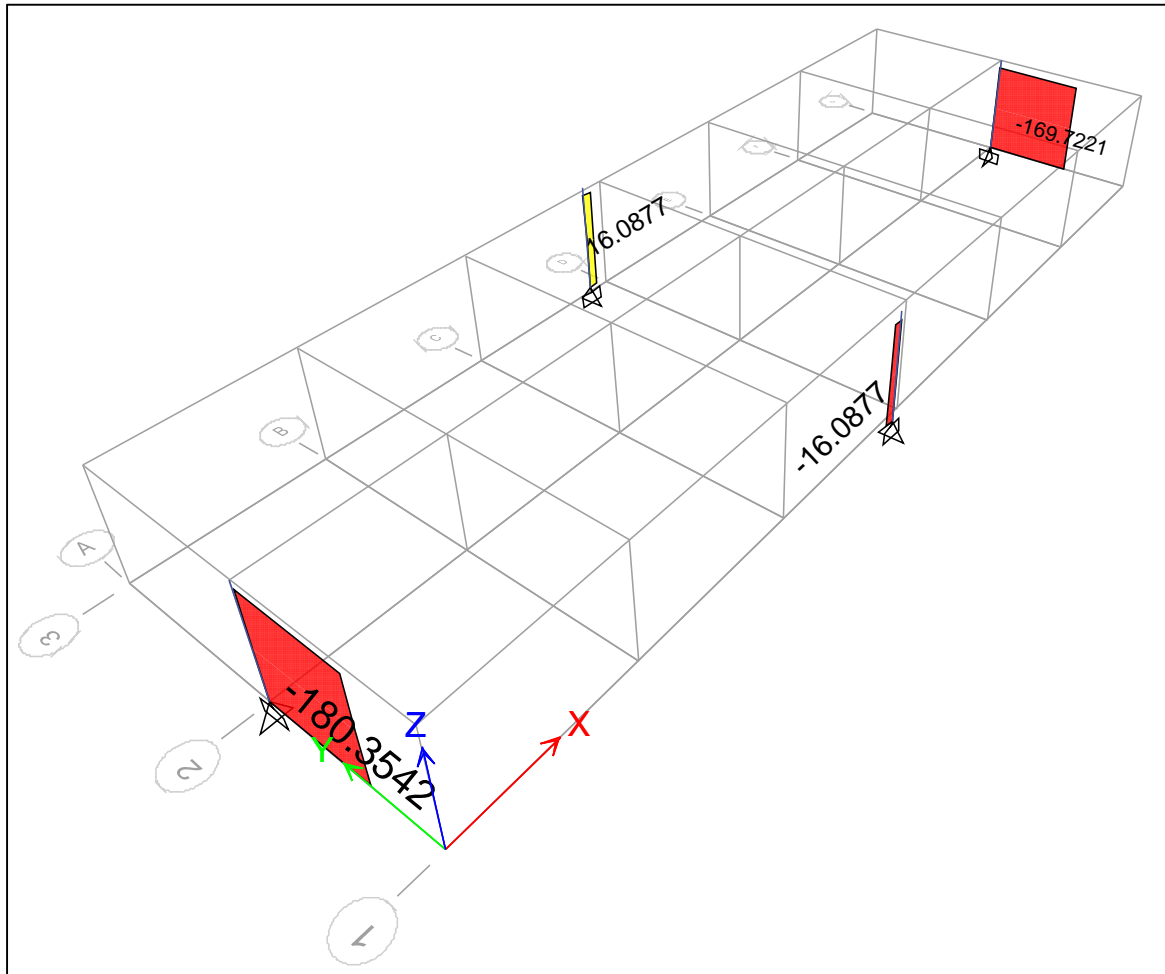
Kraftvirkninger på vertikalskiver:

Column	P	V2	M3
	kN	kN	kN-m
1.0	-198.3	-16.1	-64.3
2.0	198.6	16.1	64.3
3.0	0.0	-169.7	-671.2
4.0	0.0	-180.4	-721.3

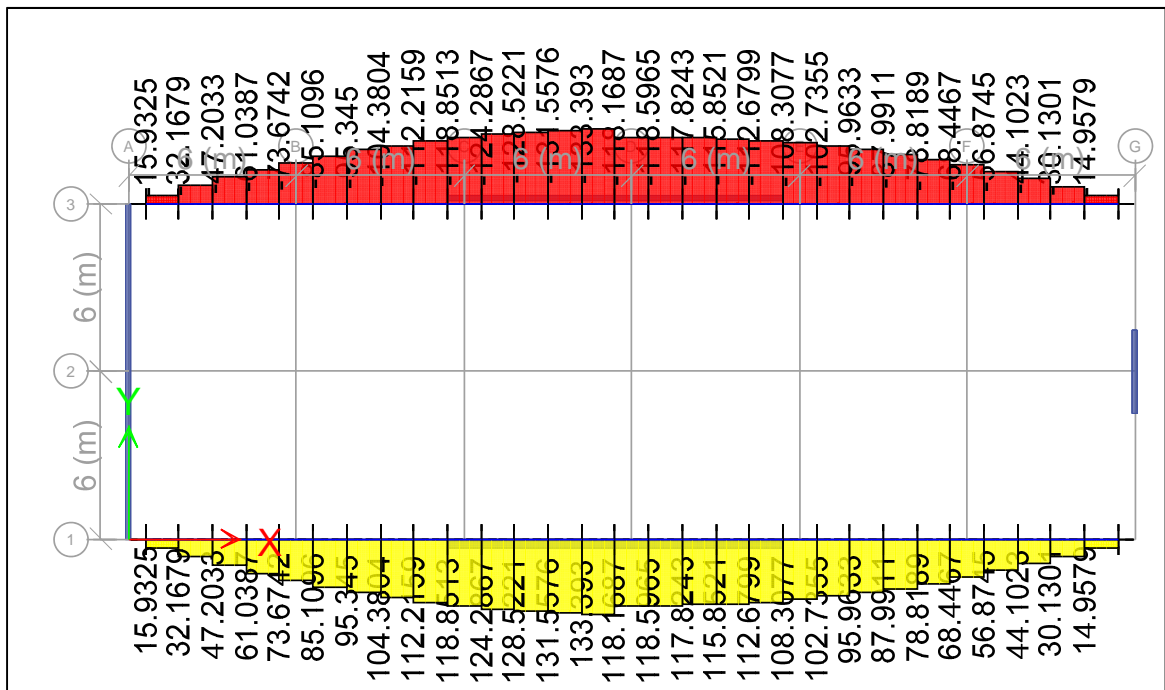
TABELL C 2 VERTIKALSKIVER, RASK-METODEN



FIGUR C 5 MOMENT, RASK-METODEN



FIGUR C 6 SKJÆRKRFTER, RASK-METODEN



FIGUR C 7 STRINGERE, RASK-METODEN

### 5.3 KJØRING 2: RESULTATBETRAKTNINGER

Langveggene, som i kjøring 1 ikke var belastet i V-skive, har nå fått hele 755kNm i momentbelastning. En økning som selvsagt er uendelig. RaSk-metoden gir langveggene ca. 64kNm i moment: ti ganger mer enn i kjøring 1.

Ved kjøring 2 har altså tradisjonell regnemodell overført mer enn 11 ganger mer moment til langveggene enn hva RaSk-metoden gjør – substansielt mye mer.

Dette er garasjeeffekten som slår inn for tradisjonell regnemodell.

Det matematisk pene uttrykket som ga 720kNm i hver av gavlene kan nå ikke brukes. V-skive har nå fordelt mesteparten av momentet til venstre gavl; skive 4. Denne gavlen må nå ta 972kNm, mot 468kNm i motsatt gavl: altså 500 kNm i forskjell.

RaSk-metoden gir 721kNm mot 671kNm respektivt – bare 50kNm i forskjell. Gavl 4 har faktisk nesten identisk belastning som matematikken gir, mens langveggene avlaster skive 3.

Største moment funnet i V-skive

$$M_{max} = 2195kNm$$

Tilsvarende stringerkraft

$$F_{s,V-skive} = \frac{M_{max}}{z} = \frac{2195kNm}{0.8 \cdot 12m} = 228.6kN$$

Største avleste kraft i RaSk-metoden

$$F_{s,RaSk} = 133.4kN$$

Forhold mellom strekkrefter

$$\frac{F_{s,RaSk}}{F_{s,V-skive}} = \frac{133.4}{228.6} = 0.58 \neq 0.8$$

Altså har de to regnemodellene skilt lag.

## 6 KONKLUSJON

Konklusjonen som kan trekkes er at tradisjonell regnemodell sier at dersom man øker stivheten til veggene vil dette være ugunstig for byggets stabilitet. Dette faller på sin egen urimelighet: Ved å forsterke en vegg kan man aldri komme i fare for at de andre veggene bryter sammen, eller at horisontalskiven kollapser. Denne problemstillingen ivaretas av RaSk-metoden. Det er fordi horisontalskiven her er så myk at den vil legge seg på alle vertikalskiver og aktivisere disse – enten de har høy relativ stivhet eller ei.

Beregningsresultatene gir oss tallverdier å feste konklusjonen til:

Første kjøring sier at vi må ha randstringer for å kunne oppta

$$F_{s,V-skive} = 168.75kN \bigwedge F_{s,RaSk} = 129.2kN$$

Som tilsvarer 3Ø12 B500NC (karakteristiske verdier brukt, både for belastning og kapasitet)

Andre kjøring gir randstringer som skal kunne oppta

$$F_{s,V-skive} = 228.6kN \bigwedge F_{s,RaSk} = 133.4kN$$

Det vil si at vi fortsatt klarer oss med 3Ø12 for RaSk-metoden, som har tilnærmet like horisontalskiveoppførsler i kjøring 1 og kjøring 2.

Men V-skive vil at vi skal armere med 3Ø16 – vesentlig mye mer armering.

Som forventet har vi da funnet at vertikalskivenes stivhet har stor innvirkning på kraftfordelingen i tradisjonell regnemodell, mens RaSk-metoden ikke er så følsom for dette.

Altså vil modellering med RaSk-metoden ikke være særs avhengig av vertikalskivens stivhet.

Q.E.D