Universitetet i Stavanger FACULTY OF SCIENCE AND TECHNOLOGY MASTER'S THESIS					
Study Programme/specialisation:	Spring semester, 2020				
Petroleum Engineering/Natural Gas	Open				
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Title of the master's thesis: Influence of Indium on Cu/Zn and Cu/Zr cataly	ysts for CO <sub>2</sub> hydrogenation to methanol				
Credits: 30 ECTS					
Keywords:					
CO <sub>2</sub> hydrogenation Methanol	Number of pages: 55				
Indium Oxide Cu-based catalysts Coprecipitation Wet Impregnation	Stavanger, 15 July 2020				

# Acknowledgements

I would like to thank Kristian Stangeland, Huong Lan Huynh, and Prof. Zhixin Yu for all the support and patience while doing this research. It was exciting to work on this subject and I will always be thankful to all of you for accepting me as a part of the team.

Agradecido con mi familia y amigos por el apoyo moral, sobre todo en estos tiempos difíciles e inusuales. También agradezco mucho a Juana Ascencio, Erika Chong, Renata Brinceño y Rúbenson Barrios por prestarme la plata pa' venir a Noruega. Nadie presta toda esa plata así de chévere. Gente buena gente.

Sist men ikke minst, til Anje. Gleder meg til en fremtid sammen.

# Abstract

The consequences of the anthropogenic carbon dioxide (CO<sub>2</sub>) released into the atmosphere have been forecasted as devastating for the global environment. It is mandatory to take action now, and there are alternatives under development to mitigate and counteract the aftermath of climate change. One possible major contributor is carbon capture, utilization, and storage (CCUS), and several of its technologies have been successfully tested, such as the use of CO<sub>2</sub> as feedstock for different chemical processes. Converting emissions into methanol (CH<sub>3</sub>OH) represents an interesting alternative for contributing to this solution. The conversion of CO<sub>2</sub> into valuable products is a technology with almost 100 years of history, although it has yet to reach optimal processing and maturity.

 $CO_2$  hydrogenation to methanol is a process that requires moderate temperature and pressure to be effective. The catalysts used for converting  $CO_2$  into methanol at a limited number of  $CO_2$ -to-methanol plants are based on a mix of metallic copper (Cu), zinc oxide (ZnO), and aluminum oxide (Al<sub>2</sub>O<sub>3</sub>). However, more efficient catalysts are necessary for large-scale implementation as the current catalyst is easily deactivated. Among many promoters tested to improve the catalyst's performance, zirconium oxide (ZrO<sub>2</sub>) is considered an excellent promoter for Cu-based catalysts. Moreover, indium oxide (In<sub>2</sub>O<sub>3</sub>) has been investigated as a promising base catalyst due to its high methanol selectivity and good performance in hightemperature applications.

In this work, a set of Cu-based catalysts were synthesized using ZnO,  $ZrO_2$ , and  $In_2O_3$  as promoters. The catalysts were prepared by coprecipitation or wet impregnation. Synthesized catalysts were characterized by N<sub>2</sub> physisorption, X-ray diffraction (XRD), N<sub>2</sub>O titration, H<sub>2</sub>temperature programmed reduction, and inductively coupled plasma optical emission spectroscopy (ICP-OES).

The activity tests were performed in a packed bed reactor (PBR) at 230 °C, 30 bars, and a feed stream of  $H_2/CO_2/N_2$  with molar ratio 3:1:1.  $In_2O_3$  improved the crystallite size of Copper particles and had a positive effect on the catalyst pore size, although has little impact in the catalytic activity of  $CO_2$  hydrogenation to methanol. CuZr-based catalysts showed better performance in terms of methanol selectivity (ca. 52%) vs.  $CO_2$  conversion (ca. 8%), however, CuZn catalysts are more active in terms of activity per area unit. Further investigations are required to achieve optimal ratios between Cu, Zn, Zr, and  $In_2O_3$  for applications in industrial processes.

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# **1** Introduction

### 1.1 Background

Climate change and sustainable development are arguably the toughest and most explored research subjects in recent years due to their implication on the environment, society, technology, politics, and economy [1]. One of the ways to address climate change is carbon capture, utilization, and storage (CCUS), as anthropogenic CO<sub>2</sub> contributes significantly to greenhouse gas emissions [2]. Governments are imposing strict environmental laws and policies that limit emissions of various gases such as NO<sub>x</sub>, CO<sub>2</sub>, and SO<sub>2</sub>, among which CO<sub>2</sub> is the most significant. Thus, CO<sub>2</sub> utilization processes are likely to play an important role in the future [3]. In a clean technology scenario, CO<sub>2</sub> utilization has been identified as a major contributor for cutting emissions within several sectors, as shown in Figure 1.1. Many alternative processes using CO<sub>2</sub> as feedstock are under development, which may become profitable in a low-carbon society [4].



Figure 1.1. Global CO<sub>2</sub> emission reductions by technology and area sector, comparing Reference Technology Scenario [5].

Methanol has been praised as an interesting alternative for moving away from fossil fuels towards cleaner energy solutions. In 2005, George A. Olah proposed that methanol rather than fossil fuels could be used as the primary energy carrier as well as feedstock for the synthesis of important hydrocarbons and their derivatives [6]. This model is based on "green" methanol produced from  $CO_2$  and  $H_2$  generated from renewable sources, creating a synthetic carbonneutral cycle. One of the great advantages of the methanol economy compared to other proposed future energy economies (e.g. hydrogen economy) is that methanol is highly versatile. Methanol is an important chemical feedstock used in a large array of chemical processes, such as methanol to olefins (MTO), paraffins (MTP), and gasoline (MTG). It can also be used as an alternative fuel in combustion engines or direct methanol fuel cells (DMFC) [7]. Furthermore, it can be utilized for wastewater treatment as it is readily biodegradable [8]. The given advantages and multiple uses of methanol and the current focus of reducing the CO<sub>2</sub> in the atmosphere are the main drivers for intensive CO<sub>2</sub>-to-methanol technology investigations [9]. Figure 2.1 presents the projected total methanol demand by end-use for 2021.



Figure 1.2. Total projected methanol demand by end-use for 2021 [10].

Currently, methanol is produced in a large-scale process from syngas, a mixture of CO,  $CO_2$ , and  $H_2$ , which is mostly generated from natural gas or coal [11]. The process for converting syngas and  $CO_2$  to methanol is very similar. Thus, with the process and the infrastructure already in place, a transition into the CO<sub>2</sub>-based methanol economy is feasible.

Syngas is converted to methanol over a heterogeneous catalyst composed of Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>. Cu-based catalysts are also the most investigated system for CO<sub>2</sub> hydrogenation to methanol [12]. However, they are often prone to deactivation due to the more severe reaction environments in CO<sub>2</sub>/H<sub>2</sub> mixtures [13]. To improve the activity and stability of Cu-based catalysts for CO<sub>2</sub> hydrogenation to methanol, different supports and promoters have been investigated (e.g. Ga<sub>2</sub>O<sub>3</sub>, Ce<sub>2</sub>O<sub>3</sub>, Cr<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, ZrO<sub>2</sub>, and In<sub>2</sub>O<sub>3</sub>) [14]. Typically, promoters increase the Cu dispersion thereby enhancing the catalyst's performance. Among other catalytic systems, In<sub>2</sub>O<sub>3</sub>-based catalysts have received considerable interest due to higher stability and methanol selectivity compared to Cu-based catalysts [15]. Typically, these

catalysts show stable performance with very high methanol selectivity over a wide temperature range but require higher reaction temperatures to obtain sufficient activity [16].

### **1.2 Scope of the work**

There have been studies on indium oxide  $(In_2O_3)$  promotion of Cu-based catalysts. Sloczynski et al. [17] reported in 2006 that adding  $In_2O_3$  to a Cu/ZnO/ZrO<sub>2</sub> catalyst considerably decreased the catalyst activity. More recent works are related to high selectivity and low conversion rates [18]. Other effects have been reported by Sadeghinia et al. [19] that adding  $In_2O_3$  can lead to an increase in Cu surface area and oxygen vacancies but lower reaction rates. Further research is required in this field to achieve the optimal performance of  $In_2O_3$  as a promoter in Cu/Zn and Cu/Zr catalysts.

The scope of this research is to gain insight into the effect of  $In_2O_3$  on the catalytic performance of Cu/ZnO and Cu/ZrO<sub>2</sub> catalysts for methanol production. The focus is to determine the role of  $In_2O_3$  on the catalytic activity and methanol selectivity. Well-ordered Cu/ZnO and Cu/ZrO<sub>2</sub> catalyst systems are synthesized by co-precipitation as a framework for  $In_2O_3$  impregnation. Furthermore, a Cu/In<sub>2</sub>O<sub>3</sub> catalyst is prepared for comparison. The catalysts are characterized by X-ray diffraction (XRD), transmission electron microscope (TEM), H<sub>2</sub>-temperatureprogrammed reduction (TPR), N<sub>2</sub> adsorption-desorption, N<sub>2</sub>O titration, and inductively coupled plasma optical emission spectroscopy (ICP-OES) to gain insight into the textural and physiochemical properties. The catalysts are tested for CO<sub>2</sub> hydrogenation to methanol at 230-270 °C and 30 bar.

# 2 Literature Review

### 2.1 Methanol: a brief history and industrial production

Methanol, or methyl alcohol, is a transparent liquid chemical compound soluble in water and quickly biodegradable. It is the simplest alcohol and has CH<sub>3</sub>OH chemical formula. This compound has an ancient history, as it is documented that the Egyptians used methanol to preserve mummies [20]. The pre-industrialized period used methanol as wood spirit or wood vinegar [21]. After methanol was obtained by Robert Doyle in 1661 by simple distillation, Jean-Baptiste Dumas and Eugene Peligot determined the elemental composition in 1834. Not before 1905 research on methanol synthesis started when Paul Sabatier and Jean-Baptiste Senderens documented methanol decomposition using Cu-based catalysts [22].

Methanol production has been in constant growth since the methanol industry began in 1923 with the BASF plant in Germany using a ZnO/Cr<sub>2</sub>O<sub>3</sub> catalyst. Natta [23] found that having Zn:Cr:Cu atomic ratios of 6:3:1 and 8:1:1 are quite active, but activity decreased considerably after a short period [24]. In 1963, Imperial Chemical Industries (ICI) started producing methanol at much lower pressures, by using a Cu/ZnO catalyst, the basis for the current methanol plants worldwide [25]. In 1971, an improved low-pressure methanol process was implemented with the Lurgi process, improving the overall reaction thermodynamics and efficiency [26]. During the new century, two major milestones have been accomplished. The first one is the George A. Olah Plant in Iceland that produces methanol from captured CO<sub>2</sub> since 2012 [27], and the second landmark is the opening of the largest methanol plant in the world: The Kaveh Plant in Iran with a reported production capacity of 2.3 million tonnes per annum. However, operations have been intermittent since its opening in 2017 [28]. In Europe, the largest methanol plant is in Norway, producing 2400 TPD (ca. 0.9 million tonnes per annum) and started operations in June 1997 [29].

### 2.2 Thermodynamics of CO<sub>2</sub> hydrogenation to methanol

 $CO_2$  hydrogenation to methanol involves 3 main reactions: methanol synthesis reaction from  $CO_2$  (Eq. 2.1), from CO (Eq. 2.2), and the reverse water-gas shift reaction (RWGS) as a side reaction (Eq. 3.3). From the reaction enthalpies, methanol synthesis is an exothermic process whereas the RWGS reaction is endothermic. Thus, according to Le Chatelier's principle, methanol production is favored at low temperatures and high pressures [30]. Thermodynamic

challenges start to appear as CO<sub>2</sub> is a very stable molecule, which requires sufficient energy to activate.

$$CO_2 + 3H_2 \leftrightarrow CH_3OH + H_2O$$
  $\Delta H_{298}^0 = -49.47 \ KJ/mol$  (Eq. 2.1)

$$CO + 2H_2 \leftrightarrow CH_3OH \qquad \qquad \Delta H_{298}^0 = -90.64 \text{ KJ/mol} \qquad (Eq. 2.2)$$

$$CO_2 + H_2 \leftrightarrow CO + H_2O$$
  $\Delta H_{298}^0 = +41.20 \ KJ/mol$  (Eq. 2.3)

The effect of pressure and temperature on the thermodynamics of  $CO_2$  hydrogenation to methanol is shown in Figure 2.1 (a) and (b) from two different studies.  $CO_2$  is a very stable molecule, which requires sufficient energy to be activated, therefore, it is difficult to obtain enough reaction rates at very low temperatures. The drawback of operating at higher temperatures is that the RWGS reaction becomes more favorable, which results in lower methanol selectivity. Typically, methanol synthesis is conducted at 200-300 °C and 50-100 bar [31, 32]. The limitations of the thermodynamics are much stricter for  $CO_2$  hydrogenation to methanol compared to methanol synthesis from syngas.



Figure 2.1. a) Effect of temperature and pressure on CO<sub>2</sub> conversion to methanol and CO (dashed lines represents gas-phase equilibrium) [30]. b) Effect of temperature and pressure on CO<sub>2</sub> conversion to methanol including the typical operating temperature range of industrial catalysts (dashed area) [32].

### 2.3 Catalysts for methanol synthesis from CO<sub>2</sub> hydrogenation

The Cu surface area plays a fundamental role in the overall activity for Cu/ZnO based catalysts. It is well known that Cu is the most active metal for methanol synthesis from CO<sub>2</sub> and H<sub>2</sub> [33]. However, metal oxides can have a significant influence on the activity and selectivity of Cu-based catalysts. Other systems include for example Pd/ZnO [34], which shows similar performance as Cu-based catalysts. In<sub>2</sub>O<sub>3</sub>-based catalyst has gained much interest lately as they

show very high methanol selectivity due to its limited activity for the RWGS reaction. The focus of this work is on the effect of  $In_2O_3$  on Cu/ZnO and Cu/ZrO<sub>2</sub> for methanol synthesis, and therefore, this review will primarily cover these catalytic systems.

### 2.3.1 Copper - Zinc Oxide (Cu/ZnO) catalysts

Cu/ZnO-based catalysts, typically with Al<sub>2</sub>O<sub>3</sub> as a structural promoter, is the most studied catalytic system for methanol synthesis. However, the role of ZnO in enhancing the catalyst's performance has been broadly debated. Studt et al. [35] noted that the presence or absence of ZnO can lead not only to changes in the activity but also in the reaction mechanism. Different promotional mechanisms have been proposed in the literature. Kakumoto [36] suggested that Zn sites are fundamental for the adsorption of the hydrogen ion (H<sup>-</sup>). ZnO sites are also a possible site for the adsorption of the methoxy (CH<sub>3</sub>O<sup>-</sup>) intermediate, though as an alternative to Cu<sup>+</sup> sites since it has a higher formation barrier. Spencer [37] suggested that the synergy between Cu and ZnO depends on the operating conditions, but is due to hydrogen spillover from the ZnO to the metallic Cu on the surface. Natesakhawat et al. [38] proposed that the relationship between metallic Cu as the active site and the ZnO promoter was due to irregular morphology and defects induced by the addition of ZnO. Furthermore, ZnO also increases the Cu surface area, which is a common descriptor of the catalyst's activity. It has also been suggested that the role of the ZnO is related to the stabilization of the Cu<sup>+</sup> species on the surface [39].

In recent years, partial coverage of Cu by Zn or  $ZnO_x$  species is widely regarded as the active configuration in Cu/ZnO-based catalysts. Kattel et al. [33] obtained a volcano-type relationship between the activity and the fraction of Cu(111) covered by ZnO, as shown in Figure. 2.2. The trend depicted is similar to the results obtained by Fujitani et al. [40] for Zn-deposited on Cu(111). They found that the optimal turnover frequency (TOF) on Zn/Cu(111) catalyst was found at a Zn Coverage ( $\Theta$ Zn) of 0.19. Behrens et al. [41] proposed undistorted pure Cu(111) facets are not active and two aspects are required to dramatically increase the catalyst activity: available steps or irregularities in the Cu facets and the presence of Zn or ZnO<sub>x</sub> at the defective Cu surface.



Figure 2.2. Rate of Conversion of CO<sub>2</sub> to methanol on Cu(111) vs. the fraction of the surface covered by Cu/ZrO<sub>2</sub> at three different reaction temperatures [33]. Observe the optimal range for methanol conversion slightly above 20%.

Complementing this observation, Karelovic and Ruiz [42] studied the Cu particle size on Cu/ZnO catalysts, since the Cu surface area is important for the activity of the catalyst. They showed that the methanol formation rate is independent of the particle size. However, they found a lower formation of CO and RWGS reactions over larger Cu particles. Van den Berg et al. [43] studied the structure sensitivity of Cu and CuZn catalysts, revealing a decrease in the turnover frequency (TOF) of the catalytic system when the Cu particle size is smaller than 8 nm. This was interpreted as methanol synthesis is favored when the Cu-based catalyst contains step-edge sites.

### 2.3.2 Zirconia (ZrO<sub>2</sub>) as a promoter

The study of the synergy between Cu and ZrO<sub>2</sub> catalysts has been investigated thoroughly, especially in the last decade. More than 30 years ago, Gasser and Baiker [44] prepared Cu/ZrO<sub>2</sub> catalysts from Cu and Zr nitrates, as well as from Cu<sub>7</sub>Zr<sub>3</sub>, suggesting that the active sites of the catalysts have similar nature and activity. Kanoun et al. [45] were among the pioneers synthesizing Cu and Zr catalysts to produce methanol from CO<sub>2</sub>, however, selectivities did not exceed 17%. Nitta et al. [46] reported much higher selectivities using Cu/Zr and Cu/Zr/Zn, though relatively low conversions. In both cases, Cu/ZrO<sub>2</sub> was found to enhance Cu dispersion. Schilke et al. [47] concluded that relatively small additions of ZrO<sub>2</sub> to Cu/SiO<sub>2</sub> favors the methanol conversion due to reactions occur on the active sites of both Cu and Zr. In later works, Zr has been identified to improve activity by controlling its phase [48]. Interactions between Cu, Zr, and doping Zn were analyzed by Arena et al. [49]. They concluded that the interaction

between Cu particles and both ZnO and ZrO<sub>2</sub> is beneficial for stabilizing the Cu active sites and enhance the adsorption/activation of  $H_2$  and CO<sub>2</sub> for the reaction. In the early 2010s, trimetal catalysts and precursors derived from hydrotalcite (HT) were the focus of many works, where Zr plays an important role in the dispersion of Cu, larger surface area and finally improving the methanol formation rate [38] [25-27].

The effect of different  $ZrO_2$  phases on Cu-based catalysts is still under discussion. Several works have come to differing conclusions in regards to which is the most active  $ZrO_2$  phase as well as the optimal preparation method for achieving the appropriate phase and high Cu dispersion. Samson et al. [50] found a direct relationship between the morphology of the  $ZrO_2$  phase and the catalyst activity. Despite being the most thermodynamically unstable phase, Cu supported on tetragonal  $ZrO_2$  (t- $ZrO_2$ ) was found as the most active catalyst, attributed to a higher concentration of acidic centers formed with the participation of Cu cations connected to the oxygen vacancies.

Witoon et al. [51] investigated the activity of Cu supported on different  $ZrO_2$  phases: amorphous (a-ZrO<sub>2</sub>), monoclinic (m-ZrO<sub>2</sub>), and t-ZrO<sub>2</sub>. The highest activity was obtained over Cu/a-ZrO<sub>2</sub>, which also had the highest Cu surface area. However, the methanol TOF over the t- phase was between 1.1–1.5 and 1.6–3.6 times higher than Cu/a-ZrO<sub>2</sub> and Cu/m-ZrO<sub>2</sub>, respectively. The relationship between the ZrO<sub>2</sub> phase and the CO<sub>2</sub> conversion and methanol selectivity is shown in Figure 2.3.



 $\label{eq:Figure 2.3. CO2} Figure 2.3. CO_2 \mbox{ conversion (a) and methanol selectivity (b) as a function of the reaction temperature on a-ZrO_2, t-ZrO_2 \mbox{, and m-ZrO}_2 \mbox{ [51]}.$ 

Tada et al. [52] also found that a-ZrO<sub>2</sub> resulted in higher conversions compared to m-ZrO<sub>2</sub> and t-ZrO<sub>2</sub>, which was attributed to higher Cu dispersion. In addition, weaker methanol adsorption was measured on a-ZrO<sub>2</sub> species, leading to higher methanol selectivity by limiting methanol decomposition. Ro et al. [53] found that the formation of Cu-ZrO<sub>2</sub> interfacial sites increased the TOF to methanol, indicating that the number of interfacial sites significantly influences the activity of Cu-ZrO<sub>2</sub> catalysts. Wang et al. [54] and Larmier et al. [55] also concluded that larger Cu surface areas do not necessarily mean a higher activity of Cu-ZrO<sub>2</sub> based catalysts. More recently, Fujiwara et al. [56] studied the influence of the particle size with highly loaded CuO on ZrO<sub>2</sub> catalysts synthesized via spray pyrolysis. They observed that when the catalysts are prepared at a slower rate, it is more likely to result in smaller ZrO<sub>2</sub> particles, which increases the number of interfacial sites and show higher activity.

Li and Chen [57] summarized the current status of research on Cu-Zr interaction and proposed further investigations on the effect of each phase on the catalytic performance. Their findings are shown in Figure 2.4. In general, Cu/ZrO<sub>2</sub> systems present four typical surface properties, i.e., acidic, basic, oxidizing, and reducing, although relatively weak. However, the structure sensitivity plays an important role in promoting the CuZr system for methanol synthesis. The authors also propose further research in the oxide-oxide interactions (e.g. ZnO-ZrO<sub>2</sub> interface).



Figure 2.4. Effects of Zr phases on the catalytic performance of Cu/ZrO<sub>2</sub> catalysts, according to [57].

Several studies have also investigated the effect of promoters on Cu-ZrO<sub>2</sub> catalysts. Tada et al. [58] considered the addition of Ag into Cu-ZrO<sub>2</sub>, evaluated the quality of the active sites by changing space velocities, and concluded an improvement in the methanol selectivity compared to a Cu-ZrO<sub>2</sub> catalytic system. The formation of an Ag-Cu alloy resulted in a new active species for the CO<sub>2</sub> hydrogenation process.

Hengne et al. [59] prepared  $ZrO_2$  supported Ni-Sn catalysts and studied the effect of adding  $In_2O_3$  as a promoter. They showed that a 99% selectivity was achieved, together with high

conversion rates and good stability. There are many other works including vanadium oxide [45], In<sub>2</sub>O<sub>3</sub> [19], TiO<sub>2</sub> [47], Y<sub>2</sub>O<sub>3</sub>, La<sub>2</sub>O<sub>3</sub>, Ce<sub>2</sub>O<sub>3</sub>, and Al<sub>2</sub>O<sub>3</sub> [60, 61], although the latter two are for methanol steam reforming and methanol fuel cells processes.

### 2.3.3 In<sub>2</sub>O<sub>3</sub> catalysts for CO<sub>2</sub> hydrogenation to methanol

In<sub>2</sub>O<sub>3</sub> alone can also be used as a catalyst for the CO<sub>2</sub> conversion to methanol. For instance, In<sub>2</sub>O<sub>3</sub> catalysts have shown interesting results in terms of activity and selectivity, in some cases reporting selectivity values close to 100% when  $ZrO_2$  promoter is present [62]. Studies conclude that high selectivity was achieved due to In<sub>2</sub>O<sub>3</sub> not being particularly active for the RWGS reaction [16], even at a broad range of temperatures of 450 – 673 K [63]. Another important effect from  $ZrO_2$  over In<sub>2</sub>O<sub>3</sub> is the suppression of dissociative CO<sub>2</sub> and stabilization of intermediates on the catalyst surface [64].

Ye et al. [15] proposed a reaction mechanism over  $In_2O_3(110)$  catalyst using density functional theory (DFT) calculations, favoring the HCOO route. More recently, Frei et al. [65] carried out a similar study over  $In_2O_3(111)$ , concluding that the activation energy (Ea) determined for the CO<sub>2</sub> to methanol synthesis was higher than the one for the RWGS reaction, explaining the superior methanol selectivity of the catalyst. In the last few years, Chen et al. [66], Chou and Lobo [67], and Frei et al. [68] have studied the promotional effect of ZrO<sub>2</sub> on In<sub>2</sub>O<sub>3</sub>, which resulted in high methanol selectivity and increased the number of active sites.

### 2.3.4 In<sub>2</sub>O<sub>3</sub> as promoter for CO<sub>2</sub> hydrogenation to methanol

Ever since the study carried out by Sloczynski et al. [17] and its discouraging results in terms of  $CO_2$  conversion,  $In_2O_3$  has received little attention as an effective promoter over Cu-based catalysts. However, the advantages of new analyses and tools to elucidate reaction mechanisms in the  $CO_2$  hydrogenation reaction have encouraged scientists to test materials once discarded in the past. For instance, Yao et al. [18] and Chamssine [69] studied the effects of  $In_2O_3$  on CuZr and hydrotalcite-like catalysts respectively, by varying both the Cu load and the  $In_2O_3$  promoting load, and demonstrated good methanol selectivity between 50% and 75%, as well as reaction stability for long-run reactions.

The latest works by Sadeghinia et al. [19] and Gao et al. [70] reveal the promotional effects to the structural properties of adding  $In_2O_3$  to Cu-based and CuZr catalysts in terms of larger surface area and pore size distribution, but mixed results in terms of CO<sub>2</sub> conversion and

methanol selectivity. The limited investigations and the lack of a solid consensus on catalytic activity for  $CO_2$  hydrogenation to methanol are yet other drivers for carrying out investigations on the promotional effects of indium over Cu-based catalytic systems.

### 2.4 Reaction Mechanisms for CO<sub>2</sub> Hydrogenation to Methanol

### 2.4.1 Cu/ZnO catalysts

Several studies have focused on the reaction mechanism of  $CO_2$  hydrogenation to methanol over Cu-based catalysts. Formate (HCOO) and methoxy (H<sub>3</sub>CO) intermediates are the most common species identified for methanol synthesis [71] and were also observed in *In Situ Fourier Transform - Infra-Red* (FT-IR) studies [72]. In literature, the reaction pathway that is most often reported goes through the formate intermediate and can be simplified to 7 elementary steps (Eqs. 2.4 to 2.10), where \* denotes the active sites.

$CO_2^* + H^* \rightleftharpoons HCOO^* + *$	( <i>Eq</i> . 2.4)
$HCOO^* + H^* \rightleftharpoons H_2COO^* + *$	( <i>Eq</i> . 2.5)
$H_2COO^* + H^* \rightleftharpoons H_2COOH^*$	( <i>Eq</i> . 2.6)
$H_2COOH^* \rightleftharpoons H_2CO^* + OH^*$	( <i>Eq</i> . 2.7)
$H_2CO^* + H^* \rightleftharpoons H_3CO^* + *$	( <i>Eq</i> . 2.8)
$H_3CO^* + H^* \rightleftharpoons CH_3OH^* + *$	( <i>Eq</i> . 2.9)
$CH_3OH^* \rightleftharpoons CH_3OH^{(g)} + *$	(Eq. 2.10)

Grabow and Mavrikakis [73] presented a comprehensive study of the reaction mechanism, which is based on energetics over Cu(111) from DFT corrected by experimental values. Figure 2.5 illustrates several intermediates and their binding configuration on Cu(111). In the figure, red dots represent oxygen, black dots show carbon, and blues denote hydrogen. Hydroxy (OH) and carbon monoxide (CO) molecules are not shown for simplicity. The Cu surface is represented by the brown dots. They found that the main route for CO<sub>2</sub> hydrogenation to methanol was through HCOO\*  $\rightarrow$  HCOOH\*  $\rightarrow$  H<sub>2</sub>COOH\*  $\rightarrow$  H<sub>2</sub>CO\*  $\rightarrow$  H<sub>3</sub>CO\*  $\rightarrow$  H<sub>3</sub>COH\*. CO could also be hydrogenated to methanol but follow a different pathway (CO  $\rightarrow$  H<sub>2</sub>CO  $\rightarrow$  H<sub>3</sub>COH).



Figure 2.5. Adsorption states of selected intermediates for CO<sub>2</sub> to methanol reaction on Cu(111). Top row: (a) formate, (b) dioxymethylene, (c) formaldehyde, (d) methoxy, (e) methanol. Middle row: (f) formyl, (g) formic acid, (h) hydroxymethylene, (i) hydroxymethyl, (j) carboxyl. Bottom row: (k) hydroxymethylidyne, (l) carbonate, (m) bicarbonate, (n) methyl formate, (o) methoxyoxymethylene. [73].

Behrens et al. [41] conducted DFT calculations to investigate the role of Zn on Cu. Methanol synthesis through the formate pathway was compared over Cu(111), Cu(211), and CuZn(211). They found that Cu steps in Cu(211) lowered the barriers and increased the stability of reaction intermediates, which was further enhanced by Zn addition to Cu(211).



Figure 2.6. a) Graphic representation of Cu and CuZn arrangements containing both Cu (yellow spheres) and zinc (silver). b) Gibbs free-energy diagram ( $\Delta G$ ) for CO<sub>2</sub> to methanol reaction from DFT calculations [41].

Other routes from  $CO_2$  to methanol have also been explored. Zhao el at. [74] studied the reaction network on Cu(111) using density functional theory (DFT) calculations. They found that methanol synthesis through the formate intermediate was unlikely due to high barriers. A hydrogen transfer mechanism was observed in the presence of co-adsorbed H<sub>2</sub>O that made the carboxyl (COOH) route more favorable. The subsequent steps were through the formation of COHOH, followed by COH, HCOH, and finally methanol (CH<sub>3</sub>OH).

#### 2.4.2 Cu/ZrO<sub>2</sub> catalysts

Wang et al. [54] and Larmier et al. [55] proposed a similar reaction mechanism over  $Cu/ZrO_2$  catalysts. Both studies conclude that hydrogenation of formate is the rate-limiting step in the hydrogenation process. They also pointed out the crucial role of the molecular interaction between the Cu and Zr compared to other structural properties, such as surface area or oxygen vacancies. Figure 2.7 shows the reaction mechanism determined by Larmier et al., which is the same as the reaction route typically proposed over Cu and Cu/ZnO systems.



Figure 2.7. Reaction Mechanism, Energy, and Gibbs Free Energy ( $\Delta G$ ) for the CO<sub>2</sub> hydrogenation to methanol at Cu/ZrO<sub>2</sub> interface [55].

### 2.4.3 In<sub>2</sub>O<sub>3</sub> catalysts

Ye et al. [15] and Frei et al. [65] studied the reaction mechanism of CO<sub>2</sub> hydrogenation to methanol using DFT calculations over In<sub>2</sub>O<sub>3</sub>(110) and In<sub>2</sub>O<sub>3</sub>(111) catalysts, respectively. A common simplified route proceeds as CO<sub>2</sub> + H<sub>2</sub> (adsorbed)  $\rightarrow$  HCOO\*  $\rightarrow$  HCOOH\*  $\rightarrow$  CH<sub>2</sub>O\*  $\rightarrow$  CH<sub>3</sub>O\*  $\rightarrow$  CH<sub>3</sub>OH\*, which is similar to Cu-based catalysts. The binding energy of intermediates is different on In<sub>2</sub>O<sub>3</sub> compared to Cu and the proposed rate-limiting step depends on the In<sub>2</sub>O<sub>3</sub> lattice. Figure 2.8 shows a representation of the In<sub>2</sub>O<sub>3</sub>(111) lattice and the adsorption of CO<sub>2</sub> and H<sub>2</sub>.



Figure 2.8. (a) Top-view of the  $In_2O_{3-x}(111)$  surface, with an oxygen vacancy per (1x1) cell. (b) Top view of the activated co-adsorption of CO<sub>2</sub> and H<sub>2</sub> on  $In_2O_{3-x}(111)$ . Color code: In (blue), O (red), C (black), and H (white) [65].

Figure 2.9 depicts the structures of the adsorbed reaction intermediates. It represents the mechanistic route for the reaction, from left to right and top to bottom. Color code: H (white), O (red), C (black) and In (grey).



Figure 2.9. Optimized adsorption structures of the reaction intermediates involved in  $CO_2$  hydrogenation to methanol on defective  $In_2O_3(110)$  surface [15].

# 2.5 Catalyst Synthesis

There are numerous catalyst preparation methods and every catalyst can be synthesized using different techniques. However, there are three basic steps that synthesis of supported metal oxides (SMOs) have in common: preparation of precursor, precursor processing (e.g., via calcination or pyrolysis), and activation of the precursor to obtaining the final active catalyst [75]. Herein, only the theoretical basis of the synthesis methods used in this work will be presented.

#### 2.5.1 Coprecipitation

Synthesis by coprecipitation is a method where a solid is precipitated from a solution that contains precursors of both the support and the active metal oxides. It is initiated by mixing the solution with a precipitating agent, which has two possible effects. First, condensation of the precursor by changing the solution pH and second, introduces ions to the solution to exceed the solubility of the product. After precipitation, aging steps can be carried out for crystal growth. Lastly, filtering and washing the counterions results in the final precursor [76]. The advantages of this procedure are a better spatially distributed framework of the oxide materials compared to other methods, which will allow better interaction between the support and the active species, also with reduced exposure of the active species to the catalytic surface as a downside. For the latter reason, it is often to find density calculation results overestimating actual values [76].

Several parameters will influence the structure of the precursors synthesized by coprecipitation: precipitating agent, pH control, efficient mixing, washing, aging, and filtering. Supporting the influence of the preparation parameters in the preparation of catalysts, Figure 2.10 describes the variation of the surface area with the pH during the coprecipitation method, from three different ZrO<sub>2</sub> catalysts [77].



Figure 2.10. Correlation of surface area vs. pH change in preparation by precipitation. Precursors are labeled as ( $\Box$ ) ZrO2• H<sub>2</sub>O, ZrO<sub>2</sub> ( $\Delta$ ) and SO<sub>4</sub>-/ZrO<sub>2</sub> ( $\blacksquare$ ) [77]

### 2.5.2 Wet impregnation

This relatively simple procedure consists of contacting a solid (solute) with a solution containing the materials to be deposited on the surface (support). During impregnation, there

are two major phenomena for the synthesis process: a *diffusion* process, where the solute spreads into the pores of the support and the *adsorption* process, where the solute attaches into the pores [78].

After a homogeneous solution is achieved with vigorous stirring for a long period, samples are dried to remove the solvent solution. This process is also common with the coprecipitation method. After the drying process, the precursor is ready for calcination.

### 2.5.3 Calcination

Calcination is a procedure where the as-prepared catalyst is heated to a high temperature, usually higher than the desired reaction temperature, in order to decompose the metal precursor by forming oxide and to remove impurities (water,  $CO_2$ , etc). High calcination temperatures can lead to a crystallization of the support and a loss of surface area [76]. When dealing with bimetallic catalysts, rigorous control of calcination temperature is required to avoid the formation of two separate oxides or the segregation of one of the components [79].

### 2.5.4 Reduction

The reduction process often occurs right before the catalyst is tested for the desired reaction, hence, it is mostly performed in the reactor. It consists of treating the catalyst with diluted hydrogen in an inert gas (usually  $N_2$ , He or Ar) at high temperatures, aiming to transform the oxide into an active metallic compound. Hydrogen is diluted to limit the rise of the adiabatic temperature, preventing particle *sintering*. To investigate and evaluate the reducibility of the catalyst, a temperature-programmed reduction (TPR) analysis is performed [80].

## 2.6 Catalyst Characterization

This section will present the different techniques, procedures, and theoretical background for the characterization of physio-chemical properties and morphology of the catalysts.

## 2.6.1 X-Ray Diffraction (XRD)

The powder X-ray diffraction technique allows evaluating the nature, concentration, and distribution of the crystals present in the catalyst, among other characteristics. XRD considers transverse planes of atoms periodically spaced, which is hit by upcoming waves (X-rays) at a specific angle. To generate interference patterns that can be interpreted, the wavelength ( $\lambda$ ) has

to be in the same order of magnitude as the interatomic space or distance (*d*), which is the case for the X-Rays ( $\lambda \approx 1$  Årmstrong). The ratio between  $\lambda$  and *d* is given by Bragg's Law (Eq. 2.11) [81].

$$n\lambda = 2d * \sin \theta$$
 (Eq. 2.11)

Where *n* is the diffraction order and  $\theta$  is the incident angle by the X-rays. The basic geometric derivation of Bragg's Law is illustrated in the following Figure 2.11.



Figure 2.11. Geometric derivation of Bragg's equation for two layers of atoms with interfacial spacing d (a) and idealized amplitude of the scattered waves (c). Also, the effect on an additional layer of atoms at d/4 (b, d) [81].

The result from the amplitude of the diffracted beam as a function of n/d or  $2\lambda^{-1}sin\theta$  can be plotted as shown in Figure 2.11 (c). In practice, the data is usually plotted against 2 $\theta$ , normally collected in a 5°-70° range. However, this applies only to an idealized crystal, with no interference from other phases [81]. Conversely, the crystallite size (*d*) can be estimated using Scherrer's equation (Eq. 2.12):

$$d = \frac{K * \lambda}{B * \cos \theta} \qquad (Eq. 2.12)$$

Where *K* is known as shape factor, related to the crystalline shape of the lattice and *B* is the full width at half of the peak in the XRD signal plot, in radians. Cu is a common component of an X-ray source and has a radiation wavelength (CuK $\alpha$ ) of 1.5418 Å [82]. The crystallography of the analyzed material will then be compared to the signals received, identifying crystal lattices previously recorded on a database for reference compounds. The most common databases are Powder Diffraction File (PDF) or the International Center for Diffraction Data (ICDD) - JCPDS (Joint Committee on Powder Diffraction Standards).

#### 2.6.2 Temperature Programmed Reduction (TPR)

This technique is used to reduce metal oxides (MO) into metallic compounds, using hydrogen gas at high temperatures and low pressures. It is possible to quantify the oxidation state and the temperature at which the reduction occurs. Furthermore, it can yield information on the degree of reduction, the metallic distribution, and the reducibility of the catalyst. An example of how the reaction proceeds is shown in Eq. 2.13 [82].

$$MO + H_2 \rightleftharpoons M (metallic) + H_2O$$
 (Eq. 2.13)

Products are the reduced metal (M) and water. As the reaction occurs at high temperatures, the amount of gas absorbed can be deducted from the furnace by a thermal conductivity detector (TCD), since its thermal conductivity is proportional to the mole fraction. Typically, hydrogen gas is dissolved in an inert gas, to facilitate the accuracy of the TCD. Common hydrogen concentrations are 1-10% [82].

### 2.6.3 Nitrogen Adsorption-Desorption

The adsorption of Nitrogen into porous materials is the most common technique to determine surface area and characterize porosity. Its theoretical foundation is based on the layered sorption of gases, specially physisorption since it occurs at lower adsorption energies, hence there are low structural changes on the absorbant surface. Brunauer, Emmet, and Teller (BET) proposed the layered model in 1938 technically applied to planar surfaces, however, the adsorption process is the same for micropores and mesopores, hence, the procedure is accepted as the standard for calculating the BET surface area [81].

The model is based on the International Union of Pure and Applied Chemistry (IUPAC)'s classification of sorption isotherms, presented in Figure 2.12 (a). The nitrogen adsorption at 77 K and (b) is equivalent to the isotherm I. This curve presents a linear behavior when relative pressure between the equilibrium and the saturation pressure ( $P/P_0$ ) at a given temperature is between 0.05-0.35. Within the linear behavior region, the BET equation is applied to determine the surface area of porous materials.

$$\frac{1}{W(\frac{P}{P_0} - 1)} = \frac{1}{W_m C} + \frac{C - 1}{W_m C} * \left(\frac{P}{P_0}\right)$$
(Eq. 2.14)

Where W is the weight of the sample, C is the BET constant related to both absorbent and absorbate. During the measurements, the data is recorded in terms of the term on the left side of Eq. 2.14, hence  $W_m$  can be easily solved to determine the surface area.



Figure 2.12. a) IUPAC classification of sorption isotherms b) Nitrogen adsorption at 77 K on an active carbon sample, containing micro and mesoporosity indicated by the occurrence of hysteresis at P/P<sub>0</sub>. [83]

The approach for determining the pore volume and pore size distribution is referred to as the Barrett-Joyner-Halenda (BJH) method. The capillary condensation region (P/P<sub>0</sub> > 0,4), pressure increase causes an increase of the thickness of the layer adsorbed on pore walls, and the capillary condensation in pore having a core size  $r_c$  (i.e. pore space) defined by the Kelvin Equation [84], as follows:

$$\ln\left(\frac{P}{P_0}\right) = \frac{-2\gamma w_m cos\theta}{RTr_c} \qquad (Eq. 2.15)$$

Where R is the universal constant for gases, T is the temperature,  $r_c$  represents the radius for cylindrical pores,  $\gamma$  the surface tension,  $w_m$  the molar volume, and  $\theta$  the contact angle. The assumption of a geometric model allows the calculation of the thickness of the adsorbed film to the total adsorption volume and core volume, followed by estimating the pore volume and pore size, assuming a given pore geometry [84].

### 2.6.4 N<sub>2</sub>O Titration

Since Cu presents the vast majority of active sites for  $CO_2$  hydrogenation to methanol, it is important to have an estimate of the Cu surface area or dispersion while characterizing Cubased catalysts. Cu surface *dispersion* (D), is defined as the ratio between Cu surface atoms and the total Cu atoms in the catalyst. In Cu-based catalysts, the estimation of metallic Cu surface area is typically done by the decomposition of nitrogen oxide ( $N_2O$ ) on the exposed Cu atoms. This process occurs by adsorbing atomic oxygen and releasing gas-phase nitrogen according to the reaction given in Eq. 2.16 [85].

$$N_2 O + 2Cu_s \rightarrow (Cu_s - O - Cu_s) + N_2$$
 (Eq. 2.16)

Where  $Cu_s$  represents the metallic Cu exposed on the catalyst's surface. One method of obtaining the Cu surface area is by injecting pulses of N<sub>2</sub>O into a reaction set-up with a small amount of the catalyst. The effluent gas composition is then monitored via a thermal conductivity detector (TCD), measuring the amount of both N<sub>2</sub>O and N<sub>2</sub>. A typical graph of the effluent gas is shown in Figure 2.13, where the mole fraction of the effluent is registered vs reaction time. Using the area under the formed N<sub>2</sub> curve and the mean Cu surface atom density (1.47x10<sup>19</sup> atoms per m<sup>2</sup>), the Cu surface area can be calculated [85]. Other N<sub>2</sub>O-based methods have also been proposed (e.g. [86]).



Figure 2.13. N<sub>2</sub>O experiment with a Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. Reaction conditions: T = 300K, p = 0.1 MPa, Flow = Nml/min gas misture of 1% N<sub>2</sub>O in He [85].

### 2.6.5 Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES)

The ICP-OES is a procedure to determine the metal concentrations present in the catalysts with high accuracy. Its principle is based on a generation of photons of light by the excitation of electrons of a pattern element, generating characteristic wavelength-specific photons emitted by the compounds in the sample [87].

### 2.6.6 Transmission Electron Microscope (TEM)

Over the last two decades, nanoscale imaging has played a fundamental role in the characterization of heterogeneous catalysts. One of the most common tools to provide detailed information from catalysts is TEM, which uses electrons through the analyzed object to create

a detailed image, to identify structural features. The schematic beam for TEM is depicted in Figure 2.13.



Figure 2.14. Schematic beam path in TEM [88]

TEM provides high-resolution images that allow identifying crystals, pores, metal dispersion, and many other properties. As an example, Figure 2.14 presents a TEM image for a Cu/Si/ZrO catalyst.



Figure 2.15. TEM image of a Cu/Si/ZrO at 50 nm resolution [89]

# 2.6.7 Gas Chromatography (GC)

Gas chromatography is by far the most explored technique to quantify catalyst activity for the desired reaction. It is defined by the IUPAC as "*a physical method of separation in which the components to be separated are distributed between two phases: stationary and mobile, the latter moving into a definite direction*" [90]. It uses the diffusion principle to determine the composition of volatile compounds, regardless of their nature.

Samples are vaporized and transported by a carrier gas throughout the chromatographic column. It contains a coating of a stationary phase. The separation of components is determined

by its distribution between the carrier gas and the stationary phase. Different compounds are separated based on their affinity to the stationary phase, measured by their vapor pressure. Information could be further captured by a mass spectrometer (MS), an instrument that measures the mass-to-charge ratio (m/z) and the quantity of a certain type of ions compared to a known m/z ratio, called External Standard (ESTD). Samples are analyzed once they leave the column into a detector, which can be Flame Ionization Detector (FID), Thermoionic Specific Detector (TSD), Flame Photometric Detector (FPD), or Thermal Conductivity Detector (TCD) [91]. Figure 2.15 illustrates the GC/MS system with its major components. Data is captured by a computer system, plotting the response factor (RF) over time for each component in the sample, compared to the calibration curve.



Figure 2.16. Conceptual illustration of the GC/MS system with major components [92].

The following equation is used to calculate the concentration of component i:

### $(Concentration)_i = RF_i * Measured Response (in area or height)_i$

Where  $RF_i$  is the response factor of i, which is the ratio between the known amount of i and the response of known amount [82]. Information from GC is used to determine catalyst activity: reactants conversion, product selectivity, etc.

# **3** Experimental

# **3.1 Catalysts Preparation**

Tables 3.1 and 3.2 list the chemicals and gases used to synthesize and test the catalysts in this work.

No.	Compound	Chemical	Manufacturer	Molecular	Purity
		Formula		Weight	
				(g/mol)	
1	Copper (II) nitrate	$CuN_2O_6$ · $3H_2O$	Acros Organics	241.60	≥99.5%
	trihydrate				
2	Zinc nitrate	$Zn(NO_3)_2 \cdot 6H_2O$	Alfa Aesar	297.49	≥99.9%
	hexahydrate				
3	Zirconium	$ZrO(NO_3)_2 \cdot 6H_2O$	Alfa Aesar	231.23 (anhy)	≥99.9%
	dinitrate oxide				(metal
	hydrate				basis)
4	Indium (III)	In(NO <sub>3</sub> ) <sub>3</sub> ·xH <sub>2</sub> O	Alfa Aesar	318.83 (anhy)	≥99.99%
	nitrate hydrate				(metal
					basis)
5	Sodium hydroxide	NaOH	Emsure	40.00	≥99.2%
6	Sodium carbonate	Na <sub>2</sub> CO <sub>3</sub>	Emsure	105.99	≥99.9%
7	Silicon	SiC	Alfa Aesar	40.1	≥98.8%
	carbide				
8	Nitric acid	HNO <sub>3</sub>	VWR	63.01	-
	(65 %)		Chemicals		
9	Hydrochloric acid	HCl	Merck	36.46	-
	fuming				
	(37 %)				

Table 3.1. List of chemicals used in catalyst synthesis and characterization tests.

Table 3.2. Gases utilized for catalytic activity tests.

No.	Compound	Chemical Formula	Manufacturer Molecular Weight		Purity
				(g/mol)	
1	Carbon Dioxide 5.2	$CO_2$	Yara Praxair	44,01	99.9992%
2	Hydrogen 5.0	$H_2$	Yara Praxair	2,01	99.999%
3	Nitrogen 5.0	$N_2$	Yara Praxair	28,01	99.999%
4	Synthetic Air 2.6	$N_2+O_2\\$	Yara Praxair	28,96	99.6%

Table 3.3 presents the catalysts prepared in this work. For analysis and characterization, catalysts will be divided by the two main components, i.e., CuZn, CuZr, and CuIn.

No.	Catalyst	Molar Ratio	Synthesis Method
1	CuZn	Cu:ZnO = 5:1	Coprecipitation
2	In/CuZn	$In_2O_3:Cu:ZnO = 0.005:5:1$	Wet Impregnation of In <sub>2</sub> O <sub>3</sub>
3	CuZr	5:1	Coprecipitation
4	In/CuZr	$In_2O_3:Cu:ZrO_2 = 0.005:5:1$	Wet Impregnation of In <sub>2</sub> O <sub>3</sub>
5	CuZrIn	$Cu:ZrO_2:In_2O_3 = 5:1:0.005$	Coprecipitation
6	CuIn	5:1	Coprecipitation
7	Zr/CuIn	$ZrO_2:Cu:In_2O_3 = 0.005:5:1$	Wet Impregnation of ZrO <sub>2</sub>

Table 3.3. List of synthesized catalysts.

### 3.1.1 Synthesis by coprecipitation

A calculated amount of the metal nitrates was dissolved in deionized water (DIW) and vigorously stirred until the compounds were completely dissolved. A second solution containing  $Na_2CO_3$  was prepared. The metal nitrate and sodium carbonate solutions were dropwise combined in a third beaker under continuous stirring such that the pH of the mixture remained constant at ca. 6.5 [49]. In the next step, the solution was aged for 14 h under vigorous stirring at 65 °C in a sealed cell under a constant flow of  $N_2$ . Following the aging process, the precursor slurry was collected using a paper filter of 12-15 µm, washed several times with DIW until the pH of the filtering liquid was 7. The precursor was then dried overnight at 90 °C before calcination at 300 or 500 °C for 3 hours.

### 3.1.2 Synthesis by wet impregnation

A calculated amount of metal nitrate and the synthesized bimetallic catalyst was dissolved and dispersed in DIW using ultrasonication until a homogeneous mixture was obtained. The mixture was then covered and stirred overnight at room temperature. Finally, the solution was dried in the oven overnight at 90 °C before calcination at 350 °C for 3 h.

### **3.1.3** Calcination procedure

The calcination procedure consisted of placing the precursor in a quartz reactor. The catalysts were calcinated at 350 °C for 3 hours, with a ramping rate of 2 °C/min under the flow of synthetic air. After the catalyst was calcinated, a sieving procedure took place to separate grains between 40 - 60 mesh (0,25 - 0,42 mm) for the activity tests.

### **3.2 Catalysts Characterization**

The equipment used and the analysis performed in this work are summarized in Table 3.4.

No.	Technique	Device Brand	Model	Property
1	$H_2 - TPR$	Micrometrics	Autochem II RS232	Reducibility
2	N <sub>2</sub> O Titration	Micrometrics	Autochem II RS232	Cu surface area
3	$N_2 - Adsorption /$	Micrometrics	TriStar II	Surface area –
	Desorption			porosity
4	XRD	Bruker-AXS	D8 Advance	Crystallography
5	ICP	Perkin Elmer	Optima 4300DV	Metal
				Composition
6	TEM	JEOL	JEM 2100plus	Morphology

Table 3.4. Summary of catalyst characterization techniques and the equipment used in this work.

### **3.2.1** Temperature Programmed Reduction (TPR)

H<sub>2</sub>-TPR was conducted by an Autochem II analyzer (Table 3.4). First, the samples (about 75 mg) were pretreated at 200 °C in Helium for 30 minutes to remove traces of water and/or CO<sub>2</sub> in the catalyst. The sample was then cooled to 50 °C and the flow was switched to 7% H<sub>2</sub>/Ar at a flow rate of 50 mL/min. The measurements were done while the temperature was increased from 50 °C to 550 °C at a rate of 5 °C/min.

#### 3.2.2 N<sub>2</sub>O Titration

A quartz tube was installed into the Autochem II analyzer (Table 3.4). Catalyst samples of ca. 75 mg were treated at 350 °C for 30 min with 7% H<sub>2</sub>/Ar. Next, the reactor was cooled in He flow to room temperature before 1% N<sub>2</sub>O/He flowed at 50 mL/min over the sample for 1 h. Then, the sample was purged with He before it was reduced by 7% H<sub>2</sub>/Ar. The amount of H<sub>2</sub> used to re-reduce the catalyst was measured. The available Cu surface area was determined by Eq. 3.1[14].

$$S_{Cu} = \frac{n_{Cu} * N_{av}}{W * A} \qquad (Eq. 3.1)$$

Where  $S_{Cu}$  is the available Cu surface area per gram catalyst (m<sup>2</sup>/g),  $n_{Cu}$  is the molar number of Cu, W is the amount of sample,  $N_{av}$  is Avogadro's number (6.022 x 10<sup>23</sup> atom/mol), and A is the number of Cu atoms per area unit (1.46 x 10<sup>19</sup> Cu atom/m<sup>2</sup>).

### 3.2.3 N<sub>2</sub> - Physisorption

Prior to the measurements, the samples were outgassed at 160 °C for 24 h in vacuum using a degassing system (Micrometrics VacPrep 061). N<sub>2</sub> physisorption measurements on the calcined support and catalysts were performed at –196 °C using a Micromeritics Tristar 3000 apparatus. The Brunauer-Emmet-Teller (BET) method was used to calculate the specific surface areas. The pore volumes were determined at  $P/P_0 = 0.9975$ . Barrett-Joyner-Halenda (BJH) method analysis (4 V/A) of the desorption branch was used to obtain the pore size distribution.

### 3.2.4 X-Ray Diffraction (XRD)

The X-ray diffraction (XRD) patterns were recorded for the catalyst precursors and calcined catalysts on a Bruker-AXS Microdiffractometer (D8 ADVANCE) using Cu K $\alpha$  radiation source ( $\lambda = 0.154$  nm). The reduced samples were passivated in 1% O<sub>2</sub>/N<sub>2</sub> mixture before being transferred to the sample holder. The patterns were collected in the range of 10–90° (2 $\theta$ ) with a step interval of 2°/min. The peaks were indexed according to the database established by the Joint Committee on Powder Diffraction Standards (JCPDS). Figures 3.1 and 3.2 show the precursors and catalysts synthesized in this work, respectively.



Figure 3.1. Catalysts' precursors listed in Table 3.3.



Figure 3.2. Calcinated catalysts listed in Table 3.3.

### 3.2.5 Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES)

To determine the metallic composition of the synthesized catalysts, an ICP-OES procedure was carried out. First, approximately 500 mg of the catalyst was dissolved in 10 ml of Aqua Regia, a solution constituted of nitric acid (HNO<sub>3</sub>) and hydrochloric acid (HCl) at a ratio of 1:3. To completely dissolve the catalysts, the mixture was boiled for 30 minutes. The samples were diluted in 25 ml of DIW before analysis. Sample analysis was performed on a *Perkin Elmer Optima 4300DV* spectrometer.

### 3.2.6 Transmission Electron Microscope (TEM)

The microstructures and morphology of the catalysts were characterized by a transmission electron microscopy (TEM) with a JEOL JEM-2100 F instrument operating at 200 kV. The samples were reduced at 350 °C for 2 h before this analysis and passivated in 1%  $O_2/N_2$ . Finally, a small fraction of the catalyst was dispersed in ethanol by ultrasonication and placed into the sample holder.

# **3.3 Catalysts Activity Tests**

The activity tests were conducted with a tubular fixed-bed reactor placed inside an oven. A thermocouple is placed just below the catalyst inside the reactor and the heating temperature is controlled by a regulator (Eurotherm 328). The reactant gases ( $CO_2$ ,  $H_2$ , and  $N_2$ ) are supplied by three independent lines, each being controlled by a mass flow controller (Bronckhorst). The pressure is controlled by a back-pressure regulator. A complete scheme of this set up is depicted in Figure 3.3, with their corresponding legends for the components. The catalyst was mixed

with SiC before being placed into the reactor on top of a quartz wool plug. The ratio of catalyst to SiC was typically around 1:5.

Before initiating activity tests, the catalysts were reduced for 2 hours at 350 °C with a temperature rate of 5 °C/min in a 50% vol H<sub>2</sub>/N<sub>2</sub> gas mixture. After reduction, the reactor was purged with N<sub>2</sub> until the temperature was below 50 °C before the reaction mixture was introduced (H<sub>2</sub>/CO<sub>2</sub>/N<sub>2</sub> = 3/1/1). Finally, the pressure was increased to 30 bars, followed by increasing the temperature by 2 °C/min to the desired reaction temperature established at 230 °C.



Figure 3.3. Catalysts activity tests set up

The reaction products were analyzed by a Gas Chromatograph (Agilent Technologies 7890B). The CO<sub>2</sub> conversion ( $X_{CO_2}$ ), and methanol selectivity ( $S_{CH_3OH}$ ) were calculated based on the Eqs. 3.2 and 3.3, respectively.

$$X_{CO_2} = \frac{n_{CO_2}^{in} - n_{CO_2}^{out}}{n_{CO_2}^{in}} * 100\%$$
 (Eq. 3.2)

$$S_{CH_3OH} = \frac{n_{CH_3OH}^{out}}{n_{CO}^{out} + n_{CH_3OH}^{out}} * 100\% \qquad (Eq. 3.3)$$

Where  $n_i^{in}$  and  $n_i^{out}$  represent the moles of the gas species *i* at the inlet and outlet streams of the reactor, respectively; F<sub>i</sub> the molar flow rate, M<sub>i</sub> the molecular weight, and W<sub>cat</sub> is the weight of the catalysts used for the experiment. Additionally, Space-Time Yield (*STY*<sub>CH<sub>3</sub>OH</sub>), defined as the quantity of product per unit of volume per unit of time, was calculated using the Eq. 3.4.

$$STY_{CH_3OH} = \frac{F_{CO_2}^{in} * X_{CO_2} * S_{CH_3OH} * M_{CH_3OH}}{W_{cat}} \quad (Eq. 3.4)$$

Where  $F_{CO_2}^{in}$  is the molar flow rate and  $M_{CH_3OH}$  is the molecular weight of methanol (32.04 gr/mol).

# 4 Results & Discussion

### 4.1 Catalyst Characterization

For identification purposes, catalysts will be denoted as in Table 3.2. For instance, CuZn refers to a Cu + ZnO catalyst prepared by coprecipitation, and In/CuZn represents  $In_2O_3$  impregnated on a Cu + ZnO catalyst.

### 4.1.1 Metal content by ICP-OES

ICP-OES was performed to determine the actual metal content compared to the theoretical concentrations. Table 4.1 shows a comparison between theoretical metal content and the measured metal concentration by ICP-OES.

Catalyst	Theoretical molar ratio (%)				Metal content determined by ICP-OES			CP-OES
					(%)			
	Cu	Zn	Zr	In	Cu	Zn	Zr	In
CuZn	83.3	16.7	_	_	83.2	16.8	_	_
In/CuZn	83.0	16.2	_	0.8	82.1	16.5	_	1.4
CuZr	83.3	_	16.7	_	89.1	_	10.9	
In/CuZr	83.0	_	16.2	0.8	88.0	_	11.0	1.0
CuZrIn	83.0	_	16.2	0.8	88.8	_	11.0	0.2
CuIn	83.3	_	_	16.7	84.1	-	-	15.9
Zr/CuIn	83.0	_	0.8	16.2	Not Avai	lable		

Table 4.1. Theoretical and measured metal content of different catalysts determined by ICP-OES.

### • CuZn and In/CuZn catalysts

For the CuZn catalyst, the actual metal concentration obtained by ICP analysis for Cu and Zn was close to the theoretical, meaning the Cu/ZnO was successfully coprecipitated. When  $In^{3+}$  was impregnated, the actual amount of  $In^{3+}$  was higher than calculated. The value was 1.4% compared to 0.8% molar concentration. This is mostly because the estimated metal content per gram catalysts was higher than the actual values obtained from ICP-OES.

• CuZr, In/CuZr, and CuZrIn catalysts

For the CuZr catalyst, the value after the ICP analysis presented a big deviation from the theoretical content. The expected value of the  $ZrO_2$  was 16.7% compared to the 10.9% obtained. Such a difference can be related to higher crystalline water content in the  $ZrO_2$ 

compound compared to the value used in the calculations. In addition, a difficult solubilization process was experienced when preparing CuZr catalysts, which could also have affected the ZrO<sub>2</sub> content.

Conversely, similar differences were found with the other two catalysts prepared from Cu and  $ZrO_2$ . For the In/CuZr catalyst, the nominal value was 0.8% compared to 1.0% obtained, with minor differences in the Cu and  $ZrO_2$  ratio. Similarly, the CuZrIn catalyst presented a close difference between theoretical In<sub>2</sub>O<sub>3</sub> content, 0.2% versus 0.8%, again without significant variation in the Cu and  $ZrO_2$  ratio. It can be concluded that both preparation methods were successful in introducing In<sub>2</sub>O<sub>3</sub> into the CuZr catalyst.

• Coprecipitated CuIn catalysts

Only Cu and In were coprecipitated to compare the CuIn catalyst with catalysts containing ZnO and ZrO<sub>2</sub>. The value obtained by ICP analysis for Cu and Zn was close to nominal, meaning the CuIn was successfully coprecipitated. Then Zr<sup>4+</sup> was also impregnated to this catalyst, however, ICP-OES was not performed due to minimal activity of the Zr/CuIn catalyst.

### 4.1.2 X-Ray Diffraction

• XRD for Catalyst Precursors

XRD patterns of catalysts' precursors are shown in Fig. 4.1. For the CuZn and CuZr, the diffraction peaks were similar to the characteristic peaks of malachite (Cu<sub>2</sub>CO<sub>3</sub>(OH)<sub>2</sub>) (PDF 01-072-0075). Peaks at 14.9°, 17.6°, 23.9°, 31.3°, 35.5° are identified, corresponding to (020), (120), (220), (201), and (240) planes respectively. Due to their small crystallite size or being amorphous, ZrO<sub>2</sub> and ZnO phases were not detectable. However, the 2 $\theta$  peak at 31.3°, corresponding to the *d* (201) plane is shifted to 32.0° for the CuZn precursor, which can be ascribed to the incorporation of Zn<sup>2+</sup> into the malachite phase [93].

For the coprecipitated CuIn precursor, besides the peaks of malachite,  $In^{3+}$  phases were observed due to the 2 $\theta$  peak at 22.47°. This corresponds to the (200) plane of In(OH)<sub>3</sub>, PDF (01-073-1810). The peak at 31.3° is attributed to (220) plane, however, it is overlapped with the malachite phases. As for the coprecipitated CuZrIn precursor, due to the low content of In<sup>3+</sup>, the representative peaks of In(OH)<sub>3</sub> was not identified.



Figure 4.1. X-Ray Diffraction patterns for catalysts' precursors. To the right, an expanded section of the Cu peak  $(20\overline{1})$  shifted from 31.3° to 32.0° due to the incorporation of Zn<sup>2+</sup> into the malachite phase.

• XRD for calcined catalysts

Figure 4.2 presents the XRD patterns for calcined catalysts. Major peaks corresponding to CuO (11 $\overline{1}$ ) and (111) are located at 2 $\theta$  values of 35.5° and 38.8°, respectively (PDF 00-048-1548). These observations agree with other works [93]. It can be stated that malachite precursors are fully decomposed after calcination at 350 °C since no other components are reflected in the XRD patterns.



Figure 4.2. XRD patterns for calcined catalysts. Horizontal red lines correspond to peaks at 35.5° and 38.8°, identifying CuO(1 1 1) and (1 1 1) planes, respectively.

According to Scherrer's equation (Eq. 2.12), crystallite size is calculated for the calcined catalysts, and the results are presented in Table 4.2. From the values in Table 4.2, it can be seen that the impregnation of  $In_2O_3$  on CuZn increases the crystallite size of CuO from 5.9 to 7.8 nm. This is probably because of the re-calcination at 350 °C, which crystallizes the CuO phase. Similarly,  $In_2O_3$  addition to the CuZr catalyst increases the particle size from 7.9 to 8.8 nm. On the other hand, the crystallite size of CuZrIn (8.2 nm) prepared by co-precipitation is comparable with the CuZr sample.

Table 4.2. Summary of morphological properties of synthesized catalysts. Cu crystallite sizes (dCuO), mean pore sizes, pore volume, BET surface area, and Cu surface area for calcinated catalysts. CuO(111) peak at  $2\theta = 38.7^{\circ}$ 

Catalyst	$d_{ m CuO}$	Pore Size	Pore Volume	BET Surface Area	Cu surface area
	(nm) <sup>a</sup>	(nm) <sup>b</sup>	$(cm^{3}/g)^{b}$	$(m^2/g)^c$	$(m^2/g)^d$
CuZn	5.9	7.7	0.17	72	18
In/CuZn	7.8	7.6	0.11	45	17
CuZr	7.8	7.9	0.18	73	34
CuZrIn	8.2	8.8	0.18	77	36
In/CuZr	8.8	9.2	0.15	63	31
CuIn	7.9	7.6	0.19	74	<1

<sup>a</sup> Determined by the Scherrer's equation from XRD data.

<sup>b</sup> Determined using the BJH method, using the peak distribution value for pore size.

<sup>c</sup> Determined by the BET method

 $^d\,\text{Determined}$  by  $N_2O$  titration

### 4.1.3 N<sub>2</sub>O Titration

The Cu surface area determined by N<sub>2</sub>O titration is also summarized in Table 4.2. Cu surface areas were calculated using the method described in section 2.6.4. and Equation 3.1. The CuZrbased catalysts show the highest Cu surface areas, with values between  $31-36 \text{ m}^2/\text{g}$ , whereas the Cu surface area of the CuZn-based catalysts is around  $17-19 \text{ m}^2/\text{g}$ . This important difference can be supported by previous works, where CuZr catalysts have shown larger Cu surface areas compared to CuZn catalysts [94].

The Cu surface area of CuIn was smaller than 1 m<sup>2</sup>/g. This was due to the coverage of surface Cu by  $In_2O_3$  species during the reduction process, since CuIn reduced at 250 °C showed a surface area of 17 m<sup>2</sup>/g. In general, there are small differences when comparing the effect of  $In_2O_3$  addition to CuZn or CuZr catalysts. A base value of Cu surface area of 34 m<sup>2</sup>/g for the

CuZr catalyst was reduced to 31 m<sup>2</sup>/g by wet impregnation and increased slightly to 36 m<sup>2</sup>/g when prepared by coprecipitation.

## 4.1.4 BET surface area

The BET surface area values are shown in Table 4.2. The surface area of the catalysts that were prepared by co-precipitation was similar (72–77 m<sup>2</sup>/g), where the CuZrIn catalyst showed the highest BET surface area of 77 m<sup>2</sup>/g.

Referring to the addition of  $In_2O_3$ , a drop in the BET surface area is observed when the  $In_2O_3$  is added to the catalyst by wet impregnation. The surface area dropped from 72 to 45 m<sup>2</sup>/g for the CuZn and 73 to 63 m<sup>2</sup>/g for the CuZr. This is probably because of sintering that occurred during the second calcination treatment. The XRD data also indicate that sintering might have occurred. Analyzing the pore sizes, similar pore size is obtained for CuZn, In/CuZn, CuZr, and CuIn around 7.6–7.9 nm. The pore size increased to 8.8 nm for the CuZrIn and was 9.2 nm for the In/CuZr sample.

# 4.1.5 TEM

A set of images was captured for a group of 5 catalysts. TEM images of CuZn-based catalysts are shown in Figure 4.3, where the scale bar is 100 nm. The morphology and particle size are similar for these catalysts, which are composed of agglomerated particles of ca. 50 nm. The large particles are probably composed of Cu, which is the most abundant species in the catalysts. The smaller particles are typically ZnO, which disperses the Cu phase [42]. For the In/CuZn catalysts, no change in the morphology can be seen after the impregnation of CuZn with In.



Figure 4.3. TEM images of reduced and passivated CuZn, and In/CuZn catalysts at 100 nm

Figure 4.4 shows the TEM images of CuZr-based catalysts. Certain dense areas can be observed in CuZr and In/CuZr, which could be caused by a more significant agglomeration of Cu phases. The morphology is relatively similar to that of CuZn-based catalysts with comparable Cu particle size. Very small particles can be seen in CuZr, In/CuZr, and CuZrIn, which can be attributed to ZrO<sub>2</sub>. This is supported by the fact that ZrO<sub>2</sub> phases are not detected by XRD. Furthermore, similar structures have been observed by other studies [58], [95].





Figure 4.4. TEM images of reduced and passivated CuZr-based catalysts (scale bar is 100 nm).

A comparison of the metal oxide phase between In/CuZr and CuZn is shown in Figure 4.5. It can be observed that a group of much smaller particles exist in the In/CuZr sample that can not be observed in the CuZn catalyst. The same observation was made by Natesakhawat et al. [38], comparing CuZnZrGaY with a CuZn catalyst.



Figure 4.5. a) TEM image of In/CuZr catalyst. Small crystals enclosed in the circle attributed to the ZrO2. b) A TEM image from CuZn, where no small particles can be identified.

### 4.1.6 Temperature Programmed Reduction (TPR)

The H<sub>2</sub>-TPR profiles are presented in Figure 4.6. All catalysts show a similar reduction pattern and are fully reduced below 200  $^{\circ}$ C.

• Reducibility of bimetallic catalysts (CuZn, CuIn, CuZr)

The most intense peak appearing at 150–175 °C ( $\beta$ ) is ascribed to highly dispersed CuO species, while the shoulder ( $\gamma$ ) at 160–190 °C is attributed to bulk CuO. A third weak peak ( $\alpha$ ) can be observed for ZrO<sub>2</sub> containing samples. This is related to the interaction between highly dispersed Cu species and the support when ZrO<sub>2</sub> is present, supported by other studies [93, 95]. It can also be seen that CuO is more easily reduced when ZrO<sub>2</sub> is present compared to ZnO or In<sub>2</sub>O<sub>3</sub>, as ( $\beta$ ) and ( $\gamma$ ) peaks are located at lower temperatures compared to CuZn and CuIn.

• Influence of In<sub>2</sub>O<sub>3</sub>

When  $In_2O_3$  is added to the catalyst by wet impregnation, the reduction profile shifts towards higher temperatures, which can be ascribed to more stable CuO species. The increased stability of the CuO species might be due to larger particles or increased crystallinity as well as weakened metal-support interaction. To some extent, this can be attributed to the second calcination cycle at 350 °C since the reducibility is similar for the CuZr and CuZrIn catalysts.



Figure 4.6. H<sub>2</sub>-TPR profiles of calcined catalysts. Peaks ( $\beta$ ) and ( $\gamma$ ) are referenced against CuZn, while ( $\alpha$ ) peak is referenced by CuZr.

## 4.2 Methanol Synthesis Activity

### 4.2.1 Activity tests at 230 °C

All the catalysts synthesized were tested for  $CO_2$  conversion to methanol. Figure 4.7 depicts the methanol selectivity at different  $CO_2$  conversions, calculated by using Eq. 3.2 and 3.3. The  $CO_2$  conversion was varied by changing the gas space hourly velocity (GSHV) from 3600 to 9800 mL/(g<sub>cat</sub> h).

It can be seen that the methanol selectivity increased for all catalysts when the GHSV was increased. This is expected as the methanol synthesis reaction is faster than the RWGS reaction at the conditions used in this work. A similar effect of contact time on the methanol selectivity has also been reported by Tada et al. [58].



Figure 4.7. CO<sub>2</sub> conversion (%) vs. Methanol Selectivity (%) for calcinated catalysts.

Comparison of CuZn and CuZr catalysts

There is a significant difference in the methanol selectivity when CuZn and CuZr catalysts are compared. It can be seen that the trendline appears at higher methanol selectivity for CuZr compared to CuZn. This indicates that the active sites generated on CuZr are more suitable for CO<sub>2</sub> hydrogenation to methanol than Cu/ZnO. The results over different catalysts at 230 °C and a CO<sub>2</sub> conversion of ca. 8% are shown in Table 4.3. For CO<sub>2</sub> conversions around 8%, the methanol selectivity of CuZn was 44.7%, whereas the selectivity was 52.1% for CuZr. However, the methanol production rate was significantly higher for CuZn. The CuZn catalyst exhibited a rate of 523 mg/(g<sub>cat</sub> h), while the rate over CuZr was 420 mg/(g<sub>cat</sub> h). This is attributed to a higher amount of interfacial sites in CuZn compared to CuZr.

The following observations support this conclusion: (i) CuZr contains a lower CuZr ratio; (ii) dense areas are observed by TEM for CuZr indicating separation, which is not observed for CuZn, and (iii) the Cu surface area is higher for CuZr than CuZn, indicating the important role of the interfacial sites as shown by other research groups [52, 53, 56].

Catalyst	CO <sub>2</sub> conversion Methanol selectivi		STY <sub>methanol</sub>
	(%)	(%)	$(mg_{methanol} g_{cat}^{-1} h^{-1})$
CuZn	8.3	44.7	523
In/CuZn	7.8	45.0	322
CuZr	7.6	52.1	420
CuZrIn	7.6	47.8	329
In/CuZr	7.7	51.6	340

Table 4.3. Catalytic performance of different catalysts at 230 °C.

### • Influence of In<sub>2</sub>O<sub>3</sub>

For the CuZn catalysts, there is no significant change in the methanol selectivity trendline when  $In_2O_3$  is added via impregnation (Figure 4.7). However, it can be seen from Table 4.2 that the STY of methanol decreases from 523 to 322 mg/(g<sub>cat</sub> h). Comparing the CuZr and In/CuZr catalysts, the effect is similar as for In addition to CuZn, where the STY of methanol drops from 420 to 329 mg/(g<sub>cat</sub> h). On the contrary, there is a noticeable decline in the methanol selectivity when  $In_2O_3$  was incorporated via coprecipitation. It can be seen from Figure 4.7 that the trendline of CuZrIn appears at lower values compared to CuZr and In/CuZr. Furthermore, CuZrIn exhibits a STY of methanol of only 329 mg/(g<sub>cat</sub> h).

The drop in STY of methanol is attributed to the blockage of active sites by  $In_2O_3$ . This is supported by the fact that CuIn and Zr/CuIn showed very low activity at 230 °C (too low activity to accurately determine it). Additionally, the Zr/CuIn catalyst showed some initial activity when reduced at 250 °C, but deactivated rapidly within the first hour and was eventually completely inactive. This is attributed to the migration of  $In_2O_3$  species that covers the Cu surface, which is supported by the N<sub>2</sub>O results obtained for CuIn reduced at different temperatures.

• Correlating activity to the Cu surface area

To compare the activity of the catalysts, the STY per Cu surface area was calculated for each of the tested catalysts. The STY per surface area Cu is plotted against the Cu surface area in Figure 4.8. No correlation between the activity and the Cu surface area is obtained for the catalysts investigated in this work at 230 °C. It can be seen that the CuZn and In/CuZn shows the highest methanol formation rate per Cu surface area. Although CuZr, In/CuZr, and CuZrIn

show significantly higher Cu surface area, the activity per Cu surface area of these catalysts is much lower than that of CuZn and In/CuZn. It is likely that a significant portion of the Cu is not in proximity to  $ZrO_2$  and therefore, not particularly active for methanol synthesis [96]. In agreement, Wang et al. [54] also concluded that larger Cu surface areas do not imply higher catalytic activity.



Figure 4.8. Cu Surface Area vs. Space-Time Yield/SACu for all selected catalysts.

When  $In_2O_3$  is added to the CuZn and CuZr by impregnation, the activity decreases significantly. This has also been reported by other researchers [17], [19]. The second calcination procedure at 350 °C for 3h after wet impregnation on In/CuZn and In/CuZr catalysts might also have resulted in lower activity due to sinter of the Cu and metal oxide phases.

### 4.2.2 Activity tests at 270 °C

#### • Comparing CuZn and CuZr

The results over different catalysts at 270 °C and a CO<sub>2</sub> conversion of 6.9–8.1% are shown in Table 4.4. Comparing the CuZn and CuZr catalyst, the selectivity of the CuZr catalyst is higher (27.9%) than that of CuZn (10.0%). Furthermore, a STY of methanol of 931 mg/( $g_{cat}$  h) is obtained over CuZr, which is almost 4 times higher than that of CuZn at 268 mg/( $g_{cat}$  h). This further supports that the active sites of CuZr are more favorable for methanol production compared to the active sites on CuZn.

Catalyst	CO <sub>2</sub> conversion	Methanol selectivity	STY <sub>methanol</sub>
	(%)	(%)	$(mg_{methanol} g_{cat}^{-1} h^{-1})$
CuZn	6.9	10.0	268
In/CuZn	7.1	10.8	174
CuZr	7.8	27.9	931
CuZrIn	7.4	32.2	971
In/CuZr	8.1	38.9	449

Table 4.4. Catalytic performance at 270 °C of different catalysts.

### • Effect of In<sub>2</sub>O<sub>3</sub>

The effect of  $In_2O_3$  addition to CuZn has no noticeable effect on the selectivity of the catalyst at similar CO<sub>2</sub> conversion. Similar to the results at 230 °C, a drop in the STY of methanol is still observed at 270 °C from 268 mg/(g<sub>cat</sub> h) for CuZn to 174 mg/(g<sub>cat</sub> h) for In/CuZn. In contrast, an improvement in methanol selectivity can be seen for In<sub>2</sub>O<sub>3</sub> addition to CuZr. The highest methanol selectivity at 270 °C of 38.9% is obtained over In/CuZr. Furthermore, the STY of methanol is higher for CuZrIn at 971 mg/(g<sub>cat</sub> h) than CuZr (931 mg/(g<sub>cat</sub> h)). These results suggest that In<sub>2</sub>O<sub>3</sub> species are involved in the active site when In<sub>2</sub>O<sub>3</sub> addition to CuZn, the results suggest that a synergistic effect between ZrO<sub>2</sub> and In<sub>2</sub>O<sub>3</sub> species is present. However, the In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> sites appear to require a higher temperature to be active, which is also typically the case for In<sub>2</sub>O<sub>3</sub>-based catalysts [16] [63] [64].

A similar conclusion has also been reported by Yao et al. for CuZrIn catalysts [18],where defective  $In_2O_3$  sites enhanced  $CO_2$  adsorption and methanol selectivity. The CuZrIn catalysts investigated in this work could have potential as a selective catalyst at high temperatures. However, further work is required to optimize the catalyst.

# **5** Conclusions

The present work evaluated the characteristics and the catalytic performance of  $In_2O_3$ -promoted CuZn and CuZr for CO<sub>2</sub> hydrogenation to methanol.  $In_2O_3$ -containing catalysts were prepared via wet impregnation and coprecipitation methods. Several procedures were carried out to evaluate the physicochemical and textural features of the catalysts, such as XRD, H<sub>2</sub>-TPR, TEM, ICP-OES, N<sub>2</sub>O titration, and N<sub>2</sub> physisorption.

The main conclusions from the systematic catalyst characterization can be summarized as in the following:

- Malachite precursors can fully decompose after calcination at 350 °C, and it is the predominant crystalline structure for the catalysts synthesized in this work.
- Adding In<sub>2</sub>O<sub>3</sub> leads to an increase in the crystallite size of Cu-based catalysts.
- The highest Cu surface area is obtained for CuZr compared to CuIn and CuZn.
- In<sub>2</sub>O<sub>3</sub> increases the reduction temperature for CuO. The opposite effect is caused by ZrO<sub>2</sub>, which leads to a lower reducing temperature.
- N<sub>2</sub>O titration indicates that In<sub>2</sub>O<sub>3</sub> species migrate to the Cu surface at relatively low temperatures.

The activity tests showed that CO<sub>2</sub> conversion, selectivity, and STY were different for CuZnand CuZr-based catalysts:

- There is no significant effect when In<sub>2</sub>O<sub>3</sub> was added to Cu-based catalysts via wet impregnation method under the experimental conditions performed in this work. On the other hand, there is a clear reduction in the catalytic activity when In<sub>2</sub>O<sub>3</sub> is synthesized by coprecipitation.
- CuZn and CuZr based catalysts present relatively similar activity for the reaction conditions of the experiment, with CO<sub>2</sub> conversion values around 8% and methanol selectivities between 45-55%. Experimental values showed CuZr catalysts yield higher methanol selectivity values compared to CuZn catalysts.
- Despite a smaller Cu surface area for CuZn catalysts, the catalytic activity per Cu surface area is 2-3 times higher for CuZn catalysts than the CuZr catalysts at 230 °C
- CuZr catalysts show better performance than CuZn at 270 °C
- CuIn and Zr/CuIn are not particularly active for the reaction conditions carried out in this work, probably because of significant coverage of Cu by In<sub>2</sub>O<sub>3</sub>.

- In<sub>2</sub>O<sub>3</sub> reduced the catalytic activity per Cu surface area at 230 °C, regardless of the synthesis method for Cu-based catalysts.
- In<sub>2</sub>O<sub>3</sub> can enhance the methanol selectivity and the STY of methanol at 270 °C for CuZr, whereas it only lowers the activity of CuZn

## **5.1 Future Work Recommendations**

Utilizing  $In_2O_3$  can enhance the performance of CuZr-based catalysts at high reaction temperatures. One of the challenges is that  $In_2O_3$  will migrate and cover the Cu surface at high  $In_2O_3$  content and deactivate the catalysts. Thus, it could be a promising catalyst for high-temperature applications if  $In_2O_3$  could be stabilized in proximity to  $ZrO_2$ .

It is necessary to investigate the  $In_2O_3$  to  $ZrO_2$  ratio to avoid coverage of Cu species. More work regarding stability is also required. The limited investigations and the lack of a solid consensus on the catalytic activity of  $In_2O_3$  for  $CO_2$  hydrogenation to methanol are yet other drivers for carrying out investigations on its promotional effects over Cu-based catalytic systems.

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